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E N S A Y O S

## TESTING FOR THE VERIFICATION OF COMPLIANCE OF PV INVERTER WITH: <br> FGW TG3: DETERMINATION OF THE ELECTRICAL CHARACTERISTICS OF POWER GENERATING UNITS AND SYSTEMS, STORAGE SYSTEMS AS WELL FOR THEIR COMPONENTS IN MV, HV AND EHV GRIDS. (REVISION 25 DATED 01/09/2018 + SUPPLEMENT 1 DATED ON 22/01/2019)

Test Report Number ..... 2219 / 0163 - A
Type

$\qquad$
Tested Model

$\qquad$ : 3 Phase Grid Connected PV Inverter : SOFAR 33000TL-G2Variant Models
$\qquad$SOFAR 30000TL-G2, SOFAR 25000TL-G2,SOFAR 20000TL-G2
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Laboratorio de Ensayos ExE
Date of issue

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## Test Report Historical Revision:

| Test Report Version | Date | Resume |
| :---: | :---: | :---: |
| $2219 / 0163-A$ | $2020 / 09 / 07$ | First issuance |
|  |  |  |


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## 1 SCOPE

SGS Tecnos, S.A. (Electrical Testing Laboratory) has been contract by Shenzhen SOFAR SOLAR Co., Ltd. to perform testing according to FGW-TG3: Technical Guidelines for Power Generating Units and Systems. TG3 (Revision 25 Dated 01/09/2018 + Supplement 1 Dated 22/01/2019): Determination of Electrical Characteristics of Power Generating Units and Systems, Storage Systems as well for their Components in MV, HV and EHV grids.

The following standards are covered with testing of FGW-TG3 (Revision 25 Dated 01/09/2018) (*):

- VDE-AR-N 4110: 2018-11. Technical requirements for the connection and operation of customer installations to the medium voltage network (TAR medium voltage).
(*) As stated in chapter 11.2.1 of VDE-AR-N 4110.

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## 2 GENERAL INFORMATION

### 2.1 TESTING PERIOD AND CLIMATIC CONDITIONS

The necessary testing has been performed along between $20^{\text {th }}$ Nov. 2019 to $26^{\text {th }}$ Dec. 2019, $1^{\text {st }}$ Mar. 2020 to 03 ${ }^{\text {rd }}$ Sep. 2020.

All the tests and checks have been performed at climatic conditions:

| Temperature | $25 \pm 10{ }^{\circ} \mathrm{C}$ |
| :---: | :---: |
| Relative Humidity | $50 \pm 20 \%$ |
| Pressure | $90 \pm 10 \mathrm{kPa}$ |

## SITE TEST 1

Name $\qquad$ : Dongguan BALUN Technology Co., Ltd.
Address $\qquad$ .: Room 104, 204, 205, Building 1, No. 6, Industrial South Road, Songshan Lake Park, Dongguan, Guangdong Province, P. R. China523808

### 2.2 Equipment under Testing

Apparatus type $\qquad$ : Grid-Connected PV Inverter
Installation $\qquad$ : Fixed installation

Manufacturer
: Shenzhen SOFAR SOLAR Co., Ltd.
Trade mark
: SOFAR SOLAR
Model / Type reference
: SOFAR 33000TL-G2
Serial Number
: SL1CS033KB5179
Software Version
: V2.50
Checksum
: N/A
$\qquad$ : Input: $1100 \mathrm{~V}_{\mathrm{dc}, \max }\left(230-960 \mathrm{~V}_{\mathrm{dc}, \text { MPPT, }}\right.$ Full load range MPPT: $580 \mathrm{~V}_{\mathrm{dc}}-850 \mathrm{~V}_{\mathrm{dc}}$ ), ; $30 \mathrm{~A}_{\mathrm{dc}} / 30 \mathrm{~A}_{\mathrm{dc}} \mathrm{Max}$. Output: 3/N/PE 230/400Vac; $50 \mathrm{~Hz} ; 3 \times 47.8 \mathrm{~A}_{\text {ac. }}$; 33000W Rated; 36300VA Max.
Date of manufacturing: 2019

| Test item particulars |  |
| :---: | :---: |
| Input ..................................................... : | DC |
| Output .................................................... | 3 Phase ~ |
| Class of protection against electric shock... : | Class I |
| Degree of protection against moisture........ : | IP 65 |
| Type of connection to the main supply ....... : | Three-phase - Fixed installation |
| Cooling group........................................ : | Forced ventilation (Fan) |
| Modular ................................................. : | No |
| Internal Transformer ............................... : | No |


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## Copy of marking plate (representative):



## Note:

1. The above markings are the minimum requirements required by the safety standard. For the final production samples, the additional markings which do not give rise to misunderstanding may be added.
2. Label is attached on the side surface of enclosure and visible after installation
3. Labels of other models are as the same with SOFAR 33000TL-G2's except the parameters of rating

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Equipment under testing:

- SOFAR 33000TL-G2

The variants models are:

- SOFAR 30000TL-G2
- SOFAR 25000TL-G2
- SOFAR 20000TL-G2

| Model Number | $\begin{aligned} & \text { SOFAR 20000TL- } \\ & \text { G2 } \end{aligned}$ | $\begin{gathered} \text { SOFAR } 25000 \mathrm{TL} \\ \text { G2 } \end{gathered}$ | $\begin{aligned} & \text { SOFAR 30000TL- } \\ & \text { G2 } \end{aligned}$ | $\begin{gathered} \text { SOFAR 33000TL- } \\ \text { G2 } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| Max. PV input voltage | $1100 \mathrm{~V}_{\mathrm{dc}}$ |  |  |  |
| Operating MPPT voltage range | $230 V_{\text {dc }}-960 V_{\text {dc }}$ |  |  |  |
| Full load MPPT voltage range | $480 \mathrm{~V}_{\mathrm{dc}}-850 \mathrm{~V}_{\text {dc }}$ | $460 \mathrm{~V}_{\mathrm{dc}}-850 \mathrm{~V}_{\mathrm{dc}}$ | $520 \mathrm{~V}_{\mathrm{dc}}-850 \mathrm{~V}_{\text {dc }}$ | $580 \mathrm{~V}_{\mathrm{dc}}-850 \mathrm{~V}_{\text {dc }}$ |
| No. Of MPP inputs | 2 |  |  |  |
| Max. input current | 24A $\mathrm{A}_{\text {dc }} / 24 \mathrm{~A}_{\text {dc }}$ | 28Adc / 28Adc | 30Adc / 30Adc | 30Adc / 30Adc |
| Rated grid voltage | 3P/N/PE 230/400V ${ }_{\text {ac }}$ |  |  |  |
| Rated grid frequency | 50 Hz |  |  |  |
| Rated output power | 20000W | 25000W | 30000W | 33000W |
| Max. output power | 22000VA | 27500VA | 33000VA | 36300VA |
| Max. AC output Current | $3 \times 32 \mathrm{Aac}^{\text {a }}$ | $3 \times 40 \mathrm{Aac}^{\text {a }}$ | $3 \times 48$ ac | $3 \times 53 \mathrm{Aac}$ |
| Rated AC output Current | $3 \times 29.0 \mathrm{Aac}$ | $3 \times 36.2 \mathrm{Aac}^{\text {a }}$ | $3 \times 43.5 \mathrm{Aac}$ | $3 \times 47.8 \mathrm{Aac}$ |
| Power factor range | 0.8 lagging to 0.8 leading |  |  |  |

The variants models have been included in this test report without tests because the following features don't change regarding to the tested model:

- Same connection system and hardware topology
- Same control algorithm.
- Same Firmware Version
- Output power within $1 / \sqrt{ } 10$ and 2 times the rated output power or the EUT or Modular inverters

The results obtained apply only to the particular sample tested that is the subject of the present test report. The most unfavorable result values of the verifications and tests performed are contained herein. Throughout this report a comma (point) is used as the decimal separator.

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### 2.2.1 Reference Values

The values presented in the following table have been used for calculation of referenced values (p.u.; \%) througth the report.

| Reference Values |  |
| :--- | :--- |
| Rated power, Pn in kW | 33 |
| Max. output power, Pmax in kW | 36.3 |
| Rated apparent power, Sn in kVA | 33 |
| Rated wind speed (only WT), vn in m/s | Not applicable |
| Rated current (determined), In in A | 47.8 |
| Rated output voltage, (phase to phase) Un in Vac | 230 |
| Note: In this report p.u. values are calculated as follows: <br> -For Active \& Reactive Power p.u values are reference to Pn <br> -For Currents p.u values, the reference is always In <br> -For Voltages p.u values, the reference is always Un |  |


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### 2.3 SGS Test EQUIPMENT LIST

Test date from 20 ${ }^{\text {th }}$ Nov. 2019 to 26 $^{\text {th }}$ Dec. 2019

| From | No. | Equipment Name | MARK/Model No. | Equipment No. | Equipment calibration due date |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \frac{\cong}{\bar{N}} \\ & \stackrel{n}{0} \end{aligned}$ | 1 | Current clamp | HIOKI / CT6863-05 | $\begin{gathered} \text { 150613621/BZ- } \\ \text { EP-L006 } \end{gathered}$ | $\begin{gathered} \text { 2019/2/28 to } \\ \text { 2020/2/27 } \end{gathered}$ |
|  | 2 | Current clamp | HIOKI / CT6863-05 | $\begin{gathered} \text { 150613623/BZ- } \\ \text { EP-L007 } \end{gathered}$ | $\begin{gathered} \text { 2019/2/28 to } \\ \text { 2020/2/27 } \end{gathered}$ |
|  | 3 | Current clamp | HIOKI / CT6863-05 | $\begin{gathered} \text { 150613626/BZ- } \\ \text { EP-L008 } \end{gathered}$ | $\begin{gathered} \text { 2019/2/28 to } \\ 2020 / 2 / 27 \end{gathered}$ |
|  | 4 | Current clamp | HIOKI / CT6863-05 | $\begin{gathered} \text { 150613627/BZ- } \\ \text { EP-L009 } \end{gathered}$ | $\begin{gathered} \text { 2019/2/28 to } \\ \text { 2020/2/27 } \end{gathered}$ |
|  | 5 | Power analyzer | DEWETRON / DEWE2-A4 | B0180377-Aut | $\begin{gathered} 2019 / 10 / 10 \text { to } \\ 2020 / 10 / 9 \end{gathered}$ |
| $\begin{aligned} & \text { 층 } \\ & \text { © } \\ & \text { त̄ } \\ & \text { © } \end{aligned}$ | 6 | Temperature \& Humidity meter | Anymeters / TH101B | 201030245220 | $\begin{aligned} & \text { 2019/2/13 to } \\ & 2020 / 2 / 12 \end{aligned}$ |
|  | 7 | Digital oscilloscope | Agilent / DS05014A | MY50070266 | $\begin{gathered} \text { 2019/2/13 to } \\ 2020 / 2 / 12 \end{gathered}$ |
|  | 8 | Voltage probe | SANHUA / SI-9110 | 111541 | $\begin{gathered} \text { 2019/2/13 to } \\ 2020 / 2 / 12 \end{gathered}$ |
|  | 9 | Voltage probe | SANHUA / SI-9110 | 152627 | $\begin{gathered} \text { 2019/2/13 to } \\ 2020 / 2 / 12 \end{gathered}$ |
|  | 10 | Voltage probe | SANHUA / SI-9110 | 111134 | $\begin{gathered} \text { 2019/2/13 to } \\ 2020 / 2 / 12 \end{gathered}$ |
|  | 11 | Power analyzer | ZLG / PA3000 | $\begin{gathered} \text { PA3005-P0005- } \\ 1246 \end{gathered}$ | $\begin{aligned} & \text { 2019/2/13 to } \\ & 2020 / 2 / 12 \end{aligned}$ |
|  | 12 | Current probe | FLUKE / i1000s | 29503223 | $\begin{gathered} \text { 2019/2/13 to } \\ 2020 / 2 / 12 \end{gathered}$ |
|  | 13 | Current probe | FLUKE / i1000s | 30413448 | $\begin{gathered} \text { 2019/2/13 to } \\ 2020 / 2 / 12 \end{gathered}$ |
|  | 14 | Current probe | CYBERTEK / <br> CP5150 | C150150008 | $\begin{aligned} & \text { 2019/2/13 to } \\ & 2020 / 2 / 12 \end{aligned}$ |
| $\begin{aligned} & \infty \\ & 0 \\ & \end{aligned}$ | 15 | True RMS Multimeter | Fluke / 289C | GZE012-53 | $\begin{gathered} \text { 2019/2/26 to } \\ 2020 / 2 / 25 \end{gathered}$ |


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Test date from $1^{\text {st }}$ Mar. 2020 to $3^{\text {rd }}$ Sep. 2020

| From | No. | Equipment Name | MARK/Model No. | Equipment No. | Equipment calibration due date |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 6 | Temperature \& Humidity meter | Anymeters / TH101B | ZB-WSDJ-001 | $\begin{gathered} 2020 / 1 / 14 \text { to } \\ 2021 / 1 / 13 \end{gathered}$ |
|  | 7 | Digital oscilloscope | Agilent / DS05014A | MY50070288 | $\begin{gathered} 2020 / 1 / 14 \text { to } \\ 2021 / 1 / 13 \end{gathered}$ |
|  | 8 | Voltage probe | SANHUA / SI-9110 | 111152 | $\begin{gathered} 2020 / 1 / 14 \text { to } \\ 2021 / 1 / 13 \end{gathered}$ |
|  | 9 | Voltage probe | SANHUA / SI-9110 | 152627 | $\begin{gathered} 2020 / 1 / 14 \text { to } \\ 2021 / 1 / 13 \end{gathered}$ |
|  | 10 | Voltage probe | SANHUA / SI-9110 | 111134 | $\begin{gathered} 2020 / 1 / 14 \text { to } \\ 2021 / 1 / 13 \end{gathered}$ |
|  | 11 | Power analyzer | ZLG / PA5000 | $\begin{gathered} \text { C820290908200 } \\ 2110001 \end{gathered}$ | 2020/3/2 to 2021/3/1 |
|  | 12 | Current probe | CP1000A | C181000922 | $\begin{gathered} 2020 / 1 / 14 \text { to } \\ 2021 / 1 / 13 \end{gathered}$ |
|  | 13 | Current probe | CP1000A | C181000925 | $\begin{gathered} 2020 / 1 / 14 \text { to } \\ 2021 / 1 / 13 \end{gathered}$ |
|  | 14 | Current probe | CP1000A | C181000929 | $\begin{gathered} 2020 / 1 / 14 \text { to } \\ 2021 / 1 / 13 \end{gathered}$ |
| $\begin{aligned} & \infty \\ & \text { © } \end{aligned}$ | 15 | True RMS Multimeter | Fluke / 289C | GZE012-53 | $\begin{gathered} \text { 2020/02/21 to } \\ 2021 / 02 / 20 \end{gathered}$ |


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### 2.4 Measurement uncertainty and Data Sampling Rates

Associated uncertainties through measurements showed in this this report are the maximum allowable uncertainties.

| Magnitude | Uncertainty |
| :--- | :--- |
| Voltage measurement | $\pm 1.5 \%$ |
| Current measurement | $\pm 2.0 \%$ |
| Frequency measurement | $\pm 0.2 \%$ |
| Time measurement | $\pm 0.2 \%$ |
| Power measurement | $\pm 2.5 \%$ |
| Phase Angle | $\pm 10$ |
| Temperature | $\pm 30 \mathrm{C}$ |
| Note1: Measurements uncertainties showed in this table are maximum allowable uncertainties. The <br> measurement uncertainties associated with other parameters measured during the tests are in the <br> laboratory at disposal of the petitioner. <br> Note2: Where the standard requires lower uncertainties that those in this table. Most restrictive <br> uncertainty has been considered. |  |

Applicable to measurement and testing equipment (without current and voltage transformers), The following measurements uncertainties have been taken into account for the performance of the testing process:

|  | Measurement uncertainty (K=2) |
| :--- | :--- |
| Voltage (Fundamental frequency) | $\leq 0.5 \%$ of Un |
| Current (Fundamental frequency) | $\leq 0.5 \%$ of In |
| Harmonic current up to 9 kHz |  |
| $\geq 0.1 \%$ In | $\leq 30 \%$ relative to the measured value |
| $<0.1 \%$ In | $\leq 0.03 \%$ of In |
| Setpoint signals | $\leq 0.5 \%$ of the reference variable (e.g 20 mA corresponding to |
| Plicker | $\leq 5.8 \%$ relative to Pst $=1$ |
| Grid protection |  |
|  | Specific voltage $\leq 0.5 \%$ of Un |
| Note: regarding flicker measurement uncertainty: IEC $61000-4-15$ relates to a tolerance (accuracy) of $<5 \%$ <br> Based on the assumption that the tolerance follows a rectangular distribution, the simple uncer-tainty is: (5\%) / <br> $\sqrt{3}=2.89 \%$. This results in an extended uncertainty at $\mathrm{k}=2$ of $5.8 \%$. |  |

Data sampling rates have been applied complying with the chapter 3.3 of the standard:

|  | Chapter of <br> standard | Voltage, <br> currents | Setpoint and actual <br> value signals | External <br> signals |
| :---: | :---: | :---: | :---: | :---: |
| Active power output | 4.1 | $\geq 3 \mathrm{kHz}$ | $\geq 3 \mathrm{kHz}$ | $\geq 1 \mathrm{~Hz}$ |
| Reactive power provision | 4.2 | $\geq 3 \mathrm{kHz}$ | $\geq 3 \mathrm{kHz}$ | $\geq 1 \mathrm{~Hz}$ |
| Switching operations, flicker | $4.3 .2,4.3 .3$ | $\geq 3 \mathrm{kHz}$ | -- | $\geq 1 \mathrm{~Hz}$ |
| Harmonics | 4.3 .4 | $\geq 20 \mathrm{kHz}$ | -- | $\geq 1 \mathrm{~Hz}$ |
| PGU disconnection from the grid | 0 | $\geq 10 \mathrm{kHz}$ | -- | $\geq 10 \mathrm{kHz}$ |
| Verification of cut-in conditions | 4.5 | $\geq 3 \mathrm{kHz}$ | -- | $\geq 1 \mathrm{~Hz}$ |
| Response during grid faults | 4.6 | $\geq 10 \mathrm{kHz}$ | -- | $\geq 1 \mathrm{~Hz}$ |


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### 2.5 Test set up \& Test Conditions

### 2.5.1 Test set up \& Test Conditions.

Below is the simplified construction of the test set up used in all test of this report


| Test Conditions |  |  |
| :---: | :---: | :---: |
| Condition | Value | Comments |
| Point of measurement | EUT Output (Low Voltage) | Equipment enounced in section 2.3 of this report has been used in the point of measurement |
| Short circuit ratio at the measurement point ( $\mathrm{S}_{\mathrm{k}} / \mathrm{Sn}$ ) | 2.27 | $S_{\text {k }}=75 \mathrm{KVA}, \mathrm{S}_{\mathrm{n}}=33 \mathrm{KVA}$ |
| If the PGU is connected directly to the medium-voltage grid and a step-up transformer is installed between the PGU and the grid (which is not part of the PGU), a standard transformer must be used, the rated apparent power of which corresponds at least to the rated apparent power of the PGU being evaluated. | All the tests have been performed measuring at the output of the PGU. No MV transformer used for the test measurments. |  |
| MV Tansformer: Short circuit Power | -- | Not applicable measured in Low voltage side |
| MV Tansformer: <br> Network impedance Phase Angle | -- | Not applicable measured in Low voltage side |
| MV Tansformer: Service voltage Uc | -- | Not applicable measured in Low voltage side |
| LV Isolation transformer: Nominal Power (kVA) | -- | AC simulator used for the test |
| LV Isolation transformer: Short circuit voltage $U_{k}$ (\%) | -- | AC simulator used for the test |
| LV Isolation transformer: Tap possition | -- | AC simulator used for the test |
| MV Side: Additional impedance | -- | Not applicable measured in Low voltage side |
| LV Side: <br> Additional impedance | Active $0 \Omega$ Reactive $0 \Omega$ |  |
| The THDSU of the voltage which includes all integer harmonics up to the 50th order must be smaller | See section 2.5.2 of this report |  |


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| Test Conditions |  |  |
| :---: | :---: | :---: |
| Condition | Value | Comments |
| than $5 \%$. It is measured as the 10-minute mean at the PGU terminals while the PGU is not generating any power. |  |  |
| The voltage, measured as a 10minute mean at the PGU terminals, must lie within a range of $\pm 10 \%$ of the rated voltage | Phase A: 0.11\% <br> Phase B: 0.07\% <br> Phase C: 0.14\% |  |
| The voltage unbalance, measured as a 10 -minute mean at the PGU terminals, must be less than $2 \%$. | -0.335\% |  |
| The grid frequency, measured as a 0.2 second mean, must lie within a range of $\pm 1 \%$ of the rated frequency around the rated frequency. The rate of change of the grid frequency, measured as a 0.2 second mean, must be smaller than $0.2 \%$ of the rated fre-quency per 0.2 seconds. | $\begin{aligned} & \hline \text { Tested Max. Value } 50.008 \mathrm{~Hz} \\ & \text { Tested Min. Value } 49.993 \mathrm{~Hz} \\ & \text { Tested Avg. Value: } 50.002 \mathrm{~Hz} \end{aligned}$ |  |
| Note 1: These test conditions have been used in all the test performed in Section 4 of this report. Note 2: See also the test bench information table in this section |  |  |


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### 2.5.2 Voltage harmonic for Test bench

Measurements of voltage harmonics at continuous operation are done according to IEC 61000-4-7:2002

| Nr./ Order | Phase A Uh(\%) | Phase A $\mathrm{U}_{\mathrm{h}}(\%)$ | Phase A $\mathrm{U}_{\mathrm{h}}(\%)$ | Limited |
| :---: | :---: | :---: | :---: | :---: |
| 2 | 0.465 | 0.075 | 0.098 | 5 |
| 3 | 0.370 | 0.234 | 0.234 | 5 |
| 4 | 0.305 | 0.050 | 0.062 | 5 |
| 5 | 0.167 | 0.170 | 0.175 | 5 |
| 6 | 0.123 | 0.018 | 0.018 | 5 |
| 7 | 0.142 | 0.105 | 0.106 | 5 |
| 8 | 0.051 | 0.021 | 0.012 | 5 |
| 9 | 0.073 | 0.063 | 0.063 | 5 |
| 10 | 0.021 | 0.015 | 0.016 | 5 |
| 11 | 0.069 | 0.040 | 0.051 | 5 |
| 12 | 0.011 | 0.009 | 0.010 | 5 |
| 13 | 0.063 | 0.040 | 0.045 | 5 |
| 14 | 0.019 | 0.020 | 0.020 | 5 |
| 15 | 0.050 | 0.039 | 0.046 | 5 |
| 16 | 0.019 | 0.024 | 0.023 | 5 |
| 17 | 0.036 | 0.042 | 0.037 | 5 |
| 18 | 0.010 | 0.018 | 0.020 | 5 |
| 19 | 0.018 | 0.031 | 0.029 | 5 |
| 20 | 0.009 | 0.011 | 0.014 | 5 |
| 21 | 0.009 | 0.018 | 0.018 | 5 |
| 22 | 0.012 | 0.009 | 0.010 | 5 |
| 23 | 0.009 | 0.014 | 0.010 | 5 |
| 24 | 0.012 | 0.012 | 0.012 | 5 |
| 25 | 0.013 | 0.013 | 0.009 | 5 |
| 26 | 0.012 | 0.010 | 0.012 | 5 |
| 27 | 0.018 | 0.013 | 0.013 | 5 |
| 28 | 0.010 | 0.008 | 0.008 | 5 |
| 29 | 0.026 | 0.015 | 0.016 | 5 |
| 30 | 0.008 | 0.009 | 0.010 | 5 |
| 31 | 0.026 | 0.013 | 0.015 | 5 |
| 32 | 0.009 | 0.011 | 0.012 | 5 |
| 33 | 0.025 | 0.014 | 0.014 | 5 |
| 34 | 0.012 | 0.012 | 0.012 | 5 |
| 35 | 0.020 | 0.012 | 0.012 | 5 |
| 36 | 0.012 | 0.012 | 0.012 | 5 |
| 37 | 0.014 | 0.012 | 0.010 | 5 |
| 38 | 0.012 | 0.010 | 0.009 | 5 |
| 39 | 0.009 | 0.010 | 0.009 | 5 |
| 40 | 0.010 | 0.008 | 0.007 | 5 |
| 41 | 0.008 | 0.010 | 0.008 | 5 |
| 42 | 0.009 | 0.006 | 0.007 | 5 |
| 43 | 0.007 | 0.011 | 0.008 | 5 |
| 44 | 0.009 | 0.006 | 0.007 | 5 |
| 45 | 0.007 | 0.009 | 0.007 | 5 |
| 46 | 0.008 | 0.006 | 0.007 | 5 |
| 47 | 0.009 | 0.009 | 0.007 | 5 |
| 48 | 0.008 | 0.007 | 0.007 | 5 |
| 49 | 0.012 | 0.009 | 0.008 | 5 |
| 50 | 0.010 | 0.008 | 0.008 | 5 |
| $\begin{aligned} & \text { TDD } \\ & (\%) \\ & \hline \end{aligned}$ | 0.734 | 0.349 | 0.360 | -- |


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| :---: | :---: | :---: |
|  | FGW-TG3+SP1 |  |

## Test bench used includes:

|  | EQUIPMENT | MARK / MODEL | RATED CHARACTERISTICS | OWNER / ID.CODE |
| :---: | :---: | :---: | :---: | :---: |
| $\underset{\boldsymbol{N}}{\boldsymbol{\sim}}$ | AC source | Wogo / WLPA-330-75kVA | $\begin{gathered} 75 \mathrm{kVA} \\ 5-300 \mathrm{Vrms} \\ 45-65 \mathrm{~Hz} \end{gathered}$ | $\begin{gathered} \text { BALUN / BZ-DGD- } \\ \text { L014 } \end{gathered}$ |
|  | DC source | Wogo / WLPA- $150 \mathrm{~kW}$ | $\begin{gathered} 0-1500 \mathrm{Vdc}(0.01 \mathrm{~V} \text { step }) \\ 0-200 \mathrm{~A}(0.01 \mathrm{~A} \text { step }) \end{gathered}$ | BALUN / BZ-DGDL013 |
|  | RLC load | Qunlin / ACLT3820H | 68kW, 68kVAr | $\begin{gathered} \text { BALUN / BZ-DGD- } \\ \text { L063 } \end{gathered}$ |

Test bench requirements according to Annex D from the standard.

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| :---: | :---: | :---: |
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### 2.6 Definitions

| EUT | Equipment Under Testing | W | Watt |
| :---: | :---: | :---: | :---: |
| A | Ampere | p.u. | Per unit |
| VAr | Volt-Ampere reactive | Pn | Nominal Active Power |
| Un | Nominal Voltage | $\mathrm{P}_{\text {mom }}$ | Instantaneous Active Power |
| In | Nominal Current | Pref | $\mathrm{P}_{\text {mom }}$ in case of PV and Storage |
| MV | Medium Voltage | $P_{10}$ | Active power as 10 s mean value |
| LV | Low Voltage | Qn | Nominal Reactive Power |
| LVRT | Low Voltage Ride Through | Sn | Nominal Apparent Power |
| $\mathrm{V} 1+$ / $\mathrm{V}_{\mathrm{AC}}+$ | Voltage positive sequence | $S_{\text {k }}$ | Symetrical Fault level |
| $\mathrm{V} 1-\mathrm{l} \mathrm{V}_{\mathrm{AC}}$ - | Voltage negative sequence | In | Harmonic Current |
| $\mathrm{K}_{\mathrm{f}}\left(\Psi_{\mathrm{k}}\right)$ | Flicker Form Factor | TDC | Total Demand Current Distortion |
| $\mathrm{K}_{\mathrm{u}}\left(\Psi_{\mathrm{k}}\right)$ | Voltage Variation Factor | TDD | Total Demand Distortion |
| $\mathrm{P}_{\text {st }}$ | Short-term flicker disturbance factor | THDSu | Subgroup Total Harmonic Distortion |
| PGU | Power Genaration Unit | Ui | Current Imbalance |
| Hz | Hertz | Uv | Voltage Imbalance |
| V | Volt | ${ }^{+}$ | Current Positive Sequence |
|  |  | 11- | Current Negative Sequence |


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| :---: | :---: | :---: |
| FGW-TG3+SP1 |  |

## 3 RESUME OF TEST RESULTS

## INTERPRETATION KEYS

Test object does meet the requirement ......................: P
Test object does not meet the requirement................: F
Test case does not apply to the test object .................: N/A
To make a reference to a table or an annex. .............: See additional sheet
To mable
To indicate that the test has not been realized ..........: N/R Not realized

| VDE-AR- | FGW TG3 | CHAPTER OF THE STANDARD |  |
| :---: | :---: | :---: | :---: |
| SECTION | SECTION | FGW-TG3 |  |
| -- | 4.1 | Active Power Output | P |
| 11.2.7 | 4.1.1 | Active power peaks | P |
| $\begin{aligned} & \hline \text { 10.2.4.1 } \\ & \text { 10.2.4.2 } \\ & \text { 11.2.7 } \end{aligned}$ | 4.1.2 | Operating power limited by grid operator | P |
| $\begin{aligned} & \hline 10.2 .4 .3 \\ & 11.2 .8 \end{aligned}$ | 4.1.3 | Active power feed-in as a function of grid frequency | P |
| $\begin{aligned} & \text { 10.2.4 } \\ & \text { 11.2.11 } \end{aligned}$ | 4.1.4 | Active power gradient following disconnection from the grid | P |
| -- | 4.2 | Reactive Power Provision | P |
| $\begin{aligned} & \hline 10.2 .2 .4 \\ & 11.2 .4 \\ & \hline \end{aligned}$ | 4.2.1 | Reactive power response in the normal operating mode ( $\mathrm{Q}=0 \mathrm{kVAr}$ ) | P |
| $\begin{aligned} & \text { 10.2.2.4 } \\ & \text { 11.2.4 } \end{aligned}$ | 4.2.2 | Measuring the maximum reactive power range (PQ Diagram) | P |
| $\begin{aligned} & \hline 10.2 .2 \\ & 11.2 .4 \\ & \hline \end{aligned}$ | 4.2.3 | Measuring separate operating points in the voltagedependent PQ diagram | P |
| $\begin{aligned} & \hline \text { 10.2.2.4 } \\ & \text { 11.2.4 } \end{aligned}$ | 4.2.4 | Reactive power following setpoints | P |
| $\begin{aligned} & \hline \text { 10.2.2.4 } \\ & \text { 11.2.4 } \\ & \hline \end{aligned}$ | 4.2.5 | Q (U) control | P |
| $\begin{aligned} & \hline 10.2 .2 .4 \\ & 11.2 .4 \end{aligned}$ | 4.2.6 | Q (P) Control | P |
| $\begin{array}{\|l\|} \hline \text { 10.2.2.4 } \\ \text { 11.2.4 } \\ \hline \end{array}$ | 4.2.7 | Reactive Power Q with voltage Limitation Function. | N/A |
| -- | 4.3 | System Perturbations | P |
| -- | 4.3.1 | General procedures | P |
| $\begin{array}{\|l\|} \hline 5.4 .2 \\ 11.2 .2 .1 \\ \hline \end{array}$ | 4.3.2 | Switching operations | P |
| $\begin{array}{\|l\|} \hline 5.4 .3 \\ 11.2 .2 .2 \\ \hline \end{array}$ | 4.3.3 | Flickers | P |
| $\begin{array}{\|l} \hline 5.4 .4 \\ 11.2 .2 .3 \end{array}$ | 4.3.4 | Harmonics | P |
| $\begin{array}{\|l\|} \hline \text { 5.4.6 } \\ \text { 11.2.2.5 } \\ \hline \end{array}$ | 4.3.5 | Unbalances of the current | P |
| 10.3 .3 .1 <br> 10.3.3.2 <br> 10.3.3.3 <br> 10.3.4.2.2 <br> 11.2.10 | 4.4 | PGU disconnection from the grid | P |
| -- | 4.5 | Verification of connection conditions | P |
| $\begin{aligned} & \hline 10.4 .1 \\ & 11.2 .11 \end{aligned}$ | 4.5.1 | Connection without previous protection trigger | P |
| $\begin{array}{\|l\|} \hline 10.4 .2 \\ 11.2 .11 \\ \hline \end{array}$ | 4.5.2 | Connection after triggering of the uncoupling protection | P |
| $\begin{array}{\|l\|} \hline 10.2 .3 \\ 11.2 .5 \\ \hline \end{array}$ | 4.6 | Response during grid faults (FRT) | P (*) |


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| :---: | :---: | :---: |
|  | FGW-TG3+SP1 |  |


| $\begin{aligned} & \text { VDE-AR- } \\ & \text { N } 4110 \\ & \text { SECTION } \end{aligned}$ | FGW TG3 SECTION | CHAPTER OF THE STANDARD | RESULT |
| :---: | :---: | :---: | :---: |
|  |  | FGW-TG3 |  |
| $\begin{aligned} & \text { 10.2.1.2 } \\ & \text { 11.2.3 } \end{aligned}$ | 4.7 | Verification of the working range with regard to voltage and frequency | P |

Note: The declaration of conformity has been evaluated taking into account the IEC Guide 115.
(*) Results are shown in Atachment I (Report No. 2219 / 0163 - A Attachment I). That Attachment must be considered together with this report

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| :---: | :---: | :---: |
| FGW-TG3+SP1 |  |

## 4 TEST RESULTS

### 4.1 ACTIVE POWER OUTPUT

### 4.1.1 Active power peaks

The aim of the test is to determine the maximum active power peaks from different averaging intervals.
The active power in the output will be measured in function of the DC input voltage applied. In this way, the DC input voltage is increased in steps, or continuously, from the minimum value of the MPPT range up until the EUT limits active power or the maximum value of the MPPT is reached. This method applies not only for PV, but also for Storage equipment.
The point of maximum active power is adopted at least twice.
The reactive power setpoint prior to the test was set to $Q=0$, and was maintained during the whole test.
The test has been performed following the testing method detailed in the point 4.1.1 of the reference standard, maximum values of injected active power by the EUT for averaging times of $0.2 \mathrm{~s} ; 60 \mathrm{~s}$ and 600 s .

Used settings of the measurement device for this active power peaks testing.

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| PA3000 | $2020 / 8 / 17$ | 100 ms values | 10 kHz |

Test results are offered in the following table:

| DC Voltage <br> $(V)$ | Active power peaks (W) |  |  | Normalized active power <br> peaks (p.u.) |  |  | No. of used 600 seconds <br> records |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathrm{P}_{0.2}$ | $\mathrm{P}_{60}$ | $\mathrm{P}_{600}$ | $\mathrm{P}_{0.2}$ | $\mathrm{P}_{60}$ | $\mathrm{P}_{600}$ |  |
| 230 | 5459 | 5444 | 5441 | 0.165 | 0.165 | 0.165 |  |
| 303 | 9242 | 9224 | 9223 | 0.280 | 0.280 | 0.279 |  |
| 376 | 14214 | 14198 | 14196 | 0.431 | 0.430 | 0.430 |  |
| 449 | 20311 | 20258 | 20219 | 0.615 | 0.614 | 0.613 |  |
| 522 | 27538 | 27513 | 27506 | 0.834 | 0.834 | 0.834 |  |
| 595 | 34664 | 34645 | 34641 | 1.050 | 1.050 | 1.050 |  |
| 668 | 36305 | 36278 | 36266 | 1.100 | 1.099 | 1.099 | 10 |
| 741 | 36573 | 36542 | 36540 | 1.108 | 1.107 | 1.107 |  |
| 814 | 36580 | 36559 | 36554 | 1.108 | 1.108 | 1.108 |  |
| 887 | 27838 | 27819 | 27818 | 0.844 | 0.843 | 0.843 |  |
| 960 | 18627 | 18617 | 18615 | 0.564 | 0.564 | 0.564 |  |


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| :---: | :---: | :---: |
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| :---: | :---: | :---: |

### 4.1.2 Operating power limited by grid operator

The aim of the test is to determine how fast (Settling time) and how precisely (setting accuracy) the PGU can follow an active power setpoint input, e.g. from a grid operator. Additionally, the capacity of following a setpoint with a specific gradient is to be tested.

| Interface information |  |
| :---: | :---: |
| Interface used | Solar communication tools, RS485 |
| Interface version used | V250 |
| Other interfaces in the equipment | N/A |
| Name or code of the parameter for active <br> power setting | Active and ON/OFF control |
| If |  |

If the EUT has several different interfaces for defining the setpoint, it has been tested the interface returning the most unfavourable results according to the manufacturer information.

### 4.1.2.1 Active Power setting accuracy

This test has been performed according to the point 4.1.2.2 of the standard.
Test procedure applied consist on active output power reductions in steps of $10 \% \mathrm{Pn}$ from $100 \% \mathrm{Pn}$ to $0 \%$ Pn. During these reduction steps there was no disconnection of the generating unit.
Between each power step, the EUT has a maximum of 1 minute to adjust to the new setpoint. After this, measurements of the setpoint are taken as 1-minute mean values as stated in the image represented below.


The active power and the reactive power have been represented in the positive phase sequence system and as 200 ms means for every setpoint step.

Measurement equipment settings used for this tes are shown in the following table:

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| PA3000 | $2019 / 12 / 2$ | 100 ms values | 10 kHz |


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| :---: | :---: | :---: |
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EUT Settings used for this test are provided in the following table:

| EUT Settings |  |
| :---: | :---: |
| Active Power Ramp Rate <br> $(\% P n / s)$ | 300 |
| Operanting mode | Active power priority |
|  | Active power control |
| Active control modes | Active Power VS Frequency mode |
|  | LVRT mode |
|  | Fixed Reactive power control |
| Reactive power VS Voltage |  |
|  | Reactive power VS Active power |
| Cos Phi |  |

The table below shows measured values:

| Active <br> Power step <br> (\%Pn) | Setpoint value |  | Actual value |  | Deviation |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | (W) | (\%Pn) | (W) | $\mathbf{( \% \mathbf { P } _ { \mathbf { n } } )}$ | (W) | $\left(\% \mathbf{P}_{\mathbf{n}}\right)$ |
| $100 \%$ | 33000 | $100.0 \%$ | 33106 | $100.3 \%$ | 106 | $0.3 \%$ |
| $90 \%$ | 29700 | $90.0 \%$ | 29656 | $89.9 \%$ | -44 | $-0.1 \%$ |
| $80 \%$ | 26400 | $80.0 \%$ | 26312 | $79.7 \%$ | -88 | $-0.3 \%$ |
| $70 \%$ | 23100 | $70.0 \%$ | 22962 | $69.6 \%$ | -138 | $-0.4 \%$ |
| $60 \%$ | 19800 | $60.0 \%$ | 19786 | $60.0 \%$ | -14 | $0.0 \%$ |
| $50 \%$ | 16500 | $50.0 \%$ | 16455 | $49.9 \%$ | -45 | $-0.1 \%$ |
| $40 \%$ | 13200 | $40.0 \%$ | 13163 | $39.9 \%$ | -37 | $-0.1 \%$ |
| $30 \%$ | 9900 | $30.0 \%$ | 9841 | $29.8 \%$ | -59 | $-0.2 \%$ |
| $20 \%$ | 6600 | $20.0 \%$ | 6553 | $19.9 \%$ | -47 | $-0.1 \%$ |
| $10 \%$ | 3300 | $10.0 \%$ | 3331 | $10.1 \%$ | 31 | $0.1 \%$ |
| $0 \%$ | 0 | $0.0 \%$ | -49 | $-0.1 \%$ | -49 | $-0.1 \%$ |


| Maximum active power above the defined setpoint (1-minute mean) | $0.3 \% \mathrm{Pn}$ |
| :--- | :--- |
| Maximum active power below the defined setpoint (1-minute mean) | $-0.4 \% \mathrm{Pn}$ |


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| :---: | :---: | :---: |
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In the following graph, test results are represented after the test has been performed:


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| :---: | :---: | :---: |
|  | FGW-TG3+SP1 |  |

### 4.1.2 2 Active Power settling time and active power gradient.

This test has been performed according to the point 4.1.2.2 of the standard for settling time and active power gradient.

Two tests have been done in order to determine both the maximum and the minimum active power gradient. The evidence for the maximum active power gradient has to be provided by a step from $90 \% \mathrm{P}_{\mathrm{n}}$ to $P_{\min }$, whereas, for the minimum active power gradient, this step has to be from $70 \% \mathrm{P}_{\mathrm{n}}$ to $50 \% \mathrm{P}_{\mathrm{n}}$. Settling time and gradient measurements have been taken in the range of $65 \% \mathrm{P}_{\mathrm{n}}$ and $55 \% \mathrm{P}_{\mathrm{n}}$.

Both tests have been repeated testing these steps in the opposite direction.
The settling times for the maximum active power gradients have been measured taking into account the tolerance band of $\pm 5 \% P_{n}$ as shown in the following image:


The active power and the reactive power have been represented in the positive phase sequence system and as 200 ms means for every setpoint step.

Used settings of the measurement device for Active Power settling time test.

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| PA3000 | $2019 / 12 / 2$ | 100 ms values | 10 kHz |


| EUT Settings |  |
| :---: | :---: |
| Maximum Active Power <br> Gradient (\%Pn/s) | 0.66 |
| Minimum Active Power <br> Gradient (\%Pn/s) | 0.33 |
| Operanting mode | Active power priority |
| Active power control |  |
| Active control modes | Active Power VS Frequency mode <br> LVRT mode <br> Reactive power control <br> Reactive power VS Voltage <br> Reactive power VS Active power <br> Cos Phi |


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| :---: | :---: | :---: |
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The table below shows measured values:

| Test at maximum power gradient |  |  |
| :---: | :---: | :---: |
| Active Power step <br> (Setpoint) | Settling time measured (s) | Gradient measured (\%Pn/s) |
| $100.0 \%$ to 0\% Pn | 140.9 | 0.674 |
| $0 \%$ to $100.0 \%$ Pn | 141.4 | 0.672 |
| $90.0 \%$ to $10.0 \%$ Pn | 111.4 | 0.673 |
| $10.0 \%$ to $90.0 \%$ Pn | 111.9 | 0.670 |
| Note: $10 \%$ has been used as Pmin for testing purposes (Type 2 PGU). Pmin that can be configured is <br> $0 \%$ Pn. |  |  |
| Stated in the standard: The evidence for the maximum active power gradient has to be provided by a <br> step of the active power setpoint from P0 = 90\% Pn to Pmin, i.e. the minimum technical power or to <br> $10 \%$ Pn (for other Type 2 systems). |  |  |


| Test at minimum power gradient |  |  |
| :---: | :---: | :---: |
| Active Power step <br> (Setpoint) | Settling time measured (s) | Gradient measured (\%Pn/s) |
| $100.0 \%$ to $0 \% \mathrm{Pn}$ | 280.9 | 0.338 |
| $0 \%$ to $100.0 \% \mathrm{Pn}$ | 285.7 | 0.333 |
| $70.0 \%$ to $50.0 \% \mathrm{Pn}$ | 44.6 | 0.336 |
| $50.0 \%$ to $70.0 \% \mathrm{Pn}$ | 45.1 | 0.333 |
| Note: $10 \%$ has been used as Pmin for testing purposes (Type 2 PGU). Pmin that can be configured is <br> $0 \%$ Pn <br> Stated in the standard: The evidence for the maximum active power gradient has to be provided by a <br> step of the active power setpoint from P0 = 90\% Pn to Pmin, i.e. the minimum technical power or to <br> $10 \%$ Pn (for other Type 2 systems). |  |  |

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The following charts shows the gradient and the settling time:


Test at maximum power gradient Output power reduction ( $90 \%$ to $10 \%$ of Pn ) and Output power increase ( $10 \%$ to $90 \%$ of Pn)


## Test at minimum power gradient

 Output power reduction ( $100 \%$ to $0 \%$ of Pn ) and Output power increase ( $0 \%$ to $100 \%$ of Pn )

## Test at minimum power gradient

 Output power reduction ( $70 \%$ to $50 \%$ of Pn ) and Output power increase ( $50 \%$ to $70 \%$ of Pn )

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| :---: | :---: | :---: |

### 4.1.3 Active Power feed-in as a function of grid frequency

The aim of the test is to demonstrate the response of the EUT due to a deviation in grid frequency from rated value in terms of speed (rise/settling time) and the active power gradient.

This test has been performed according to the point 4.1.3.1 of the standard, changing the parameters in the PGU control system. The following figure has been performed.

Two tests have been done for both over and underfrequency tests:

- Overfrequency test (LFSM-O): According to chapter 4.1.3.1.a).
- Underfrequency test (LFSM-U): According to chapter 4.1.3.1.b).

| Testing Method Used (LFSM-O \& LFSM-U) |  | Comments |
| :--- | :---: | :--- |
| Changing parameters in the <br> PGU control system | $\square$ |  |
| Signal input to control system | $\square$ |  |
| Grid simulator | $\boxtimes$ | By changing the grid simulator's frequency by <br> setpoint and measuring the unit output. |
| Alternative procedures | $\square$ |  |

### 4.1.3.1 Overfrequency (LFSM-O)

For this test, power reduction has been applied with a gradient of $-40 \% \mathrm{Pref} / \mathrm{Hz}$ in the range of 50.2 Hz to 51.5 Hz . Once the grid frequency falls below the 50.2 Hz threshold, the active power recuperation must be with a maximum gradient of $10 \% \mathrm{P}_{\mathrm{n}} / \mathrm{min}$.

For the test, at the beginning, active power was set over 100\%Pn and, before the power reduction started, active power was reduced to a $50 \%$ Pn through a setpoint.
Frequency values must be inside next ranges (referred to the points on the figure):


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| :---: | :---: | :---: |
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| Frequency <br> Step | Simulated grid frequencies | Note |
| :---: | :---: | :--- |
| 1 | $50.00 \mathrm{~Hz} \pm 0.05 \mathrm{~Hz}$ |  |
| 2 | $50.30 \mathrm{~Hz} \pm 0.05 \mathrm{~Hz}$ |  |
| 3 | $51.40 \mathrm{~Hz} \pm 0.05 \mathrm{~Hz}$ | Verification of adherence to characteristic |
| 4 | $50.30 \mathrm{~Hz} \pm 0.05 \mathrm{~Hz}$ |  |
| 5 | $50.00 \mathrm{~Hz} \pm 0.05 \mathrm{~Hz}$ | Power increase to the maximum possible active power <br> with a maximum gradient $\mathrm{P}(\mathrm{t})$ of $10 \% \mathrm{Pn} / \mathrm{min}$ |

60s after reaching point 5 , the power reduction applied at the beginning of the test is disabled in order to verify the recuperation gradient limit of $10 \% \mathrm{Pn} / \mathrm{min}$.

Starting at $P_{\text {ref, }}$ it has been performed the frequency steps that can be seen on the table above, taking measures of the active power at every set point of frequency. Every point has a measured duration of 30 seconds at least.

Gradient has been calculated as follows:

$$
\frac{\Delta P}{\Delta f}=\frac{P_{\text {Step } i+1}-P_{\text {Step } i}}{\left|f_{\text {Step } i+1}-f_{\text {Step } i}\right|}
$$

| PStep $i+1$ | 10-s-mean of the active power which is calculated at the end of frequency step $i+1$. |
| :--- | :--- |
| $P_{\text {Step } i}$ | 10-s-mean of the active power which is calculated at the end of frequency step $i$. |
| $f_{\text {Step } i+1}$ | $10-s-m e a n$ of the grid frequency, at which PStep $i+1$ is determined. |
| $\mathrm{f}_{\text {Step } i}$ | $10-\mathrm{s}$-mean of the grid frequency, at which PStep $i$ is determined. |

To determine the rise and settling times, a tolerance band of $\pm 5 \%$ of Pn is applied around the controlled active power end value.

Used settings of the measurement device for this power limitation for an increase in grid frequency testing.

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| PA3000 | $2019 / 12 / 2$ | 100 ms values | 10 kHz |

The tables below show measured values:
a) Accuracy results - test at $\mathbf{1 0 0 \% P n}$

| Step |  | $\begin{array}{c}\text { Simulated } \\ \text { grid frequency } \\ \text { (Hz) }\end{array}$ | $\begin{array}{c}\text { Measured } \\ \text { grid } \\ \text { frequency } \\ \text { (Hz) }\end{array}$ | $\begin{array}{c}\text { Normalized Active } \\ \text { Power } \\ \text { Setpoint } \\ \text { (P/Pn) }\end{array}$ | $\begin{array}{c}\text { Normalized Active } \\ \text { Power } \\ \text { Measured } \\ \text { (P/Pn) }\end{array}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{array}{c}\text { Active power } \\ \text { gradient P(f) } \\ \text { relative to the } \\ \text { reference }\end{array}$ |  |  |  |  |
| frequency |  |  |  |  |  |  |$]$

(*): As the EUT is Type 2, according to the standard Pmom = Pref is defined as the mean value of the active power immediately prior to frequency transition at 50.2 Hz . Here, the manufacturer specifies the averaging time 100 ms

| $\Delta \mathrm{P} / \Delta \mathrm{f}$ |  |  |
| :---: | :---: | :---: |
| Mean active power gradient while frequency limit is exceeded | $-40.2 \% \mathrm{P}_{\text {ref }} / \mathrm{Hz}$ |  |
| Defined active power gradient $\Delta \mathrm{P} / \Delta \mathrm{f}$ | $-40.0 \% \mathrm{Pref}_{\text {ref }} / \mathrm{Hz}$ |  |

b) Settling time and Rise time results - test at 100\%Pn

| Frequency step | Rise Time (s) | Settling time (s) |
| :---: | :---: | :---: |
| Step 2 $\rightarrow$ Step 3 | 0.2 | 0.2 |
| Step 3 $\rightarrow$ Step 4 | 0.5 | 0.5 |

c) Accuracy results - test at 50\%Pn

| LSFM-O |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Step | Simulated grid frequency (Hz) | Measured grid frequency (Hz) | Normalized Active Power Setpoint (P/Pn) | Normalized Active Power Measured (P/Pn) |  | Active power gradient $\mathbf{P ( f )}$ relative to the reference frequency |
|  |  |  |  | Whole step | $\mathbf{P}_{10}$ |  |
| 1 | $50.00 \pm 0.01$ | 50.00 | 0.500 | 0.501 | 0.502 | ------- |
| (*) | 50.20 to 50.30 | 50.20 | 0.500 | 0.501 | 0.502 | ------- |
| 2 | $50.30 \pm 0.05$ | 50.30 | 0.480 | 0.483 | 0.482 | ------- |
| 3 | $51.40 \pm 0.05$ | 51.40 | 0.260 | 0.262 | 0.262 | -40.1\% Pref/ Hz |
| 4 | $50.30 \pm 0.05$ | 50.30 | 0.480 | 0.482 | 0.482 | -40.0\% $\mathrm{Pref}^{\text {/ }} \mathrm{Hz}$ |
| 5 | $50.00 \pm 0.05$ | 50.00 | 1.000 | 1.001 | 1.001 | ------- |

$\left(^{*}\right)$ : As the EUT is Type 2, according to the standard Pmom = Pref is defined as the mean value of the active power immediately prior to frequency transition at 50.2 Hz . Here, the manufacturer specifies the averaging time 100 ms

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| :---: | :---: | :---: |


| $\Delta \mathbf{P} / \Delta \mathbf{f}$ |  |  |
| :---: | :---: | :---: |
| Mean active power gradient while frequency limit is exceeded | $-40.1 \% \mathrm{Pref} / \mathrm{Hz}$ |  |
| Defined active power gradient $\Delta \mathbf{P} / \Delta \mathbf{f}$ | $-40.0 \% \mathrm{P}_{\mathrm{ref}} / \mathrm{Hz}$ |  |

d) Settling time and Rise time results - test at 50\%Pn

| Frequency step | Rise Time (s) | Settling time (s) |
| :---: | :---: | :---: |
| Step 2 $\rightarrow$ Step 3 | 0.2 | 0.2 |
| Step 3 $\rightarrow$ Step 4 | 0.2 | 0.2 |

e) Output power increase - test at 50\%Pn

| $\Delta P / \Delta t$ |  |
| :---: | :---: |
| Maximum active power gradient | 8.97\% Pn/min |
| Mean active power gradient | 8.97\% Pn/min |
| Defined gradient $\Delta \mathrm{P} / \Delta \mathrm{t}$ | 10.0\% Pn/min |
| The gradient of active power after removal of the active power limitation has been measured as follows: |  |
| The active power has to be calculated as a 0.2 second mean. |  |
| The mean 1-minute power is determined at intervals of 1 min . |  |
| The first averaging interval starts 1 min prior to the removal of the active power limitation. The last averaging interval ends after reaching the stationary final value of active power. |  |
| The gradient of the active power increase $\Delta \mathrm{P} / \Delta \mathrm{t}$ is determined from the difference between consecutive |  |
| 1-minute mean values with reference to 1 min in each case for the time point at the boundary between two averaging intervals. |  |

In following graphs, test results are represented:






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| :---: | :---: | :---: |
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### 4.1.3.2 Underfrequency (LSFM-U)

For this test, power increase has been applied with a gradient of $40 \% \mathrm{P}_{\mathrm{ref}} / \mathrm{Hz}$ in the range of 49.8 Hz to 47.5 Hz . Once the grid frequency falls below the 49.8 Hz threshold, the active power recuperation must be with a maximum gradient of $10 \% \mathrm{P}_{\mathrm{n}} / \mathrm{min}$.

For the test, before the power reduction starts, active power has been reduced to a $10 \% \mathrm{Pn}$ through a setpoint.

Frequency values must be inside next ranges (referred to the points on the figure):


| Frequency <br> Step | Simulated grid frequencies | Note |
| :---: | :---: | :--- |
| 1 | $50.00 \mathrm{~Hz} \pm 0.05 \mathrm{~Hz}$ |  |
| 2 | $49.70 \mathrm{~Hz} \pm 0.05 \mathrm{~Hz}$ |  |
| 3 | $3.1: 47.60 \mathrm{~Hz} \pm 0.05 \mathrm{~Hz}$ |  |
| 4 | $4.1: 48.70 \mathrm{~Hz} \pm 0.05 \mathrm{~Hz}$ |  |
| 5 | $49.70 \mathrm{~Hz} \pm 0.05 \mathrm{~Hz}$ |  |
| 6 | $50.00 \mathrm{~Hz} \pm 0.05 \mathrm{~Hz}$ | Charge of active power with a maximum gradient of |
| $10 \% \mathrm{Pn} / \mathrm{min}$ |  |  |

60s after reaching point 5, the power reduction applied at the beginning of the test is disabled in order to verify the recuperation gradient limit of $10 \% \mathrm{Pn} / \mathrm{min}$

Starting at $P_{\text {ref, }}$ it has been performed the frequency steps that can be seen on the table above, taking measures of the active power at every set point of frequency. Every point has a measured duration of 30 seconds at least.

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| :---: | :---: | :---: |

Gradient has been calculated as follows:

$$
\frac{\Delta P}{\Delta f}=\frac{P_{\text {Step } i+1}-P_{\text {Step } i}}{\left|f_{\text {Step } i+1}-f_{\text {Step } i}\right|}
$$

| PStep $i+1$ | 10-s-mean of the active power which is calculated at the end of frequency step $i+1$. |
| :--- | :--- |
| $P_{\text {Step } i}$ | $10-s$-mean of the active power which is calculated at the end of frequency step $i$. |
| $\mathrm{f}_{\text {Step } i+1}$ | 10-s-mean of the grid frequency, at which PStep $\mathrm{i}+1$ is determined. |
| $\mathrm{f}_{\text {Step } i}$ | $10-\mathrm{s}$-mean of the grid frequency, at which PStep $i$ is determined. |

To determine the rise and settling times, a tolerance band of $\pm 5 \%$ of Pn is applied around the controlled active power end value.

Used settings of the measurement device for this power limitation for an increase in grid frequency testing.

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| PA3000 | $2019 / 12 / 2$ | 100 ms values | 10 kHz |

The tables below show measured values:
a) Accuracy results - test at $50 \% \mathrm{Pn}$

| LSFM-U |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Step | Simulated grid frequency (Hz) | Measured grid frequency (Hz) | Normalized Active Power Setpoint (P/Pn) | Normalized Active Power Measured (P/Pn) |  | Active power gradient $\mathbf{P ( f )}$ relative to the reference frequency |
|  |  |  |  | Whole step | $\mathrm{P}_{10}$ |  |
| 1 | $50.00 \pm 0.05$ | 50.00 | 0.500 | 0.501 | 0.501 | ------- |
| (*) | 50.00 to 49.70 | 49.80 | 0.500 | 0.501 | 0.501 | ------- |
| 2 | $49.70 \pm 0.05$ | 49.70 | 0.540 | 0.543 | 0.543 | ------- |
| 3 | $47.60 \pm 0.05$ | 47.60 | 1.000 | 1.001 | 1.002 | 43.7\% Pref/Hz |
| 4 | $48.70 \pm 0.05$ | 48.70 | 0.760 | 0.760 | 0.760 | 43.9\% Pref/Hz |
| 5 | $49.70 \pm 0.05$ | 49.70 | 0.540 | 0.544 | 0.543 | 43.1\% Pref/Hz |
| 6 | $50.00 \pm 0.05$ | 50.00 | 1.000 | 1.001 | 1.001 | ------- |

(*): As the EUT is Type 2, according to the standard Pmom = Pref is defined as the mean value of the active power immediately prior to frequency transition at 48.8 Hz . Here, the manufacturer specifies the averaging time 100 ms

| $\Delta \mathbf{P} / \Delta \mathbf{f}$ |  |
| :---: | :---: |
| Mean active power gradient while frequency limit is exceeded | $43.8 \%$ Pref $/ \mathrm{Hz}$ |
| Defined active power gradient $\Delta \mathbf{P} / \Delta \mathbf{f}$ | $40.0 \% \mathrm{Pref} / \mathrm{Hz}$ |

b) Settling time and Rise time results - test at 50\%Pn

| Frequency step | Rise Time (s) | Settling time (s) |
| :---: | :---: | :---: |
| Step 2 $\rightarrow$ Step 3 | 0.4 | 0.4 |
| Step 3 $\rightarrow$ Step 4 | 0.2 | 0.2 |
| Step 4 $\rightarrow$ Step 5 | 0.2 | 0.2 |


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| :---: | :---: | :---: |

c) Accuracy results - test at $25 \% \mathrm{Pn}$

| LSFM-U |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Step | Simulated grid frequency (Hz) | Measured grid frequency (Hz) | Normalized Active Power Setpoint (P/Pn) | Normalized Active Power Measured (P/Pn) |  | Active power gradient $\mathbf{P ( f )}$ relative to the reference frequency |
|  |  |  |  | Whole step | $\mathbf{P}_{10}$ |  |
| 1 | $50.00 \pm 0.05$ | 50.00 | 0.250 | 0.250 | 0.251 | ------- |
| (*) | 50.00 to 49.80 | 49.80 | 0.250 | 0.250 | 0.251 | ------- |
| 2 | $49.70 \pm 0.05$ | 49.70 | 0.290 | 0.291 | 0.292 | 40.1 Pref/ Hz |
| 3 | $47.60 \pm 0.05$ | 47.60 | 1.000 | 1.001 | 1.001 | 33.8 Pref/Hz (**) |
| 4 | $48.70 \pm 0.05$ | 48.70 | 0.690 | 0.690 | 0.690 | 28.3 Pref/Hz (**) |
| 5 | $49.70 \pm 0.05$ | 49.70 | 0.290 | 0.292 | 0.292 | 39.9 Pref/Hz |
| 6 | $50.00 \pm 0.05$ | 50.00 | 1.000 | 1.001 | 1.001 | ------- |

(*): As the EUT is Type 2, according to the standard Pmom = Pref is defined as the mean value of the active power immediately prior to frequency transition at 48.8 Hz . Here, the manufacturer specifies the averaging time 100 ms
$\left(^{* *}\right)$ : Setting active power gradient $P(f)$ is $40 \% \mathrm{Pn} / \mathrm{Hz}$, when test $\mathrm{P}_{\mathrm{M}}=25 \% \mathrm{Pn}$, it will be rise $100 \% \mathrm{Pn}$ at 47.92 Hz , when the frequency is below 47.92 Hz , It will be lock at $100 \%$ Pn output.

| $\Delta \mathbf{P} / \Delta \mathbf{f}$ |  |
| :---: | :---: |
| Mean active power gradient while frequency limit is exceeded | $40.0 \% \mathrm{P}_{\mathrm{ref}} / \mathrm{Hz}$ |
| Defined active power gradient $\mathbf{\Delta P} / \Delta \mathbf{f}$ | $40.0 \% \mathrm{P}_{\mathrm{ref}} / \mathrm{Hz}$ |

d) Settling time and Rise time results - test at 25\%Pn

| Frequency step | Rise Time (s) | Settling time (s) |
| :---: | :---: | :---: |
| Step 2 $\rightarrow$ Step 3 | 0.3 | 0.3 |
| Step 3 $\rightarrow$ Step 4 | 0.2 | 0.2 |
| Step 4 $\rightarrow$ Step 5 | 0.2 | 0.2 |


| $\Delta \mathbf{M P / \Delta t}$ |  |
| :--- | ---: |
| Maximum active power gradient |  |
| Defined gradient $\Delta P / \Delta t$ |  |
| The gradient of active power after removal of the active power limitation has been measured as follows: |  |
| The active power has to be calculated as a 0.2 second mean. |  |
| The mean 1-minute power is determined at intervals of 1 min. |  |
| The first averaging interval starts 1 min prior to the removal of the active power limitation. The last |  |
| averaging interval ends after reaching the stationary final value of active power. |  |
| The gradient of the active power increase $\Delta \mathrm{P} / \Delta \mathrm{t}$ is determined from the difference between consecutive |  |
| 1-minute mean values with reference to 1 min in each case for the time point at the boundary between |  |
| two averaging intervals. |  |

In following graphs, test results are represented after the test has been performed:
Output power increase: Active power and Frequency over time_test at 50\%Pn




Power gradient (Step 4 to Step 5) _test at 50\%Pn


Output power increase: Active power over Frequency_test at 50\%Pn





Power gradient (Step 4 to Step 5) _test at 25\%Pn


Output power increase: Active power over Frequency_test at 25\%Pn


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| :---: | :---: | :---: |

### 4.1.4 Active Power gradient following disconnection from the grid

The aim of this test is to measure the PGU's active power gradient when restarting following disconnection from the grid.

The test was performed according to the point 4.1.4 of the standard. By the following graph, it is represented the test to be done:


In the example tested, the inverter was adjusted to be disconnected from the grid when the output voltage is lower than $75 \%$ of the rated voltage in less than 100 ms .

After this, the inverter was set to be reconnected when the voltage grid is recovered over $75 \%$ of the rated voltage for more than 70 seconds and not exceeding more than 75 seconds.

Once reconnected, the inverter shall start to inject active power into the grid following a soft ramp according to requirements stated in VDE AR-N $4110: 2018$ (19.8\%Pn/min - 39.6\%Pn/min). For the tested case, the active power gradient was set to follow a ramp rate corresponding to $30 \% \mathrm{Pn} / \mathrm{min}$.

Active output power and output voltage have been represented as 0.1 seconds mean as shown in the graphs below.

Used settings of the measurement device for the active power gradient testing.

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| PA3000 | $2020 / 6 / 24$ | 100 ms values | 10 kHz |


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| :---: | :---: | :---: |
|  | FGW-TG3+SP1 |  |

By the following graph, test results are represented after the test has been performed:


As it can be seen in the graph above, the active power gradient has been done according with option 2 of FGW Rev. 25 as seen in the picture below:


NOTE: It is desirable that the active power increases as a ramp. In case this cannot be implemented due to the design, an active power step in the beginning of connection is permitted (max. to $20 \% P_{n}$ ).

Fig. 4-10: Example with the first averaging interval 90 s before power increase
Gradients are calculated using averaging periods of 60 seconds starting at -90 seconds before the connection starts.

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| :---: | :---: | :---: |

For each one of this averaging periods, the active power gradient is calculated according to the following equation:

$$
\frac{\Delta p}{1 \min }=\frac{P_{t=t 1+1 \min }-P_{t=t 1}}{1 \min }
$$

Here t1 is the time commencing the generator active power feed in after reconnection until the end of power limitation.

For the example tested, they have been calculated up to 5 averaging periods as represented in the image below:


In the following table, they are summarized all active power gradients calculated. They are as well calculated the maximum and the mean active power gradients take in to account all power gradients determined

| Active power gradient determined for the averaging period 0 | $0.0 \% \mathrm{P}_{\mathrm{n}} / \mathrm{min}$ |
| :---: | :---: |
| Active power gradient determined for the averaging period 1 | $13.3 \% \mathrm{P}_{\mathrm{n}} / \mathrm{min}$ |
| Active power gradient determined for the averaging period 2 | $30.1 \% \mathrm{P}_{\mathrm{n}} / \mathrm{min}$ |
| Active power gradient determined for the averaging period 3 | $30.1 \% \mathrm{P}_{\mathrm{n}} / \mathrm{min}$ |
| Active power gradient determined for the averaging period 4 | $24.4 \% \mathrm{P}_{\mathrm{n}} / \mathrm{min}$ |
| Maximum active power gradient | $30.1 \% \mathrm{P}_{\mathrm{n}} / \mathrm{min}$ |
| Mean active power gradient (averaging periods 0 to 4) | $19.6 \% \mathrm{P}_{\mathrm{n}} / \mathrm{min}$ |
| Mean active power gradient (averaging periods 2 to 3) | $30.1 \% \mathrm{P}_{\mathrm{n}} / \mathrm{min}$ |
| Defined gradient DP/Dt | $30 \% \mathrm{P}_{\mathrm{n}} / \mathrm{min}$ |


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| :---: | :---: | :---: |

### 4.2 REACTIVE POWER PROVISION

### 4.2.1 Reactive Power response in the normal operating mode and Maximum Reactive Power

Aims of these tests are to determine the PGU's active and reactive power response in normal operating mode for a specified setpoint of $Q=0$ and the maximum capacitive (overexcited) and inductive (underexcited) reactive power provision of the EUT.

For all tests, the active power of the inverter must vary from $0 \%$ to $100 \%$. This variation must be done such as 3 steps of each $10 \%$ Pn increasing range are taken. Each step was maintained for at least 1 minute, taken for the calculations 1-minute displacement factor $\cos \varphi$, voltage and reactive power mean.

Five different tests have been performed:

- According to the point 4.2.1 of the standard, the first test has been performed with a specified setpoint $\mathrm{Q}=0 \mathrm{kVAr}$ in normal operating mode.
- According to the point 4.2.2 of the standard, the second test has been performed in order to determine the maximum capacitive (overexcited) and inductive (underexcited) reactive power provision of the PGU (PQ diagram). In this test the apparent power, S, has been kept at 100\%Sn.
- In addition to point 4.2.2, it has been done a rectangular curve to prove that the inverter is capable of providing a fixed amount of reactive power at any active power level.
The reactive power value has been set at $48.43 \% \mathrm{Pn}$ (inductive and capacitive).
- In addition to point 4.2.2, it has been done a triangular curve to prove that the inverter is capable of providing a fixed amount of reactive power in relation to its power factor.
Power factor value has been set at 0.90 (inductive and capacitive)
- According to the point 4.2.3 of the standard, the fifth test has been performed in order to verify the maximum capacitive (overexcited) and inductive (underexcited) recative power provision of the PGU with under/over voltage situations (voltage-dependent PQ diagram)
This capability has been verified at $90 \%$ Un as well as $110 \%$ Un
The maximum steady-state error between the desired and actual value in the range $P \geq 0.10$ p.u. will be $\pm 2 \%$. It will be allowed $\pm 4 \%$ for equipments with capacity below 300 kVA .

Below a power of 0.10 p.u, an underexcited operation in the amount of up to $5 \%$ will be permitted. While for overexcited, the maximum deviation allowed will be a maximum of $2 \%$.

The positive phase sequence values of the active and reactive power, as well as the displace-ment factor, have been determined from each measured record.

In following points are offered all test results after tests above detailed.

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| :---: | :---: | :---: |
|  | FGW-TG3+SP1 |  |


| Interface information |  |
| :---: | :---: |
| Interface used | Solar communication tools, RS485 |
| Interface version used | V250 |
| Other interfaces in the equipment | N/A |
| Name or code of the parameter for active <br> power setting | Active and ON/OFF control |
| Name or code of the parameter for reactive |  |
| power setting |  |$\quad$ Reactive parameters

EUT Settings used for these tests are provided in the following table:

| EUT Settings |  |
| :---: | :---: |
| Operanting mode | Active power priority |
|  | Active power control |
|  | Active Power VS Frequency mode |
| Active control modes | LVRT mode |
|  | Reactive power control |
|  | Reactive power VS Voltage |
|  | Reactive power VS Active power |
|  | Cos Phi |


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| :---: | :---: | :---: |
| FGW-TG3+SP1 |  |

### 4.2.1.1 Reactive Power Fixed $(Q=0)$

Used settings of the measurement device for Normal operating mode (Q=OkVAr).

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| PA3000 | $2019 / 12 / 03$ | 100 ms values | 10 kHz |

The table below shows measured values for each power step tested:

| Reactive Power Fixed: Q = 0 kVAr |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P Desired <br> (\%Pn) | P measured <br> $(\mathbf{k W})$ | Q measured <br> $(\mathbf{k V A r})$ | Q Deviation <br> $(\mathbf{k V A r})$ | Power Factor <br> $(\mathbf{c o s} \boldsymbol{\varphi})$ | $\mathbf{V}_{\text {AC + (V) }}$ | Number of <br> records |
| $\mathbf{0 \%}$ | -0.051 | 0.331 | 0.331 | -0.152 | 229.825 | 1 |
| $\mathbf{1 0 \%}$ | 3.295 | 0.316 | 0.316 | 0.995 | 230.063 | 1 |
| $\mathbf{2 0 \%}$ | 6.617 | 0.292 | 0.292 | 0.999 | 230.174 | 1 |
| $\mathbf{3 0 \%}$ | 9.938 | 0.352 | 0.352 | 0.999 | 230.280 | 1 |
| $\mathbf{4 0 \%}$ | 13.227 | 0.425 | 0.425 | 0.999 | 230.306 | 1 |
| $\mathbf{5 0 \%}$ | 16.555 | 0.504 | 0.504 | 1.000 | 230.384 | $\mathbf{1}$ |
| $\mathbf{6 0 \%}$ | 19.856 | 0.598 | 0.598 | 1.000 | 230.469 | $\mathbf{1}$ |
| $\mathbf{7 0 \%}$ | 23.169 | 0.712 | 0.712 | 1.000 | 230.593 | $\mathbf{1}$ |
| $\mathbf{8 0 \%}$ | 26.516 | 0.846 | 0.846 | 0.999 | 230.703 | 1 |
| $\mathbf{9 0 \%}$ | 29.788 | 0.979 | 0.979 | 0.999 | 230.804 | 1 |
| $\mathbf{1 0 0 \%}$ | 33.098 | 1.034 | 1.034 | 1.000 | 230.928 | $\mathbf{1}$ |

In following graphs, test results are represented after the test has been performed:


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| :---: | :---: | :---: |
| FGW-TG3+SP1 |  |

### 4.2.1.2 Semicircular Curve: Maximum Apparent Power

Used settings of the measurement device for this semicircular curve testing.

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| PA3000 | $2019 / 12 / 06$ | 100 ms values | 10 kHz |

Tables below show measured values for each power step tested, at both the inductive and the capacitive sides:

| Semicircular Curve (U = 100\% Un) - Inductive |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{P}$ <br> Desired <br> (\%Pn) | P <br> measured <br> (kW) | Q <br> measured <br> (kVAr) | S <br> measured <br> (kVA) | S <br> deviation <br> (kVA) | Power Factor <br> (cos $\boldsymbol{\varphi})$ | $\mathbf{V A C}_{\text {AC (V) }}$ | Number of <br> records |
| $\mathbf{0 \%}$ | -0.073 | 0.516 | 0.521 | 35.779 | -0.141 | 228.890 | 1 |
| $\mathbf{1 0 \%}$ | 3.318 | 16.488 | 16.819 | 19.481 | 0.197 | 229.295 | 1 |
| $\mathbf{2 0 \%}$ | 6.642 | 16.073 | 17.392 | 18.908 | 0.382 | 229.405 | 1 |
| $\mathbf{3 0 \%}$ | 9.978 | 16.021 | 18.874 | 17.426 | 0.529 | 229.672 | 1 |
| $\mathbf{4 0 \%}$ | 13.265 | 15.998 | 20.782 | 15.518 | 0.638 | 229.849 | 1 |
| $\mathbf{5 0 \%}$ | 16.572 | 15.975 | 23.018 | 13.282 | 0.720 | 230.018 | 1 |
| $\mathbf{6 0 \%}$ | 19.818 | 15.958 | 25.445 | 10.855 | 0.779 | 230.129 | 1 |
| $\mathbf{7 0 \%}$ | 23.137 | 15.964 | 28.110 | 8.190 | 0.823 | 230.307 | 1 |
| $\mathbf{8 0 \%}$ | 26.443 | 15.979 | 30.896 | 5.404 | 0.856 | 230.487 | 1 |
| $\mathbf{9 0 \%}$ | 29.696 | 16.009 | 33.737 | 2.563 | 0.880 | 230.672 | 1 |
| $\mathbf{1 0 0 \%}$ | 33.011 | 16.066 | 36.714 | -0.414 | 0.899 | 230.867 | 1 |
| $\mathbf{1 0 2 \%}$ | 33.665 | 14.033 | 36.473 | -0.173 | 0.923 | 230.886 | 1 |
| $\mathbf{1 0 4 \%}$ | 34.353 | 11.842 | 36.337 | -0.037 | 0.945 | 230.421 | 1 |
| $\mathbf{1 0 6 \%}$ | 35.133 | 9.654 | 36.436 | -0.136 | 0.964 | 230.434 | 1 |
| $\mathbf{1 0 8 \%}$ | 35.714 | 7.655 | 36.525 | -0.225 | 0.978 | 230.444 | 1 |
| $\mathbf{1 1 0 \%}$ | 36.053 | 6.019 | 36.552 | -0.252 | 0.986 | 230.461 | $\mathbf{1}$ |


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| :---: | :---: | :---: |

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| Semicircular Curve (U = 100\% Un) - Capacitive |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{P}$ <br> Desired <br> (\%Pn) | $\mathbf{P}$ <br> measured <br> (kW) | Q <br> measured <br> (kVAr) | S <br> measured <br> (kVA) | $\mathbf{S}$ <br> deviation <br> (kVA) | Power Factor <br> (cos $\boldsymbol{\varphi})$ | $\mathbf{V}_{\text {AC + (V) }}$ | Number of <br> records |
| $\mathbf{0 \%}$ | -0.018 | -0.486 | 0.486 | 35.814 | -0.037 | 228.903 | 1 |
| $\mathbf{1 0 \%}$ | 3.238 | -15.207 | 15.547 | 20.753 | 0.208 | 228.736 | 1 |
| $\mathbf{2 0 \%}$ | 6.613 | -15.709 | 17.045 | 19.255 | 0.388 | 229.094 | 1 |
| $\mathbf{3 0 \%}$ | 9.942 | -15.952 | 18.797 | 17.503 | 0.529 | 229.098 | 1 |
| $\mathbf{4 0 \%}$ | 13.261 | -15.995 | 20.778 | 15.522 | 0.638 | 229.365 | 1 |
| $\mathbf{5 0 \%}$ | 16.565 | -16.032 | 23.052 | 13.248 | 0.719 | 229.537 | $\mathbf{1}$ |
| $\mathbf{6 0 \%}$ | 19.861 | -16.058 | 25.541 | 10.759 | 0.778 | 229.712 | $\mathbf{1}$ |
| $\mathbf{7 0 \%}$ | 23.105 | -16.068 | 28.143 | 8.157 | 0.821 | 229.889 | 1 |
| $\mathbf{8 0 \%}$ | 26.411 | -16.077 | 30.919 | 5.381 | 0.854 | 230.044 | 1 |
| $\mathbf{9 0 \%}$ | 29.739 | -16.122 | 33.828 | 2.472 | 0.879 | 230.277 | 1 |
| $\mathbf{1 0 0 \%}$ | 32.983 | -16.161 | 36.729 | -0.429 | 0.898 | 230.460 | $\mathbf{1}$ |
| $\mathbf{1 0 2 \%}$ | 33.618 | -13.837 | 36.354 | -0.054 | 0.925 | 230.548 | $\mathbf{1}$ |
| $\mathbf{1 0 4 \%}$ | 34.314 | -11.848 | 36.302 | -0.002 | 0.945 | 230.629 | $\mathbf{1}$ |
| $\mathbf{1 0 6 \%}$ | 35.102 | -9.532 | 36.373 | -0.073 | 0.965 | 230.676 | $\mathbf{1}$ |
| $\mathbf{1 0 8 \%}$ | 35.691 | -7.550 | 36.481 | -0.181 | 0.978 | 230.760 | $\mathbf{1}$ |
| $\mathbf{1 1 0 \%}$ | 35.985 | -5.888 | 36.464 | -0.164 | 0.987 | 230.745 | $\mathbf{1}$ |

In following graphs, test results are represented after the test has been performed:


## Semicircular Curve (100\%Un), Capacitive side: Power Factor and Powers over time



Semicircular Curve (100\%Un): Active Power over Reactive Power


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| :---: | :---: | :---: |
| FGW-TG3+SP1 |  |

### 4.2.1.3 Rectangular Curve: Fixed Reactive Power ( $\mathrm{Q}=\mathbf{4 8 . 4 3} \% \mathrm{Pn}$ )

Used settings of the measurement device for this rectangular curve $(Q=48.43 \% \mathrm{Pn})$ testing.

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| PA3000 | $2019 / 12 / 06$ | 100 ms values | 10 kHz |

Tables below show measured values for each power step tested, at both the inductive and the capacitive sides:

| Rectangular Curve (Q=48 \% $\mathrm{P}_{\mathrm{n}}$ ) - Inductive |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { P Desired } \\ & \text { (\%Pn) } \end{aligned}$ | $\begin{gathered} P \\ \text { measured } \\ (k W) \end{gathered}$ | $\begin{gathered} Q \\ \text { measured } \\ (k V A r) \end{gathered}$ | $\begin{gathered} \mathrm{S} \\ \substack{\text { measured } \\ (\mathrm{kVAr})} \end{gathered}$ | Q Deviation (kVAr) | Power Factor $(\cos \varphi)$ | $\mathrm{V}_{\mathrm{AC}}+(\mathrm{V})$ | Number of records |
| 0\% | -0.076 | 0.528 | 0.533 | 15.312 | -0.142 | 229.869 | 1 |
| 10\% | 3.304 | 16.347 | 16.678 | -0.507 | 0.198 | 230.298 | 1 |
| 20\% | 6.611 | 15.990 | 17.302 | -0.150 | 0.382 | 230.408 | 1 |
| 30\% | 9.973 | 15.952 | 18.813 | -0.112 | 0.530 | 230.479 | 1 |
| 40\% | 13.190 | 15.937 | 20.687 | -0.097 | 0.638 | 230.513 | 1 |
| 50\% | 16.490 | 15.917 | 22.919 | -0.077 | 0.719 | 230.647 | 1 |
| 60\% | 19.773 | 15.905 | 25.376 | -0.065 | 0.779 | 230.699 | 1 |
| 70\% | 23.098 | 15.911 | 28.048 | -0.071 | 0.824 | 230.845 | 1 |
| 80\% | 26.398 | 15.919 | 30.827 | -0.079 | 0.856 | 230.890 | 1 |
| 90\% | 29.730 | 15.953 | 33.740 | -0.113 | 0.881 | 231.033 | 1 |
| 100\% | 33.010 | 16.012 | 36.689 | -0.172 | 0.900 | 231.145 | 1 |


| Rectangular Curve (Q=48.43 \% $\mathrm{P}_{\mathrm{n}}$ ) - Capacitive |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { P Desired } \\ & \text { (\%Pn) } \end{aligned}$ | $\begin{gathered} \mathbf{P} \\ \text { measured } \\ (\mathrm{kW}) \end{gathered}$ | $\begin{gathered} \hline \mathbf{Q} \\ \text { measured } \\ (k V A r) \end{gathered}$ | $\begin{gathered} \mathrm{S} \\ \text { measured } \\ (\mathrm{kVAr}) \end{gathered}$ | $\begin{gathered} \mathbf{Q} \\ \text { Deviation } \\ \text { (kVAr) } \end{gathered}$ | Power Factor $(\cos \varphi)$ | $\mathrm{V}_{\mathrm{AC}}+(\mathrm{V})$ | Number of records |
| 0\% | -0.020 | -0.490 | 0.491 | -15.350 | -0.041 | 229.896 | 1 |
| 10\% | 3.293 | -15.486 | 15.833 | -0.354 | 0.208 | 229.774 | 1 |
| 20\% | 6.663 | -15.931 | 17.269 | 0.091 | 0.386 | 229.917 | 1 |
| 30\% | 9.961 | -16.163 | 18.986 | 0.323 | 0.525 | 230.035 | 1 |
| 40\% | 13.356 | -16.204 | 20.998 | 0.364 | 0.636 | 230.016 | 1 |
| 50\% | 16.521 | -16.235 | 23.163 | 0.395 | 0.713 | 230.144 | 1 |
| 60\% | 19.771 | -16.263 | 25.601 | 0.423 | 0.772 | 230.252 | 1 |
| 70\% | 23.061 | -16.282 | 28.230 | 0.442 | 0.817 | 230.372 | 1 |
| 80\% | 26.349 | -16.294 | 30.980 | 0.454 | 0.851 | 230.478 | 1 |
| 90\% | 29.659 | -16.345 | 33.865 | 0.505 | 0.876 | 230.590 | 1 |
| 100\% | 33.072 | -16.467 | 36.945 | 0.627 | 0.895 | 230.722 | 1 |

In following graphs, test results are represented after the test has been performed:


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| :---: | :---: | :---: |
|  | FGW-TG3+SP1 |  |



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| :---: | :---: | :---: |
| FGW-TG3+SP1 |  |

### 4.2.1.4 Triangular Curve: Fixed Power Factor ( $\mathrm{PF}=0.9$ )

Used settings of the measurement device for this triangular curve ( $\mathrm{PF}=0.9$ ) testing.

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| PA3000 | $2019 / 12 / 03$ | 100 ms values | 10 kHz |

Tables below show measured values for each power step tested, at both the inductive and the capacitive sides:

| Triangular Curve (PF=0.9) - Inductive |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P Desired <br> (\%Pn) | P measured <br> (kW) | Q measured <br> (kVAr) | Power <br> Factor <br> Measured <br> $(\cos \boldsymbol{\varphi})$ | Power Factor <br> Deviation <br> $(\cos \boldsymbol{\varphi})$ | $\mathbf{V}_{\mathrm{AC}}+(\mathrm{V})$ | Number of <br> records |  |
| $\mathbf{0 \%}$ | -0.051 | -0.334 | -0.151 | -1.051 | 229.887 | 1 |  |
| $\mathbf{1 0 \%}$ | 3.331 | 1.656 | 0.895 | -0.005 | 229.933 | 1 |  |
| $\mathbf{2 0 \%}$ | 6.644 | 3.280 | 0.897 | -0.003 | 230.175 | 1 |  |
| $\mathbf{3 0 \%}$ | 9.954 | 4.865 | 0.898 | -0.002 | 230.254 | 1 |  |
| $\mathbf{4 0 \%}$ | 13.254 | 6.486 | 0.898 | -0.002 | 230.484 | 1 |  |
| $\mathbf{5 0 \%}$ | 16.541 | 8.115 | 0.898 | -0.002 | 230.601 | 1 |  |
| $\mathbf{6 0 \%}$ | 19.814 | 9.734 | 0.898 | -0.002 | 230.674 | 1 |  |
| $\mathbf{7 0 \%}$ | 23.095 | 11.354 | 0.897 | -0.003 | 230.746 | 1 |  |
| $\mathbf{8 0 \%}$ | 26.355 | 12.968 | 0.897 | -0.003 | 230.853 | 1 |  |
| $\mathbf{9 0 \%}$ | 29.704 | 14.634 | 0.897 | -0.003 | 230.971 | 1 |  |
| $\mathbf{1 0 0 \%}$ | 32.983 | 16.244 | 0.897 | -0.003 | 231.126 | 1 |  |


| Triangular Curve (PF=0.9) - Capacitive |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P Desired <br> (\%Pn) | P measured <br> (kW) | Q measured <br> (kVAr) | Power <br> Factor <br> Measured <br> (cos $\boldsymbol{\varphi})$ | Power Factor <br> Deviation <br> (cos $\boldsymbol{\varphi})$ | $\mathbf{V}_{\text {AC }}+(\mathbf{V}$ ) | Number of <br> records |  |
| $\mathbf{0 \%}$ | -0.052 | 0.332 | -0.156 | -1.056 | 229.867 | 1 |  |
| $\mathbf{1 0 \%}$ | 3.314 | -1.621 | 0.898 | -0.002 | 229.919 | 1 |  |
| $\mathbf{2 0 \%}$ | 6.618 | -3.169 | 0.902 | 0.002 | 230.059 | 1 |  |
| $\mathbf{3 0 \%}$ | 9.915 | -4.753 | 0.902 | 0.002 | 230.055 | 1 |  |
| $\mathbf{4 0 \%}$ | 13.207 | -6.330 | 0.902 | 0.002 | 230.215 | 1 |  |
| $\mathbf{5 0 \%}$ | 16.519 | -7.916 | 0.902 | 0.002 | 230.263 | 1 |  |
| $\mathbf{6 0 \%}$ | 19.812 | -9.493 | 0.902 | 0.002 | 230.341 | 1 |  |
| $\mathbf{7 0 \%}$ | 23.047 | -11.045 | 0.902 | 0.002 | 230.438 | 1 |  |
| $\mathbf{8 0 \%}$ | 26.334 | -12.622 | 0.902 | 0.002 | 230.525 | 1 |  |
| $\mathbf{9 0 \%}$ | 29.634 | -14.213 | 0.902 | 0.002 | 230.642 | 1 |  |
| $\mathbf{1 0 0 \%}$ | 32.995 | -15.847 | 0.901 | 0.001 | 230.713 | 1 |  |

## FGW-TG3+SP1

In following graphs, test results are represented after the test has been performed:


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| :---: | :---: | :---: |
|  | FGW-TG3+SP1 |  |



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### 4.2.1.5 Voltage-Dependent PQ diagram: Semicircular Curve

| Testing Method Used for voltage variation |  | Comments |
| :--- | :---: | :---: |
| LVRT and/or HVRT container | $\square$ |  |
| PGU transformer tap-changer | $\square$ |  |
| Grid simulator | $\boxtimes$ |  |
| Autotransformer | $\square$ |  |
| Alternative test method | $\square$ |  |

### 4.2.1.5.1 Test 1 (90 \% Un)

Used settings of the measurement device for this voltage-dependant PQ diagram (90\% Un) testing.

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| PA3000 | $2019 / 12 / 03$ and <br> $2019 / 12 / 04$ | 100 ms values | 10 kHz |

Tables below show measured values for each power step tested, at both the inductive and the capacitive sides:

| Semicircular Curve (U = 90\% Un) - Inductive |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P Desired <br> (\%Pn) | $\mathbf{P}$ <br> measured <br> (kW) | Q <br> measured <br> (kVAr) | S <br> measured <br> (kVA) | S <br> deviation <br> (kVA) | Power Factor <br> (cos $\boldsymbol{\varphi})$ | $\mathbf{V}_{\mathrm{AC}}+(\mathrm{V})$ | Number of <br> records |
| $\mathbf{0 \%}$ | -0.084 | 0.468 | 0.475 | 32.525 | -0.177 | 206.9 | 1 |
| $\mathbf{1 0 \%}$ | 3.265 | 16.432 | 16.753 | 16.247 | 0.195 | 207.3 | 1 |
| $\mathbf{2 0 \%}$ | 6.579 | 16.051 | 17.347 | 15.653 | 0.379 | 207.1 | 1 |
| $\mathbf{3 0 \%}$ | 9.946 | 16.009 | 18.847 | 14.153 | 0.528 | 207.1 | 1 |
| $\mathbf{4 0 \%}$ | 13.263 | 15.994 | 20.778 | 12.222 | 0.638 | 207.2 | 1 |
| $\mathbf{5 0 \%}$ | 16.562 | 15.972 | 23.009 | 9.991 | 0.720 | 207.3 | 1 |
| $\mathbf{6 0 \%}$ | 19.841 | 15.964 | 25.466 | 7.534 | 0.779 | 207.4 | 1 |
| $\mathbf{7 0 \%}$ | 23.130 | 15.976 | 28.111 | 4.889 | 0.823 | 207.3 | 1 |
| $\mathbf{8 0 \%}$ | 26.390 | 16.015 | 30.869 | 2.131 | 0.855 | 207.4 | 1 |
| $\mathbf{9 0 \%}$ | 29.261 * $\left.^{*}\right)$ | 16.110 | 33.403 | -0.403 | 0.876 | 207.5 | 1 |
| $\mathbf{1 0 0 \%}$ | 29.258 * $\left.^{*}\right)$ | 16.110 | 33.400 | -0.400 | 0.876 | 207.5 | 1 |

(*) Working at $90 \%$ Un the inverter does not reach $100 \%$ Sn due to the current limitation function. Maximum apparent power that can be reached corresponds to $100 \%$ Sn, approximately. Deviations are calculated in relation to this expected semicircular value. See further details in figure below.

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| Semicircular Curve (U = 90\% Un) - Capacitive |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P Desired <br> (\%Pn) | P <br> measured <br> (kW) | Q <br> measured <br> (kVAr) | S <br> measured <br> (kVA) | S <br> deviation <br> (kVA) | Power Factor <br> (cos $\boldsymbol{\varphi}$ ) | $\mathbf{V}_{\text {AC }+(V)}$ | Number of <br> records |
| $\mathbf{0 \%}$ | -0.024 | -0.452 | 0.453 | 32.547 | -0.053 | 206.9 | 1 |
| $\mathbf{1 0 \%}$ | 3.325 | -15.493 | 15.845 | 17.155 | 0.210 | 206.7 | 1 |
| $\mathbf{2 0 \%}$ | 6.662 | -15.507 | 16.877 | 16.123 | 0.395 | 206.9 | 1 |
| $\mathbf{3 0 \%}$ | 9.992 | -15.518 | 18.457 | 14.543 | 0.541 | 206.9 | 1 |
| $\mathbf{4 0 \%}$ | 13.276 | -15.531 | 20.432 | 12.568 | 0.650 | 207.1 | 1 |
| $\mathbf{5 0 \%}$ | 16.541 | -15.555 | 22.706 | 10.294 | 0.728 | 207.2 | 1 |
| $\mathbf{6 0 \%}$ | 19.808 | -15.569 | 25.194 | 7.806 | 0.786 | 207.3 | 1 |
| $\mathbf{7 0 \%}$ | 23.094 | -15.584 | 27.860 | 5.140 | 0.829 | 207.4 | 1 |
| $\mathbf{8 0 \%}$ | 26.425 | -15.646 | 30.710 | 2.290 | 0.860 | 207.6 | 1 |
| $\mathbf{9 0 \%}$ | 29.031 * $\left.^{*}\right)$ | -15.775 | 33.040 | -0.040 | 0.879 | 207.7 | $\mathbf{1}$ |
| $\mathbf{1 0 0 \%}$ | 29.03 (*) $^{*}$ | -15.774 | 33.042 | -0.042 | 0.879 | 207.711 | $\mathbf{1}$ |

(*) Working at $90 \%$ Un the inverter does not reach $100 \%$ Pn due to the current limitation function while reactive power priority. Maximum apparent power that can be reached corresponds to $100 \%$ Sn, approximately. Deviations are calculated in relation to this expected semicircular value. See further details in figure below.

## FGW-TG3+SP1

In following graphs, test results are represented after the test has been performed:


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| :---: | :---: | :---: |

### 4.2.1.5.2 Test 2 (110 \% Un)

Used settings of the measurement device for this voltage-dependant PQ diagram (110\% Un) testing.

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| PA3000 | $2020 / 08 / 27$ | 100 ms values | 10 kHz |

Tables below show measured values for each power step tested, at both the inductive and the capacitive sides:

| Semicircular Curve (U = 110\% Un) - Inductive |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{P}$ Desired <br> (\%Pn) | $\mathbf{P}$ <br> measured <br> (kW) | Q <br> measured <br> (kVAr) | S <br> measured <br> (kVA) | $\mathbf{S}$ <br> deviation <br> (kVA) | Power Factor <br> (cos $\boldsymbol{\varphi}$ ) | $\mathbf{V}_{\text {AC }+(V)}$ | Number of <br> records |
| $\mathbf{0 \%}$ | 0.133 | 15.860 | 15.861 | -0.121 | 0.008 | 252.7 | 1 |
| $\mathbf{1 0 \%}$ | 3.431 | 15.912 | 16.278 | -0.041 | 0.211 | 252.8 | 1 |
| $\mathbf{2 0 \%}$ | 6.741 | 15.967 | 17.332 | 0.041 | 0.389 | 252.8 | 1 |
| $\mathbf{3 0 \%}$ | 9.963 | 16.015 | 18.862 | 0.062 | 0.528 | 252.9 | 1 |
| $\mathbf{4 0 \%}$ | 13.171 | 16.001 | 20.725 | -0.003 | 0.636 | 253.0 | 1 |
| $\mathbf{5 0 \%}$ | 16.443 | 16.052 | 22.979 | 0.008 | 0.716 | 253.1 | 1 |
| $\mathbf{6 0 \%}$ | 19.884 | 16.043 | 25.549 | 0.104 | 0.778 | 253.2 | 1 |
| $\mathbf{7 0 \%}$ | 23.280 | 15.965 | 28.229 | 0.139 | 0.825 | 253.3 | 1 |
| $\mathbf{8 0 \%}$ | 26.319 | 16.016 | 30.809 | -0.051 | 0.854 | 253.4 | 1 |
| $\mathbf{9 0 \%}$ | 29.729 | 16.072 | 33.795 | 0.068 | 0.880 | 253.4 | 1 |
| $\mathbf{1 0 0 \%}$ | 33.109 | 16.130 | 36.829 | 0.162 | 0.899 | 253.5 | $\mathbf{1}$ |
| $\mathbf{1 0 8 \%}$ (*) | 33.108 | 16.130 | 36.828 | -2.834 | 0.899 | 253.5 | $\mathbf{1}$ |

(*) Working at $110 \%$ Un the inverter can reach $108 \%$ Pn while reactive power priority. Maximum apparent power that can be reached corresponds to $110 \% \mathrm{Sn}$, approximately. Deviations are calculated in relation to this expected semicircular value. See further details in figure below.

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| :---: | :---: | :---: |
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| Semicircular Curve (U = 110\% Un) - Capacitive |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P Desired <br> (\%Pn) | $\mathbf{P}$ <br> measured <br> (kW) | measured <br> (kVAr) | S <br> measured <br> (kVA) | S <br> deviation <br> (kVA) | Power Factor <br> (cos $\boldsymbol{\varphi})$ | $\mathbf{V}_{\text {AC }+(\text { (V) }}$ | Number of <br> records |
| $\mathbf{0 \%}$ | 0.091 | -16.092 | 16.093 | 0.112 | 0.006 | 252.6 | 1 |
| $\mathbf{1 0 \%}$ | 3.368 | -15.998 | 16.349 | 0.030 | 0.206 | 252.7 | 1 |
| $\mathbf{2 0 \%}$ | 6.686 | -15.957 | 17.301 | 0.010 | 0.386 | 252.8 | 1 |
| $\mathbf{3 0 \%}$ | 9.984 | -15.916 | 18.788 | -0.011 | 0.531 | 252.9 | 1 |
| $\mathbf{4 0 \%}$ | 13.340 | -15.871 | 20.732 | 0.004 | 0.643 | 253.0 | 1 |
| $\mathbf{5 0 \%}$ | 16.716 | -16.018 | 23.151 | 0.180 | 0.722 | 253.1 | 1 |
| $\mathbf{6 0 \%}$ | 19.978 | -15.976 | 25.580 | 0.135 | 0.781 | 253.2 | 1 |
| $\mathbf{7 0 \%}$ | 23.218 | -15.936 | 28.161 | 0.071 | 0.824 | 253.2 | 1 |
| $\mathbf{8 0 \%}$ | 26.410 | -16.060 | 30.910 | 0.049 | 0.854 | 253.3 | 1 |
| $\mathbf{9 0 \%}$ | 29.645 | -16.021 | 33.697 | -0.030 | 0.880 | 253.4 | 1 |
| $\mathbf{1 0 0 \%}$ | 33.065 | -15.977 | 36.722 | 0.056 | 0.900 | 253.5 | $\mathbf{1}$ |
| $\mathbf{1 1 0 \%}$ | $\left.33.2444^{*}\right)$ | -15.984 | 36.887 | -2.775 | 0.901 | 253.5 | $\mathbf{1}$ |

${ }^{(*)}$ Working at $110 \%$ Un the inverter can reach $108 \%$ Pn while reactive power priority. Maximum apparent power that can be reached corresponds to $110 \%$ Sn, approximately. Deviations are calculated in relation to this expected semicircular value. See further details in figure below.

## FGW-TG3+SP1

In following graphs, test results are represented after the test has been performed:


### 4.2.1.5.3 Voltage-Dependent PQ diagram: resume of results

In following graphs, semicircular curves are represented for tests above detailed.


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| :---: | :---: | :---: |

### 4.2.2 Reactive Power Following Setpoints

The aim of this test is to determine the PGU's reaction to the reactive power setpoint input in relation to the setting accuracy and the settling time.
The required testing has been performed according to the point 4.2.4 of the standard. It can be applied to both PV and storage systems

Different reactive power Q setpoint signals were applied to the inverter in order to verify the proper behavior working at different active power levels. In addition, it was verified the capability of the inverter to set different setting values for the time response.

For all test, the displacement factor, the active power and the reactive power measurements in the positive phase sequence system have been represented as 20 milisecond means for every setpoint step.

| Interface information |  |
| :---: | :---: |
| Interface used | Solar communication tools, RS485 |
| Interface version used | V250 |
| Other interfaces in the equipment | N/A |
| Name or code of the parameter for <br> Reactive power setpoint \& settling time | Reactive parameters |
| If the EUT has several different interfaces for defining the setpoint, it has been tested the interface <br> returning the most unfavourable results according to the manufacturer information. |  |

EUT Settings used for this test are provided in the following table:

| EUT Settings |  |
| :---: | :---: |
| Operanting mode | Reactive power priority |
| Active control modes | Active power control |
|  | LVRT mode |
|  | Fixed Reactive power control |

Test results are offered in following points.

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| :---: | :---: | :---: |

### 4.2.2.1 Determining the settling time

Different tests have been performed at two different power levels:

- Test $1: 50 \%$ of $P_{n}$ (settling time shortest as possible); Configured time setting value: 6 s
- Test 2: $80 \%$ of $P_{n}$ (settling time longest as possible); Configured time setting value: 60 s
(Due to the maximum reactive power range lies within an active power level of $48.43 \% \mathrm{Pn}$ ).
Time setting values that may be parametrized in the control as given by manufacturer's specifications: Range from 0 to 60 s

The following table shows de reactive power range:

| Q range at 50\% Pn | 0 to $48.43 \% \mathrm{Pn}$ |
| :---: | :---: |
| Maximum Q range | 0 to $48.48 \% \mathrm{Pn}$ |
| Note: Maxímum power range is acchivied with an Active power of $93.0 \% \mathrm{Pn}$ |  |

## - Test 1: Active power at 50\%Pn

Operating at this active power level, the inverter was subjected to following reactive power step changes providing its maximum Q level available corresponding to $48.43 \% \mathrm{Pn}$.

| Step | Comments |  |
| :---: | :---: | :---: |
| 1 | $\mathrm{t}_{1}=0 \mathrm{~s}$ | Recording is started |
| 2 | $\mathrm{t}_{2}=10 \mathrm{~s}$ | Setting the setpoint to the maximum possible <br> reactive power in overexcited operation with <br> the selected active power level Qmax,oe |
| 3 | $\mathrm{t}_{3} \geq \mathrm{t}_{2}+\mathrm{t}_{\text {settling }}+10 \mathrm{~s}$ | Setting the setpoint to the maximum possible <br> reactive power in underexcited operation with <br> the selected active power level Qmax,ue |
| 4 | $\mathrm{t}_{4} \geq \mathrm{t}_{3}+\mathrm{t}_{\text {settling }}+10 \mathrm{~s}$ | Setpoint set to $\cos \varphi=1(\mathrm{Q}=0)$ |
| 5 | $\mathrm{t}_{5} \geq \mathrm{t}_{4}+\mathrm{t}_{\text {settling }}+10 \mathrm{~s}$ | Recording is stopped |

The settling time for this test was set to be the shortest as possible (but no longer than 6 s ) corresponding to 5.8 seconds, approximately.

- Test 2: Active power at $80 \%$ Pn

Operating at this active power level, the inverter was subjected to following reactive power step changes providing its maximum Q level available corresponding to $48.43 \% \mathrm{Pn}$.

| Step | Comments |  |
| :---: | :---: | :---: |
| 1 | $\mathrm{t}_{1}=0 \mathrm{~s}$ | Recording is started |
| 2 | $\mathrm{t}_{2}=10 \mathrm{~s}$ | Setting the setpoint to the maximum possible <br> reactive power in overexcited operation with <br> the selected active power level 50\%Qmax,oe |
| 3 | $\mathrm{t}_{3} \geq \mathrm{t}_{2}+\mathrm{t}_{\text {settling }}+10 \mathrm{~s}$ | Setting the setpoint to the maximum possible <br> reactive power in underexcited operation with <br> the selected active power level 50\%Qmax,ue |
| 4 | $\mathrm{t}_{4} \geq \mathrm{t}_{3}+\mathrm{t}_{\text {settling }}+10 \mathrm{~s}$ | Setpoint set to $\cos \varphi=1(\mathrm{Q}=0)$ |
| 5 | $\mathrm{t}_{5} \geq \mathrm{t}_{4}+\mathrm{t}_{\text {settling }}+10 \mathrm{~s}$ | Recording is stopped |

The settling time for this test was set to be the shortest as possible (but no longer than 6 s ) corresponding to 60 seconds, approximately.

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| :---: | :---: | :---: |
|  | FGW-TG3+SP1 |  |

Used settings of the measurement device for the testing of reactive power following setpoins (Settling time). According to the standard, measurements must be taken every 20 ms .

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| PA3000 | $2019 / 12 / 04$ | 100 ms values | 10 kHz |

Test results are offered in following points:
The settling time for all steps is determined and given while taking the $\pm 5 \%$ Pn tolerance band into consideration.

### 4.2.2.1.1 Test 1

The following table show test results of the settling time determined after each step.


In following graphs, test results are represented after the test has been performed:


## FGW-TG3+SP

## Test 1: zoom time of the step 2



Test 1: zoom time of the step 3


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| :---: | :---: | :---: |
| FGW-TG3+SP1 |  |



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| :---: | :---: | :---: |
|  | FGW-TG3+SP1 |  |

### 4.2.2.1.2 Test 2

The following table show test results of the settling time determined after each step.

| Settling time (longest possible but lower than 60 seconds) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Power |  | Reactive Power Steps |  | Point in time of setpoint Change (s) | Point in time of settling (s) | Time Difference <br> (s) |
| Desired (\% Pn) | Measured (\% Pn) | Step | Description |  |  |  |
| 80.0\% | 80.2\% | 1 | 0\% $\mathrm{Q}_{\text {max }}$ | - | - | - |
|  |  | 2 | 0\% $\mathrm{Qmax}^{\text {m }}+50 \% \mathrm{Q}_{\text {max }}$ | 129.3 | 175.3 | 46.0 |
|  |  | 3 | $+50 \% Q_{\max } \rightarrow-50 \% \mathrm{Q}_{\max }$ | 336.7 | 390.2 | 53.5 |
|  |  | 4 | $-50 \% \mathrm{Q}_{\max } \rightarrow 0 \% \mathrm{Q}_{\max }$ | 571.1 | 619.2 | 48.1 |
|  |  | 5 | 0\% Q ${ }_{\text {max }}$ | - | - | - |
|  |  |  |  |  |  |  |
| Longest measured setting time (s) |  |  |  |  | 53.5 |  |

In following graphs, test results are represented after the test has been performed:


Zoom time of the step 2


## FGW-TG3+SP1

## Zoom time of the step 3



Zoom time of the step 4


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| :---: | :---: | :---: |
| FGW-TG3+SP1 |  |

### 4.2.2.2 Determining the setting accuracy

They have been done following steps measuring the time from leaving the initial $Q$ set point until reaching the final.

| Step | Comments |  |
| :---: | :---: | :---: |
| 1 | $\mathrm{t}_{1}=0 \mathrm{~s}$ | Recording is started |
| 2 | $\mathrm{t}_{2}=10 \mathrm{~s}$ | Setpoint set to $50.0 \% \mathrm{Qmax}_{\text {ma }}$ oe |
| 3 | $\mathrm{t}_{3}=\mathrm{t}_{2}+120 \mathrm{~s}$ | Setpoint set to $50.0 \% \mathrm{Q}_{\text {max }, \text { ue }}$ |
| 4 | $\mathrm{t}_{4}=\mathrm{t}_{3}+120 \mathrm{~s}$ | Setpoint set to $\cos \varphi=1(\mathrm{Q}=0)$ |
| 5 | $\mathrm{t}_{5}=\mathrm{t}_{4}+120 \mathrm{~s}$ | Recording is stopped |

Used settings of the measurement device for the testing of reactive power following setpoins (Accuracy).

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| PA3000 | $2019 / 12 / 04$ | 100 ms values | 10 kHz |

The following table shows the results of reactive power, active power, displacement factor and output voltage measured for the test performed under partial load ( $50 \% \mathrm{Pn}$ ). Setpoints of reactive power fixed, as 1 minute mean values, have a maximum tolerance allowed up to $\pm 5 \% \mathrm{Pn}$.
All values are in the positive sequence system.

| Accuracy test |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Reactive <br> Power steps | Setpoint <br> value (kVAr) | Actual value <br> (kVAr) | Setpoint - <br> actual value <br> (kVAr) | $\cos \boldsymbol{\varphi}$ | Grid <br> voltage <br> $(\mathbf{V})$ | Measured <br> Active Power <br> (kW) |
| $\mathrm{Q}_{0}$ | 0 | 0.788 | -0.788 | 1.000 | 230.9 | 26.467 |
| $50 \%$ Qmax $^{\text {Overexited }}$ | 7.991 | 8.051 | -0.060 | 0.957 | 230.9 | 26.438 |
| $50 \% Q_{\max }$ <br> Underexcited | -7.991 | -8.063 | 0.072 | 0.957 | 230.7 | 26.502 |


| Maximum deviation from the setpoint (kVAr) | 0.788 |
| :---: | :---: |
| Q range at 50\% $\mathbf{n}$ | 0 to $48.43 \% \mathrm{Pn}$ |
| Maximum Q range | $48.43 \% \mathrm{Pn}$ |

In following graphs, test results are represented after the test has been performed:

## FGW-TG3+SP1



## Zoom time of the step 2: +50\% to -50\% Q $_{\text {max }}$



Zoom time of the step 3: -50\% to 0\% $\mathbf{Q}_{\text {max }}$


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| :---: | :---: | :---: |

### 4.2.3 $\quad Q(U)$ Control (Voltage regulation)

The aim of this test is to examine the voltage regulation method by means of reactive power or displacement factor control as a function of the voltage.

These tests have been performed according to the point 4.2.5 of the standard. It can be applied to both PV and storage systems.

The $Q(U)$ characteristic curve was set to follow a response as represented in the following image:


Being defined this $Q(U)$ curve as follows:

| Output Voltage, U | 0.96 Un | Un | 1.04 Un |
| :--- | :---: | :---: | :---: |
| Reactive Power, Q | $48.43 \% \mathrm{Pn}$ (leading) | $0 \% \mathrm{Pn}$ | $48.43 \% \mathrm{Pn}$ (lagging) |

Different tests have been done to determinate both the setting accuracy and the setting time. In both cases, the setting time was adjusted to be the shortest as possible.

For all test, the active power, reactive power and voltage have been measured in the positive phase sequence system and have been represented as 200 milisecond means for every setpoint step.

| Interface information |  |
| :---: | :---: |
| Interface used | Solar communication tools, RS485 |
| Interface version used | V250 |
| Other interfaces in the equipment | N/A |
| Name or code of the parameter for |  |
| Reactive power setpoint \& settling time | Reactive parameters |

If the EUT has several different interfaces for defining the setpoint, it has been tested the interface returning the most unfavourable results according to the manufacturer information.

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| :---: | :---: | :---: |

EUT Settings used for this test are provided in the following table:

| EUT Settings |  |
| :---: | :---: |
| Operanting mode | Reactive power priority |
| Active control modes | Active power control |
|  | LVRT mode |
|  | Fixed Reactive power control |
|  | Reactive power VS Voltage |

Test results are offered in following points.

### 4.2.3.1 Determining the accuracy

This test verifies the capability of the inverter to modify the injection of reactive power under voltage variations inside the normal operation range.

Used settings of the measurement device for the testing of $Q(U)$ control:

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| PA3000 | $2020 / 04 / 13$ | 100 ms values | 10 kHz |

Steps have been commanded as follow that can be seen on the following table:

| Step | Step time | Voltage desired <br> (p.u) | Reactive Power expected (\%Pn) |
| :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | $\mathrm{t} 1=0 \mathrm{~s}$ | 1.00 | $0 \%$ |
| $\mathbf{2}$ | $\mathrm{t} 2=\mathrm{t} 1+120 \mathrm{~s}$ | 0.97 | $36.32 \%$ |
| $\mathbf{3}$ | $\mathrm{t} 3=\mathrm{t} 2+120 \mathrm{~s}$ | 1.03 | $-36.32 \%$ |
| $\mathbf{4}$ | $\mathrm{t} 4=\mathrm{t} 3+120 \mathrm{~s}$ | 1.00 | $0 \%$ |
| $\mathbf{5}$ | $\mathrm{t} 5=\mathrm{t} 4+120 \mathrm{~s}$ | 1.00 | $0 \%$ |

Each voltage step was maintained for at least 60 seconds and the complete test was performed maintaining an active power level corresponding to $50 \% \mathrm{Pn}$, as the standard requires a power level superior to $50 \%$ Pn.

The maximum tolerance allowed for reactive power measurements is $\pm 5 \% \mathrm{Pn}$ and they have been verified for the last 1 minute mean average at the end of the step.

The following table shows the test results for the last 60 seconds average of each step:

| Step | Measured Vac + |  | Measured P |  | Measured Q |  | deviation <br> (kVAr) | Measured Power Factor |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | (p.u) | (V) | (\%Sn) | (kW) | (\%Sn) | (kVAr) |  |  |
| 1 | 1.000 | 229.9 | 51.01 | 16.833 | 0.57 | 0.187 | 0.187 | 1.000 |
| 2 | 0.969 | 223.0 | 50.70 | 16.730 | 36.47 | 12.035 | 0.050 | 0.810 |
| 3 | 1.031 | 237.0 | 50.91 | 16.801 | -36.65 | -12.096 | -0.110 | 0.813 |
| 4 | 1.000 | 230.0 | 51.01 | 16.832 | 0.52 | 0.173 | 0.173 | 1.000 |
| 5 | 1.000 | 230.0 | 51.01 | 16.833 | 0.58 | 0.191 | 0.191 | 1.000 |

Maximum deviation from the setpoint (kVAr) $\quad 0.191$

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| :---: | :---: | :---: |

In following graphs, test results are represented after test has been performed:


Reactive Power over Voltage


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| :---: | :---: | :---: |

### 4.2.3.2 Determining the settling time

This test determines the time response of the inverter to modify the injection of reactive power under voltage variations inside the normal operation range.

Used settings of the measurement device for the testing of $Q(U)$ control:

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| PA3000 | $2020 / 04 / 13$ | 100 ms values | 10 kHz |

Operating at an active power level corresponding to $50 \% \mathrm{Pn}$, the inverter was subjected to following voltage step changes:

| Step | Comment |  |
| :---: | :---: | :---: |
| 1 | $\mathrm{t}_{1}=0 \mathrm{~s}$ | Recording is started |
| 2 | $\mathrm{t}_{2}=120 \mathrm{~s}$ | Step change to 0.97 Un |
| 3 | $\mathrm{t}_{3}=\mathrm{t}_{2}+120 \mathrm{~s}$ | Step change to 1.03 Un |
| 4 | $\mathrm{t}_{4}=\mathrm{t}_{3}+120 \mathrm{~s}$ | Step change to Un |
| 5 | $\mathrm{t}_{5}=\mathrm{t}_{4}+120 \mathrm{~s}$ | Recording is stopped |

The settling time for all steps is determined and given while taking the $\pm 5 \% \mathrm{Pn}$ tolerance band into consideration.

Two tests have been carried out, one with the case of settling time set as the shortest as possible and another with the settling time set as the longest as possible.

- Test 1: Settling time shortest as possible: Configured time setting value: 1 s
- Test 2: Settling time longest as possible: Configured time setting value: 60 s

Time setting values that may be parametrized in the control as given by manufacturer's specifications: Range from 1 to 60 s .

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| :---: | :---: | :---: |
| FGW-TG3+SP1 |  |

### 4.2.3.2.1 Test 1

The following table shows test results:
The actual value is predefined by the network operator, then a value of 1 s applies. Due to the installations may have adjustable settling time between 1 s and 5 s (step response time)

| Settling time (shortest possible) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Power |  | Step | Comments | Point in time of setpoint change (s) | Point in time of settling inside the tolerance band (s) | Time different (s) |
| $\begin{aligned} & \text { Desired } \\ & \text { (\% Pn) } \end{aligned}$ | Measured (\% Pn) |  |  |  |  |  |
| $\geq 50 \%$ | 50.9\% | 1 | $\mathrm{U}_{0}=0.93 \mathrm{U}_{\mathrm{n}}$ | -- | -- | -- |
|  |  | 2 | $0.93 \mathrm{U}_{\mathrm{n}} \rightarrow 0.97 \mathrm{U}_{\mathrm{n}}$ | 140.2 | 140.8 | 0.6 |
|  |  | 3 | $0.97 \mathrm{U}_{\mathrm{n}} \rightarrow 1.03 \mathrm{U}_{n}$ | 291.3 | 291.9 | 0.6 |
|  |  | 4 | $1.03 \mathrm{Un}_{\mathrm{n}} \rightarrow \mathrm{U}_{n}$ | 442.1 | 443.1 | 1.0 |
|  |  | 5 | Recording is Stopped | -- | -- | -- |
|  |  |  |  |  |  |  |
| Longest Measured settling time (s) |  |  |  |  | 1.0 |  |

The following table shows the reactive power variation to time $(\Delta Q / \Delta t)$ during the settling time:

| Step | $\mathbf{Q}$ at the start <br> $\mathbf{( k V A r )}$ | $\mathbf{Q}$ at the end <br> $\mathbf{( k V A r )}$ | Time Response <br> $(\mathbf{s})$ | $\mathbf{\Delta \mathbf { Q } / \mathbf { \Delta t }}$ <br> $\mathbf{( k V A r} / \mathbf{s})$ |
| :---: | :---: | :---: | :---: | :---: |
| $\mathbf{2}$ | 1.335 | 12.045 | 0.6 | 17.850 |
| $\mathbf{3}$ | 12.111 | -12.144 | 0.6 | -40.425 |
| $\mathbf{4}$ | -12.210 | 0.528 | 1.0 | 12.738 |

In following graphs, they are represented test results after the test performed:


Zoom time of the step 2: Un to 0.97 Un



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| :---: | :---: | :---: |
| FGW-TG3+SP1 |  |

### 4.2.3.2.2 Test 2

The following table shows test results:
The actual value is predefined by the network operator, then a value of 60 s applies. Due to the installations may have adjustable settling time between 6 s and 60 s (step response time)

| Settling time (longest possible) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Power |  | Step | Comments | Point in time of setpoint change (s) | Point in time of settling inside the tolerance band (s) | Time different <br> (s) |
| Desired (\% Pn) | Measured (\% Pn) |  |  |  |  |  |
| $\geq 50 \%$ |  | 1 | $\mathrm{U}_{0}=0.93 \mathrm{U}_{\mathrm{n}}$ | -- | -- | -- |
|  |  | 2 | $0.93 \mathrm{Un}_{\mathrm{n}} \rightarrow 0.97 \mathrm{U}_{\mathrm{n}}$ | 224.4 | 282.0 | 57.6 |
|  |  | 3 | $0.97 \mathrm{U}_{\mathrm{n}} \rightarrow 1.03 \mathrm{U}_{\mathrm{n}}$ | 451.9 | 511.6 | 59.7 |
|  |  | 4 | $1.03 \mathrm{U}_{\mathrm{n}} \rightarrow \mathrm{U}_{\mathrm{n}}$ | 643.3 | 703.0 | 59.7 |
|  |  | 5 | Recording is Stopped | -- | -- | -- |

## Longest Measured settling time (s)

The following table shows the reactive power variation to time $(\Delta \mathrm{Q} / \Delta \mathrm{t})$ during the settling time:

| Step | $\mathbf{Q}$ at the start <br> $\mathbf{( k V A r )}$ | $\mathbf{Q}$ at the end <br> $\mathbf{( k V A r})$ | Time Response <br> $(\mathbf{s})$ | $\mathbf{\Delta \mathbf { Q } / \mathbf { \Delta t }}$ <br> $\mathbf{( k V A r / s )}$ |
| :---: | :---: | :---: | :---: | :---: |
| $\mathbf{2}$ | 0.792 | 12.012 | 57.6 | 0.195 |
| $\mathbf{3}$ | 12.111 | -12.144 | 59.7 | -0.406 |
| $\mathbf{4}$ | -12.276 | 0.495 | 59.7 | 0.214 |

following graphs, they are represented test results after the test performed:


Zoom time of the step 2: Un to 0.97 Un


## Zoom time of the step 3: 0.97 Un to 1.03 Un



Zoom time of the step 4: 1.03 Un to Un


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| :---: | :---: | :---: |

### 4.2.4 $\quad Q(P)$ control

The aim of this test is to examine the reactive power control method as a function of the active power.
These tests have been performed according to the point 4.2.6 of the standard. Although this test is optional, it has been tested nevertheless.

The $Q(P)$ characteristic curve was set to follow a response as represented in the following image:


Being defined this $Q(P)$ curve as follows:

| Node Position | $\mathbf{P}_{\text {mom }} / \mathbf{P}_{\mathbf{n}}$ | $\mathbf{Q} / \mathbf{P}_{\mathbf{n}}$ |
| :---: | :---: | :---: |
| P1 | 0 | 0 |
| P2 | 0.5 | 0 |
| P3 | 0.6 | -0.109 |
| P4 | 0.9 | -0.436 |
| P5 | 1.0 | -0.436 |

The response time was adjusted to be the shortest as possible.
Test results are offered in following points.

| Interface information |  |
| :---: | :---: |
| Interface used | Solar communication tools, RS485 |
| Interface version used | V250 |
| Other interfaces in the equipment | N/A |
| Name code of the parameter for <br> (P) \& settling time |  |
| If the EUT has several different interfaces for defining the setpoint, it has been tested the interface <br> returning the most unfavourable results according to the manufacturer information. |  |
| As the interface tested has different versions it has been tested the most unfauvorable version <br> according to manufacturer information. |  |

EUT Settings used for this test are provided in the following table:

| EUT Settings |  |
| :---: | :---: |
| Operanting mode | Reactive power priority |
| Active control modes | Active power control |
|  | LVRT mode |
|  | Reactive power VS Active power |

- Test 1: Settling time shortest as possible: Configured time setting value: 1 s

Time setting values that may be parametrized in the control as given by manufacturer's specifications:
Range from 0 to 60 s

### 4.2.4.1 Determining the setting accuracy

This test verifies the capability of the inverter to modify the reactive power under changes in the active power commanded by setpoint.

Used settings of the measurement device for the testing of $Q(P)$ control:

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| PA3000 | $2020 / 04 / 13$ | 100 ms values | 10 kHz |

They have been commanded steps that can be seen on the following table:

| Step | Active power desired (\%Sn) | Reactive Power expected |
| :---: | :---: | :---: |
| $\mathbf{1}$ | $10.0 \%$ | $0.0 \%$ |
| $\mathbf{2}$ | $45.0 \%$ | $0.0 \%$ |
| $\mathbf{3}$ | $55.0 \%$ | $5.5 \%$ |
| $\mathbf{4}$ | $75.0 \%$ | $27.2 \%$ |
| $\mathbf{5}$ | $95.0 \%$ | $43.6 \%$ |

The inverter shall calculate automatically the reactive power setpoint from the measured active power.
Each active power step was maintained for at least 120 seconds, being calculated voltage, powers and power factor signals for the last 60 seconds mean average at the end of the step.
The response time was adjusted to be the shortest as possible (but no longer than 6s).
According to testing method of the standard, the 1-minute mean value at the end of the step is measured. Dropping below or exceeding the active power node points in the stationary condition of a step has to be avoided.

The following table shows the test results for the last 60 second average of each step, showing the positive phase sequence components:

| Step | P Setpoint |  | Measured P |  | Q Setpoint |  | Measured Q |  | Q <br> deviation <br> $(\mathbf{k V A r})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{( \% P n )}$ | $\mathbf{( k W )}$ | $\mathbf{( \% P n )}$ | $\mathbf{( k W )}$ | $\mathbf{( \% P n )}$ | $\mathbf{( k V A r )}$ | $\mathbf{( \% P n )}$ | $\mathbf{( k V A r )}$ |  |
| $\mathbf{1}$ | $10.00 \%$ | 3.3 | $10.17 \%$ | 3.357 | $0.00 \%$ | 0 | $1.50 \%$ | 0.495 | 0.511 |
| $\mathbf{2}$ | $45.00 \%$ | 14.85 | $44.95 \%$ | 14.833 | $0.00 \%$ | 0 | $1.55 \%$ | 0.511 | 0.510 |
| $\mathbf{3}$ | $55.00 \%$ | 18.15 | $55.12 \%$ | 18.189 | $-5.50 \%$ | -1.815 | $-5.71 \%$ | -1.886 | -0.071 |
| $\mathbf{4}$ | $75.00 \%$ | 24.75 | $74.82 \%$ | 24.691 | $-27.20 \%$ | -8.976 | $-27.30 \%$ | -9.009 | -0.033 |
| $\mathbf{5}$ | $95.00 \%$ | 31.35 | $94.62 \%$ | 31.225 | $-43.60 \%$ | -14.388 | $-44.13 \%$ | -14.564 | -0.176 |


| Maximum deviation from the Q calculated setpoint (kVAr) | 0.511 |
| :---: | :---: |
| Settling time (s) | 0.9 |

The maximum tolerance allowed for each value is $2 \%$ of the rated value per each value.

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| :---: | :---: | :---: |
|  | FGW-TG3+SP1 |  |

In following graphs, test results are represented using 200 ms mean values of active power, reactive power and calculated reactive power set-point input after the test has been performed:


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| :---: | :---: | :---: |
|  | FGW-TG3+SP1 |  |

### 4.2.5 Reactive Power $Q$ with voltage limitation function

These tests have been requriment with chapter 4.2.7, 6.1.3.2 and 6.1.4.2 of the standards.
The aim of these tests is to show compliance with the characteristic curve from both VDE AR-N 4110:2018 presented below:


The active power at the beginning of this test should be $\geq 40 \%$ of the total rated active power of the operating PGU. Each step has been measured at least 2 min . The 1-minute mean value at the end of each step have been measured.

Different tests have been done to determinate both the setting accuracy and the setting time. In both cases, the setting time was adjusted to be the shortest as possible.

As commnunite with customer, this test is not performed due to this test is optional.

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| :---: | :---: | :---: |

### 4.3 SYSTEM PERTURBATIONS.

### 4.3.1 Switching operations

The aim of this test is to determine the grid-dependent voltage variation factors $\mathrm{K}_{\mathrm{u}}\left(\Psi_{\mathrm{k}}\right)$ and flicker form factors $K_{f}\left(\Psi_{k}\right)$ in order to estimate systems perturbations at the point of common coupling.

This test has been performed according to the 4.3.2. of the standard.
These measures have been done following the reference IEC 61400-21
The following definitions apply to the test:

- Maximum number of switching operations within a time period of $10 \mathrm{~min} . \mathrm{N}_{10}$
- Maximum number of switching operations within a time period of $120 \mathrm{~min} . \mathrm{N}_{120}$

The following switching operations should be investigated at each impedance angle ( $30^{\circ}, 50^{\circ}, 70^{\circ}, 85^{\circ}$ ):

- Test 1: Switching at Pavailable $<10 \%$ Pn. $\mathrm{N}_{10}=20, \mathrm{~N}_{120}=240 . \mathrm{T}_{\mathrm{p}}=65 \mathrm{~s}$.
- Test 2: Switching at Pavailable $=$ Pn. $\mathrm{N}_{10}=20, \mathrm{~N}_{120}=240 . \mathrm{T}_{\mathrm{p}}=65 \mathrm{~s}$
- Test 3: Service shutdown at rated power (no emergency stop).

Note: $T_{p} \equiv$ Time per switching operation $T_{p}=t_{3}-t_{0} . T_{p}$ includes the following times:

1. Start of measurement.
2. Beginning of recording analysis range $\left(\mathrm{t}=\mathrm{t}_{0}\right)$
3. Beginning of switching operation ( $\mathrm{t}=\mathrm{t}_{1}$ )
4. Switching operation's transient phenomena have dissipated, PGU feeds in active power in line with the active power setpoint $\left(\mathrm{t}=\mathrm{t}_{2}\right)$
5. End of recording analysis range ( $\mathrm{t}=\mathrm{t}_{3}$ )
6. End of measurement.

The following parameters are to be reported:
Flicker factor $\mathrm{kf}_{\mathrm{f}}\left(\Psi_{\mathrm{k}}\right)$ :

$$
\mathrm{k}_{\mathrm{f}}\left(\Psi_{\mathrm{k}}\right)=\frac{1}{130} \times \frac{\mathrm{S}_{\mathrm{k}, \mathrm{fic}}}{\mathrm{~S}_{\mathrm{n}}} \times \mathrm{P}_{\mathrm{st}, \text { fic }} \times \mathrm{T}_{\mathrm{p}}^{0,31}
$$

Voltage variation factor $\mathrm{ku}\left(\Psi_{\mathrm{k}}\right)$ :

$$
\mathrm{k}_{\mathrm{u}}\left(\Psi_{\mathrm{k}}\right)=\sqrt{3} \times \frac{\mathrm{U}_{\mathrm{fic}, \text { max }}-\mathrm{U}_{\mathrm{fic}, \text { min }}}{\mathrm{U}_{\mathrm{n}}} \times \frac{\mathrm{S}_{\mathrm{k}, \text { fic }}}{\mathrm{S}_{\mathrm{n}}}
$$

General specifications:

- PGU operation mode

Q setpoint = 0

- $S_{k, \text { fic }} / S_{n}$ 2.273
- Voltage range 230 V
- Grid frequency range

Used settings of the measurement device for switching operations measurement

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| DEWE2-A4 | $2019 / 12 / 24$, | 10 min values | 200 kHz |
|  | $2020 / 08 / 20$ |  |  |

The switching operations tests results are offered below with more detail.

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### 4.3.1.1 Test 1: Switch-on at $\mathbf{P}<10 \%$ Pn

Test conditions:

- $T_{p}=65 \mathrm{~s}$.
- Voltage output $=230 \mathrm{Vac}$

Results obtained from the test are offered at the table below.
Flicker factor and voltage change factor are determined for each record of measured voltage and measured current per phase according to the table below:

| Case of switching operation | Switch-on at $\mathrm{P}_{\text {available }}<10 \% \mathrm{P}_{\mathrm{n}}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Max, number of switching operations, $\mathbf{N}_{10}$ | 20 |  |  |  |
| Max, number of switching operations, $\mathbf{N}_{120}$ | 240 |  |  |  |
| Grid impedance angle | 30o․ | 50o․ | 70응 | 85응 |
| Flicker step factor, $\mathbf{k f}_{\mathbf{f}}\left(\Psi_{\mathrm{k}}\right)$ | 0.002 | 0.002 | 0.001 | 0.001 |
| Voltage change factor, $\mathrm{k}_{\mathrm{u}}\left(\Psi_{\mathrm{k}}\right)$ | 0.001 | 0.001 | 0.001 | 0.001 |

### 4.3.1.2 Test 2: Switch-on at $P=110 \%$ Pn

Test conditions:

- $\mathrm{T}_{\mathrm{p}}=65 \mathrm{~s}$.
- Voltage output $=230 \mathrm{Vac}$

Results obtained from the test are offered at the table below.
Flicker factor and voltage change factor are determined for each record of measured voltage and measured current per phase according to the table below:

| Case of switching operation | Switch-on at $\mathbf{P}_{\text {available }} \mathbf{P}=110 \% \mathbf{P n}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Max, number of switching operations, $\mathbf{N}_{10}$ | 20 |  |  |  |
| Max, number of switching operations, $\mathbf{N}_{120}$ |  |  |  |  |
| Grid impedance angle | $30^{\circ}$ | $50^{\circ}$ | $70^{\circ}$ | $85^{\circ}$ |
| Flicker step factor, $\mathbf{k}_{\mathbf{f}}\left(\Psi_{\mathbf{k}}\right)$ | 0.018 | 0.014 | 0.012 | 0.006 |
| Voltage change factor, $\mathbf{k}_{\mathbf{u}}\left(\Psi_{\mathbf{k}}\right)$ | 0.001 | 0.001 | 0.001 | 0.001 |

### 4.3.1.3 Test 3: Service shutdown $\mathrm{P}=110 \% \mathrm{Pn}$

Test conditions:

- $T_{p}=65 \mathrm{~s}$.
- Voltage output $=230 \mathrm{Vac}$

| Case of switching operation | Service shutdown P=110\%Pn |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Max, number of switching operations, $\mathbf{N}_{10}$ | 10 |  |  |  |
| Max, number of switching operations, $\mathbf{N}_{120}$ | 120 |  |  |  |
| Grid impedance angle | $30^{\circ}$ | $50^{\circ}$ | $70^{\circ}$ | $85^{\circ}$ |
| Flicker step factor, $\mathbf{k}_{\mathbf{f}}\left(\boldsymbol{\Psi}_{\mathbf{k}}\right)$ | 0.014 | 0.013 | 0.007 | 0.007 |
| Voltage change factor, $\mathbf{k u}(\boldsymbol{\Psi k})$ | 0.014 | 0.014 | 0.014 | 0.014 |


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| :---: | :---: | :---: |
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### 4.3.2 Flickers

The aim of this test is to determine the flicker coefficient c as a function of the grid impedance phase angle.

Test performed according point 4.3.3 of the standard. It applies to both PV and storage systems.
According to standard, it has been measured at least $12 \mathrm{P}_{\text {st }}$ in total between $0 \%-90 \%$ of $\mathrm{P}_{\mathrm{n}}$, at least one $P_{\text {st }}$ per $10 \%$ of $P_{n}$ and at least $3 P_{\text {st }}$ in total between $90 \%$ and $100 \% P_{n}$ per each phase and per each operation point. The power bins tested can be found on the table of results offered at this chapter of the test report.

The value of $S_{k, \text { fic }} / S_{n}$ used for the analysis has been 2.273 .

The flicker coefficient c $\left(\Psi_{\mathrm{k}}\right)$ is determinate per each flicker emission value $\mathrm{P}_{\mathrm{st}, \mathrm{fic}}$ :

$$
\mathrm{c}(\Psi \mathrm{k})=\operatorname{Pst}(\Psi \mathrm{k}) x \frac{S k}{S n}
$$

NOTE: According to Standard, the requirements for Flicker test are applicable at plant level, the results shown in this chapter are performed at inverter level. The results shown are informative.

Used settings of the measurement device for flicker measurement.

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| DEWE2-A4 | $2020 / 03 / 16$, | 10 min values | 200 kHz |
|  | $2020 / 03 / 17$, |  |  |
|  | $2020 / 08 / 20$ |  |  |

The conditions during testing are specified below:

- PGU operation mode $Q$ setpoint $=0$
- Voltage range

230 V

- Grid frequency range

50 Hz

- Voltage unbalance

Same conditions as point 4.3.4 of this test report (*) (Umbalance chapter)

- Date 2020/03/16 and 2020/03/17
- Measured period

Oh 10min 0 sec for each power bin
(*) As the test procedure for both tests is similar, representing the inverter working in continuous operation in a wide range of power bins, it is considered that the voltage unbalance conditions will be similar at both tests.

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The system flicker coefficient is the maximum value of all measurements, the following table shows the results obtained.

| Phase A |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Network impedance phase angle, $\boldsymbol{\Psi} \mathbf{k}$ | 30 | 50 | $\mathbf{o}$ | 70 | 85 |
| Average active power, P (\%Pn) | Flicker coefficient, C ( $\left.\Psi \mathrm{k}, \mathrm{P}_{\text {bin }}\right)$ |  |  |  |  |
| $\mathbf{0}$ | 0.041 | 0.041 | 0.041 | 0.041 |  |
| $\mathbf{1 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |  |
| $\mathbf{2 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |  |
| $\mathbf{3 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |  |
| $\mathbf{4 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |  |
| $\mathbf{5 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |  |
| $\mathbf{6 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |  |
| $\mathbf{7 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |  |
| $\mathbf{8 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |  |
| $\mathbf{9 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |  |
| $\mathbf{1 0 0}$ | 0.055 | 0.067 | 0.077 | 0.080 |  |
| $\mathbf{1 1 0}$ | 0.064 | 0.054 | 0.074 | 0.080 |  |


| Phase B |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Network impedance phase angle, $\boldsymbol{\Psi k}$ | $30^{\circ}$ | $500^{\circ}$ | 700 | 850 |
| Average active power, P (\%Pn) | Flicker coefficient, C ( $\left.\Psi \mathrm{k}, \mathrm{P}_{\text {bin }}\right)$ |  |  |  |
| $\mathbf{0}$ | 0.041 | 0.041 | 0.041 | 0.041 |
| $\mathbf{1 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |
| $\mathbf{2 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |
| $\mathbf{3 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |
| $\mathbf{4 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |
| $\mathbf{5 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |
| $\mathbf{6 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |
| $\mathbf{7 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |
| $\mathbf{8 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |
| $\mathbf{9 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |
| $\mathbf{1 0 0}$ | 0.055 | 0.067 | 0.076 | 0.079 |
| $\mathbf{1 1 0}$ | 0.049 | 0.066 | 0.076 | 0.079 |


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| Phase C |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Network impedance phase angle, $\boldsymbol{\Psi k}$ | $30^{\circ}$ | $500^{\circ}$ | $70^{\circ}$ | 850 |
| Average active power, P (\%Pn) | Flicker coefficient, C $\left(\Psi \mathrm{k}, \mathrm{P}_{\text {bin }}\right)$ |  |  |  |
| $\mathbf{0}$ | 0.041 | 0.041 | 0.041 | 0.041 |
| $\mathbf{1 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |
| $\mathbf{2 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |
| $\mathbf{3 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |
| $\mathbf{4 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |
| $\mathbf{5 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |
| $\mathbf{6 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |
| $\mathbf{7 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |
| $\mathbf{8 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |
| $\mathbf{9 0}$ | 0.041 | 0.041 | 0.041 | 0.041 |
| $\mathbf{1 0 0}$ | 0.057 | 0.069 | 0.077 | 0.080 |
| $\mathbf{1 1 0}$ | 0.057 | 0.069 | 0.071 | 0.074 |


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| :---: | :---: | :---: |

### 4.3.3 Harmonic

The aim of this test is to determine relevant values for PGU continuous operation.
Test performed according to point 4.3.4 of the standard. It can be applied at both PV and storage systems.
The reactive power setpoint is 0 VAr , the harmonics have been measured 10 minutes average values of line current, at least three records consisting of 3-phase measurements.
They have been verified limits at different power levels, from $10 \% \mathrm{Pn}$ to $100 \% \mathrm{Pn}$, in $10 \% \mathrm{Pn}$ steps.
The arithmetic average is formed over the 10 minutes record for each harmonic, interharmonic and higher frequency component of the current.

The total distortion of the current harmonics (TDC) has been calculated according to standard:

$$
\mathrm{TDC}=\frac{\sqrt{\sum_{h=2}^{50} I_{h}^{2}}}{I_{\mathrm{n}}} \cdot 100
$$

See point 2.6 (Definitions) of this report.
The total distortion of the voltage harmonics (TDD) has been determined using the same procedure.
NOTE: According to Standard, the requirements for Harmonics test are applicable at plant level, the results shown in this chapter are performed at inverter level. The results shown are informative.

Used settings of the measurement device for harmonic measurement.

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| PA3000 | $2019 / 12 / 04$ | 100 ms values | 10 kHz |
| PA5000H | $2020 / 4 / 13,2020 / 4 / 14$, <br> $2020 / 8 / 19$ | 100 ms values | 10 kHz |

- PGU operation mode; Q (VAr)
- Voltage range (V)
- Voltage unbalance
- Measured period (min)

Q setpoint $=0 \mathrm{VAr}$
230 V
Same conditions as point 4.3.4 of this test report (*) (Umbalace Chapter)
3 min each active power level
(*) As the test procedure for both tests is similar, representing the inverter working in continuous operation $^{*}$ in a wide range of power bins, it is considered that the voltage unbalance conditions will be similar at both tests.

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| Power bin (\%Pn) | Number of <br> records |
| :---: | :---: |
| $0 \%$ | 1 |
| $10 \%$ | 1 |
| $20 \%$ | 1 |
| $30 \%$ | 1 |
| $40 \%$ | 1 |
| $50 \%$ | 1 |
| $60 \%$ | 1 |
| $70 \%$ | 1 |
| $80 \%$ | 1 |
| $90 \%$ | 1 |
| $100 \%$ | 1 |
| $110 \%$ | 1 |


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| :---: | :---: | :---: |

## FGW-TG3+SP1

### 4.3.3.1 Current harmonics

| Phase A |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{P}_{\mathrm{n}}$ (\%) | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 | 110 | Max <br> (\%) |
| Nr./ Order | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}$ (\%) | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ |  |
| 2 | 0.031 | 0.035 | 0.029 | 0.041 | 0.040 | 0.034 | 0.052 | 0.036 | 0.043 | 0.094 | 0.046 | 0.056 | 0.094 |
| 3 | 0.086 | 0.055 | 0.043 | 0.042 | 0.044 | 0.034 | 0.046 | 0.010 | 0.029 | 0.079 | 0.021 | 0.047 | 0.086 |
| 4 | 0.019 | 0.030 | 0.011 | 0.010 | 0.040 | 0.008 | 0.011 | 0.035 | 0.039 | 0.053 | 0.115 | 0.045 | 0.115 |
| 5 | 0.554 | 0.173 | 0.067 | 0.189 | 0.315 | 0.383 | 0.393 | 0.380 | 0.387 | 0.409 | 0.415 | 0.358 | 0.554 |
| 6 | 0.003 | 0.010 | 0.006 | 0.021 | 0.011 | 0.020 | 0.026 | 0.014 | 0.016 | 0.020 | 0.021 | 0.042 | 0.042 |
| 7 | 0.176 | 0.197 | 0.071 | 0.153 | 0.288 | 0.344 | 0.379 | 0.373 | 0.411 | 0.424 | 0.510 | 0.135 | 0.510 |
| 8 | 0.015 | 0.011 | 0.010 | 0.019 | 0.008 | 0.019 | 0.020 | 0.006 | 0.007 | 0.011 | 0.069 | 0.047 | 0.069 |
| 9 | 0.033 | 0.003 | 0.034 | 0.019 | 0.014 | 0.029 | 0.033 | 0.042 | 0.036 | 0.044 | 0.024 | 0.074 | 0.074 |
| 10 | 0.015 | 0.006 | 0.007 | 0.012 | 0.005 | 0.008 | 0.004 | 0.011 | 0.006 | 0.010 | 0.033 | 0.042 | 0.042 |
| 11 | 0.469 | 0.257 | 0.071 | 0.113 | 0.198 | 0.241 | 0.258 | 0.272 | 0.288 | 0.287 | 0.324 | 0.255 | 0.469 |
| 12 | 0.017 | 0.009 | 0.013 | 0.014 | 0.022 | 0.015 | 0.019 | 0.011 | 0.022 | 0.021 | 0.004 | 0.025 | 0.025 |
| 13 | 0.181 | 0.186 | 0.091 | 0.110 | 0.204 | 0.249 | 0.260 | 0.262 | 0.279 | 0.296 | 0.288 | 0.107 | 0.296 |
| 14 | 0.029 | 0.006 | 0.006 | 0.004 | 0.005 | 0.005 | 0.006 | 0.006 | 0.007 | 0.012 | 0.020 | 0.033 | 0.033 |
| 15 | 0.012 | 0.030 | 0.013 | 0.011 | 0.018 | 0.005 | 0.010 | 0.006 | 0.010 | 0.021 | 0.026 | 0.073 | 0.073 |
| 16 | 0.017 | 0.002 | 0.006 | 0.001 | 0.003 | 0.005 | 0.008 | 0.006 | 0.004 | 0.006 | 0.012 | 0.034 | 0.034 |
| 17 | 0.159 | 0.091 | 0.081 | 0.029 | 0.053 | 0.072 | 0.080 | 0.075 | 0.074 | 0.068 | 0.048 | 0.190 | 0.190 |
| 18 | 0.017 | 0.003 | 0.000 | 0.007 | 0.005 | 0.003 | 0.006 | 0.006 | 0.006 | 0.006 | 0.009 | 0.017 | 0.017 |
| 19 | 0.145 | 0.034 | 0.066 | 0.024 | 0.057 | 0.073 | 0.078 | 0.081 | 0.092 | 0.082 | 0.077 | 0.180 | 0.180 |
| 20 | 0.019 | 0.002 | 0.002 | 0.002 | 0.003 | 0.001 | 0.004 | 0.004 | 0.001 | 0.003 | 0.010 | 0.024 | 0.024 |
| 21 | 0.001 | 0.020 | 0.006 | 0.002 | 0.004 | 0.006 | 0.008 | 0.002 | 0.012 | 0.013 | 0.001 | 0.054 | 0.054 |
| 22 | 0.014 | 0.001 | 0.004 | 0.001 | 0.002 | 0.004 | 0.001 | 0.003 | 0.003 | 0.003 | 0.004 | 0.030 | 0.030 |
| 23 | 0.072 | 0.056 | 0.056 | 0.032 | 0.041 | 0.063 | 0.069 | 0.066 | 0.073 | 0.077 | 0.080 | 0.141 | 0.141 |
| 24 | 0.017 | 0.002 | 0.010 | 0.005 | 0.016 | 0.010 | 0.003 | 0.010 | 0.002 | 0.007 | 0.002 | 0.012 | 0.017 |
| 25 | 0.102 | 0.068 | 0.032 | 0.037 | 0.049 | 0.070 | 0.069 | 0.061 | 0.067 | 0.070 | 0.068 | 0.185 | 0.185 |
| 26 | 0.016 | 0.002 | 0.004 | 0.003 | 0.001 | 0.001 | 0.003 | 0.001 | 0.001 | 0.003 | 0.003 | 0.017 | 0.017 |
| 27 | 0.005 | 0.010 | 0.002 | 0.001 | 0.007 | 0.006 | 0.007 | 0.005 | 0.008 | 0.005 | 0.003 | 0.046 | 0.046 |
| 28 | 0.005 | 0.002 | 0.000 | 0.001 | 0.003 | 0.002 | 0.001 | 0.002 | 0.001 | 0.001 | 0.002 | 0.029 | 0.029 |
| 29 | 0.035 | 0.053 | 0.015 | 0.031 | 0.032 | 0.051 | 0.047 | 0.043 | 0.041 | 0.035 | 0.034 | 0.084 | 0.084 |
| 30 | 0.013 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.006 | 0.006 | 0.002 | 0.005 | 0.004 | 0.012 | 0.013 |
| 31 | 0.064 | 0.043 | 0.006 | 0.036 | 0.035 | 0.054 | 0.052 | 0.052 | 0.055 | 0.053 | 0.050 | 0.174 | 0.174 |
| 32 | 0.010 | 0.002 | 0.002 | 0.001 | 0.001 | 0.002 | 0.002 | 0.000 | 0.001 | 0.002 | 0.002 | 0.013 | 0.013 |
| 33 | 0.007 | 0.012 | 0.005 | 0.004 | 0.004 | 0.009 | 0.006 | 0.006 | 0.011 | 0.010 | 0.010 | 0.030 | 0.030 |
| 34 | 0.006 | 0.005 | 0.004 | 0.002 | 0.003 | 0.002 | 0.003 | 0.002 | 0.001 | 0.001 | 0.003 | 0.034 | 0.034 |
| 35 | 0.023 | 0.012 | 0.022 | 0.031 | 0.021 | 0.039 | 0.042 | 0.043 | 0.039 | 0.041 | 0.037 | 0.063 | 0.063 |
| 36 | 0.013 | 0.001 | 0.002 | 0.001 | 0.004 | 0.005 | 0.002 | 0.001 | 0.001 | 0.002 | 0.002 | 0.012 | 0.013 |
| 37 | 0.047 | 0.013 | 0.024 | 0.030 | 0.029 | 0.044 | 0.041 | 0.038 | 0.042 | 0.034 | 0.031 | 0.135 | 0.135 |
| 38 | 0.013 | 0.004 | 0.001 | 0.000 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.002 | 0.000 | 0.011 | 0.013 |
| 39 | 0.005 | 0.003 | 0.003 | 0.003 | 0.006 | 0.005 | 0.004 | 0.004 | 0.005 | 0.005 | 0.004 | 0.020 | 0.020 |
| 40 | 0.002 | 0.003 | 0.004 | 0.003 | 0.006 | 0.004 | 0.007 | 0.005 | 0.004 | 0.005 | 0.004 | 0.033 | 0.033 |
| 41 | 0.014 | 0.037 | 0.031 | 0.030 | 0.021 | 0.036 | 0.038 | 0.035 | 0.030 | 0.029 | 0.029 | 0.047 | 0.047 |
| 42 | 0.011 | 0.002 | 0.001 | 0.001 | 0.004 | 0.002 | 0.003 | 0.002 | 0.002 | 0.003 | 0.003 | 0.013 | 0.013 |
| 43 | 0.033 | 0.049 | 0.028 | 0.030 | 0.021 | 0.039 | 0.039 | 0.041 | 0.046 | 0.047 | 0.040 | 0.109 | 0.109 |
| 44 | 0.011 | 0.001 | 0.001 | 0.001 | 0.003 | 0.001 | 0.002 | 0.001 | 0.002 | 0.002 | 0.002 | 0.016 | 0.016 |
| 45 | 0.005 | 0.006 | 0.003 | 0.003 | 0.006 | 0.003 | 0.004 | 0.002 | 0.006 | 0.006 | 0.007 | 0.018 | 0.018 |
| 46 | 0.008 | 0.003 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.001 | 0.003 | 0.002 | 0.003 | 0.051 | 0.051 |
| 47 | 0.015 | 0.043 | 0.027 | 0.027 | 0.012 | 0.029 | 0.032 | 0.038 | 0.037 | 0.036 | 0.037 | 0.054 | 0.054 |
| 48 | 0.008 | 0.002 | 0.001 | 0.002 | 0.004 | 0.001 | 0.002 | 0.003 | 0.001 | 0.001 | 0.003 | 0.047 | 0.047 |
| 49 | 0.024 | 0.037 | 0.014 | 0.022 | 0.025 | 0.041 | 0.035 | 0.031 | 0.036 | 0.032 | 0.030 | 0.085 | 0.085 |
| 50 | 0.011 | 0.003 | 0.002 | 0.000 | 0.001 | 0.001 | 0.001 | 0.001 | 0.003 | 0.001 | 0.003 | 0.022 | 0.022 |
| $\begin{aligned} & \text { TDC } \\ & \text { (\%) } \end{aligned}$ | 0.678 | 0.206 | 0.047 | 0.100 | 0.286 | 0.424 | 0.476 | 0.464 | 0.524 | 0.573 | 0.675 | 0.474 | 0.678 |


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| Phase B |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{P}_{\mathrm{n}}$ (\%) | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 | 110 |  |
| Nr./ Order | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{n}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{n}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | (\%) |
| 2 | 0.030 | 0.026 | 0.018 | 0.038 | 0.043 | 0.041 | 0.051 | 0.036 | 0.012 | 0.030 | 0.037 | 0.057 | 0.057 |
| 3 | 0.017 | 0.016 | 0.018 | 0.042 | 0.086 | 0.070 | 0.050 | 0.069 | 0.087 | 0.125 | 0.110 | 0.041 | 0.125 |
| 4 | 0.016 | 0.023 | 0.011 | 0.007 | 0.020 | 0.007 | 0.010 | 0.013 | 0.019 | 0.033 | 0.088 | 0.038 | 0.088 |
| 5 | 0.614 | 0.196 | 0.075 | 0.151 | 0.269 | 0.267 | 0.303 | 0.271 | 0.297 | 0.313 | 0.304 | 0.277 | 0.614 |
| 6 | 0.018 | 0.010 | 0.005 | 0.012 | 0.006 | 0.008 | 0.013 | 0.021 | 0.014 | 0.022 | 0.011 | 0.049 | 0.049 |
| 7 | 0.179 | 0.165 | 0.039 | 0.132 | 0.267 | 0.312 | 0.327 | 0.321 | 0.357 | 0.402 | 0.410 | 0.134 | 0.410 |
| 8 | 0.017 | 0.013 | 0.007 | 0.006 | 0.006 | 0.006 | 0.002 | 0.010 | 0.007 | 0.012 | 0.022 | 0.040 | 0.040 |
| 9 | 0.016 | 0.046 | 0.021 | 0.031 | 0.032 | 0.029 | 0.042 | 0.034 | 0.045 | 0.039 | 0.045 | 0.038 | 0.046 |
| 10 | 0.020 | 0.011 | 0.008 | 0.012 | 0.020 | 0.022 | 0.019 | 0.026 | 0.014 | 0.025 | 0.003 | 0.032 | 0.032 |
| 11 | 0.426 | 0.215 | 0.117 | 0.131 | 0.235 | 0.266 | 0.267 | 0.279 | 0.289 | 0.299 | 0.325 | 0.183 | 0.426 |
| 12 | 0.029 | 0.002 | 0.009 | 0.010 | 0.015 | 0.011 | 0.014 | 0.009 | 0.011 | 0.010 | 0.002 | 0.038 | 0.038 |
| 13 | 0.172 | 0.165 | 0.097 | 0.085 | 0.175 | 0.213 | 0.214 | 0.223 | 0.245 | 0.271 | 0.260 | 0.061 | 0.271 |
| 14 | 0.023 | 0.007 | 0.003 | 0.011 | 0.014 | 0.014 | 0.012 | 0.018 | 0.009 | 0.014 | 0.013 | 0.027 | 0.027 |
| 15 | 0.010 | 0.010 | 0.004 | 0.013 | 0.022 | 0.033 | 0.039 | 0.031 | 0.037 | 0.051 | 0.044 | 0.026 | 0.051 |
| 16 | 0.013 | 0.001 | 0.008 | 0.006 | 0.005 | 0.003 | 0.008 | 0.007 | 0.003 | 0.004 | 0.013 | 0.021 | 0.021 |
| 17 | 0.143 | 0.090 | 0.079 | 0.036 | 0.063 | 0.065 | 0.067 | 0.075 | 0.066 | 0.054 | 0.062 | 0.121 | 0.143 |
| 18 | 0.026 | 0.001 | 0.001 | 0.004 | 0.004 | 0.003 | 0.006 | 0.005 | 0.002 | 0.003 | 0.003 | 0.025 | 0.026 |
| 19 | 0.157 | 0.046 | 0.070 | 0.025 | 0.059 | 0.064 | 0.063 | 0.071 | 0.080 | 0.070 | 0.058 | 0.159 | 0.159 |
| 20 | 0.019 | 0.001 | 0.003 | 0.004 | 0.003 | 0.003 | 0.004 | 0.004 | 0.002 | 0.002 | 0.001 | 0.022 | 0.022 |
| 21 | 0.003 | 0.011 | 0.004 | 0.004 | 0.004 | 0.007 | 0.016 | 0.011 | 0.012 | 0.008 | 0.010 | 0.017 | 0.017 |
| 22 | 0.011 | 0.004 | 0.005 | 0.004 | 0.006 | 0.001 | 0.003 | 0.010 | 0.004 | 0.004 | 0.004 | 0.018 | 0.018 |
| 23 | 0.066 | 0.060 | 0.046 | 0.031 | 0.049 | 0.064 | 0.056 | 0.061 | 0.074 | 0.072 | 0.078 | 0.089 | 0.089 |
| 24 | 0.020 | 0.004 | 0.004 | 0.001 | 0.007 | 0.003 | 0.006 | 0.004 | 0.002 | 0.003 | 0.004 | 0.016 | 0.020 |
| 25 | 0.104 | 0.057 | 0.036 | 0.034 | 0.043 | 0.056 | 0.050 | 0.049 | 0.047 | 0.051 | 0.056 | 0.182 | 0.182 |
| 26 | 0.018 | 0.005 | 0.005 | 0.006 | 0.005 | 0.004 | 0.002 | 0.004 | 0.001 | 0.001 | 0.003 | 0.015 | 0.018 |
| 27 | 0.002 | 0.005 | 0.002 | 0.007 | 0.011 | 0.013 | 0.016 | 0.014 | 0.023 | 0.020 | 0.014 | 0.017 | 0.023 |
| 28 | 0.009 | 0.003 | 0.002 | 0.003 | 0.002 | 0.004 | 0.004 | 0.004 | 0.002 | 0.005 | 0.005 | 0.024 | 0.024 |
| 29 | 0.027 | 0.065 | 0.013 | 0.037 | 0.041 | 0.052 | 0.043 | 0.043 | 0.036 | 0.032 | 0.037 | 0.043 | 0.065 |
| 30 | 0.016 | 0.000 | 0.003 | 0.002 | 0.004 | 0.003 | 0.001 | 0.003 | 0.003 | 0.003 | 0.004 | 0.012 | 0.016 |
| 31 | 0.069 | 0.050 | 0.012 | 0.032 | 0.031 | 0.044 | 0.042 | 0.044 | 0.045 | 0.038 | 0.041 | 0.174 | 0.174 |
| 32 | 0.013 | 0.004 | 0.003 | 0.002 | 0.005 | 0.003 | 0.004 | 0.004 | 0.004 | 0.002 | 0.002 | 0.011 | 0.013 |
| 33 | 0.005 | 0.011 | 0.009 | 0.007 | 0.013 | 0.009 | 0.009 | 0.009 | 0.006 | 0.012 | 0.012 | 0.021 | 0.021 |
| 34 | 0.010 | 0.004 | 0.006 | 0.002 | 0.005 | 0.001 | 0.004 | 0.005 | 0.004 | 0.003 | 0.004 | 0.030 | 0.030 |
| 35 | 0.014 | 0.016 | 0.016 | 0.031 | 0.027 | 0.037 | 0.034 | 0.041 | 0.046 | 0.041 | 0.036 | 0.041 | 0.046 |
| 36 | 0.015 | 0.003 | 0.003 | 0.001 | 0.003 | 0.001 | 0.002 | 0.001 | 0.000 | 0.001 | 0.002 | 0.011 | 0.015 |
| 37 | 0.046 | 0.018 | 0.021 | 0.031 | 0.028 | 0.036 | 0.035 | 0.036 | 0.032 | 0.027 | 0.023 | 0.139 | 0.139 |
| 38 | 0.014 | 0.002 | 0.002 | 0.001 | 0.003 | 0.002 | 0.003 | 0.004 | 0.002 | 0.002 | 0.002 | 0.012 | 0.014 |
| 39 | 0.003 | 0.004 | 0.005 | 0.002 | 0.009 | 0.007 | 0.009 | 0.005 | 0.010 | 0.008 | 0.002 | 0.026 | 0.026 |
| 40 | 0.010 | 0.004 | 0.005 | 0.002 | 0.003 | 0.005 | 0.008 | 0.009 | 0.005 | 0.003 | 0.004 | 0.028 | 0.028 |
| 41 | 0.006 | 0.040 | 0.023 | 0.029 | 0.026 | 0.037 | 0.032 | 0.032 | 0.032 | 0.030 | 0.027 | 0.040 | 0.040 |
| 42 | 0.014 | 0.002 | 0.001 | 0.001 | 0.003 | 0.000 | 0.002 | 0.001 | 0.001 | 0.001 | 0.002 | 0.013 | 0.014 |
| 43 | 0.036 | 0.047 | 0.031 | 0.029 | 0.021 | 0.032 | 0.032 | 0.040 | 0.037 | 0.034 | 0.035 | 0.111 | 0.111 |
| 44 | 0.016 | 0.001 | 0.001 | 0.002 | 0.005 | 0.002 | 0.003 | 0.002 | 0.002 | 0.001 | 0.001 | 0.019 | 0.019 |
| 45 | 0.005 | 0.006 | 0.004 | 0.002 | 0.010 | 0.008 | 0.008 | 0.006 | 0.012 | 0.008 | 0.010 | 0.025 | 0.025 |
| 46 | 0.012 | 0.002 | 0.002 | 0.002 | 0.005 | 0.004 | 0.005 | 0.004 | 0.004 | 0.002 | 0.005 | 0.050 | 0.050 |
| 47 | 0.005 | 0.044 | 0.023 | 0.028 | 0.018 | 0.031 | 0.032 | 0.039 | 0.039 | 0.037 | 0.036 | 0.051 | 0.051 |
| 48 | 0.013 | 0.003 | 0.002 | 0.002 | 0.002 | 0.001 | 0.003 | 0.002 | 0.000 | 0.002 | 0.003 | 0.046 | 0.046 |
| 49 | 0.026 | 0.034 | 0.019 | 0.024 | 0.024 | 0.033 | 0.033 | 0.032 | 0.027 | 0.024 | 0.026 | 0.090 | 0.090 |
| 50 | 0.014 | 0.001 | 0.003 | 0.002 | 0.003 | 0.002 | 0.002 | 0.003 | 0.001 | 0.003 | 0.004 | 0.026 | 0.026 |
| TDC <br> (\%) | 0.698 | 0.175 | 0.050 | 0.081 | 0.260 | 0.322 | 0.351 | 0.344 | 0.402 | 0.470 | 0.486 | 0.320 | 0.698 |


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|  | FGW-TG3+SP1 |  |

## FGW-TG3+SP1

| Phase C |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{P}_{\mathrm{n}}$ (\%) | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 | 110 |  |
| Nr./ Order | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | (\%) |
| 2 | 0.008 | 0.022 | 0.021 | 0.013 | 0.046 | 0.024 | 0.040 | 0.047 | 0.029 | 0.086 | 0.010 | 0.027 | 0.086 |
| 3 | 0.100 | 0.038 | 0.037 | 0.073 | 0.079 | 0.090 | 0.104 | 0.089 | 0.085 | 0.103 | 0.102 | 0.081 | 0.104 |
| 4 | 0.006 | 0.016 | 0.013 | 0.005 | 0.027 | 0.004 | 0.008 | 0.034 | 0.042 | 0.064 | 0.075 | 0.029 | 0.075 |
| 5 | 0.577 | 0.206 | 0.028 | 0.089 | 0.201 | 0.266 | 0.276 | 0.302 | 0.314 | 0.312 | 0.298 | 0.307 | 0.577 |
| 6 | 0.016 | 0.008 | 0.005 | 0.011 | 0.014 | 0.014 | 0.013 | 0.026 | 0.010 | 0.014 | 0.013 | 0.037 | 0.037 |
| 7 | 0.184 | 0.163 | 0.074 | 0.121 | 0.255 | 0.288 | 0.327 | 0.321 | 0.371 | 0.388 | 0.462 | 0.085 | 0.462 |
| 8 | 0.005 | 0.008 | 0.010 | 0.012 | 0.013 | 0.018 | 0.020 | 0.013 | 0.007 | 0.018 | 0.048 | 0.034 | 0.048 |
| 9 | 0.030 | 0.043 | 0.025 | 0.046 | 0.042 | 0.050 | 0.028 | 0.035 | 0.015 | 0.006 | 0.049 | 0.100 | 0.100 |
| 10 | 0.008 | 0.010 | 0.015 | 0.020 | 0.016 | 0.022 | 0.021 | 0.016 | 0.019 | 0.031 | 0.030 | 0.028 | 0.031 |
| 11 | 0.483 | 0.225 | 0.102 | 0.088 | 0.198 | 0.238 | 0.276 | 0.275 | 0.298 | 0.330 | 0.351 | 0.209 | 0.483 |
| 12 | 0.012 | 0.005 | 0.004 | 0.005 | 0.008 | 0.005 | 0.005 | 0.002 | 0.013 | 0.012 | 0.004 | 0.026 | 0.026 |
| 13 | 0.178 | 0.176 | 0.094 | 0.096 | 0.191 | 0.230 | 0.229 | 0.239 | 0.243 | 0.246 | 0.262 | 0.101 | 0.262 |
| 14 | 0.012 | 0.004 | 0.009 | 0.011 | 0.012 | 0.010 | 0.015 | 0.011 | 0.011 | 0.013 | 0.008 | 0.026 | 0.026 |
| 15 | 0.004 | 0.022 | 0.006 | 0.020 | 0.030 | 0.029 | 0.031 | 0.034 | 0.027 | 0.026 | 0.017 | 0.083 | 0.083 |
| 16 | 0.003 | 0.002 | 0.005 | 0.007 | 0.003 | 0.005 | 0.002 | 0.004 | 0.004 | 0.010 | 0.002 | 0.023 | 0.023 |
| 17 | 0.154 | 0.084 | 0.089 | 0.044 | 0.075 | 0.086 | 0.096 | 0.101 | 0.093 | 0.066 | 0.067 | 0.156 | 0.156 |
| 18 | 0.010 | 0.004 | 0.001 | 0.004 | 0.002 | 0.001 | 0.002 | 0.001 | 0.004 | 0.003 | 0.006 | 0.019 | 0.019 |
| 19 | 0.157 | 0.055 | 0.067 | 0.028 | 0.056 | 0.069 | 0.071 | 0.080 | 0.074 | 0.071 | 0.063 | 0.194 | 0.194 |
| 20 | 0.012 | 0.003 | 0.002 | 0.004 | 0.006 | 0.003 | 0.006 | 0.007 | 0.002 | 0.003 | 0.009 | 0.021 | 0.021 |
| 21 | 0.007 | 0.012 | 0.011 | 0.005 | 0.006 | 0.005 | 0.002 | 0.006 | 0.010 | 0.009 | 0.014 | 0.077 | 0.077 |
| 22 | 0.003 | 0.005 | 0.002 | 0.004 | 0.005 | 0.006 | 0.004 | 0.008 | 0.002 | 0.003 | 0.002 | 0.026 | 0.026 |
| 23 | 0.073 | 0.046 | 0.052 | 0.034 | 0.050 | 0.068 | 0.070 | 0.070 | 0.084 | 0.086 | 0.088 | 0.111 | 0.111 |
| 24 | 0.012 | 0.005 | 0.006 | 0.003 | 0.009 | 0.006 | 0.005 | 0.008 | 0.001 | 0.003 | 0.003 | 0.015 | 0.015 |
| 25 | 0.105 | 0.074 | 0.033 | 0.034 | 0.042 | 0.054 | 0.063 | 0.061 | 0.057 | 0.054 | 0.057 | 0.205 | 0.205 |
| 26 | 0.012 | 0.005 | 0.002 | 0.005 | 0.003 | 0.002 | 0.003 | 0.004 | 0.004 | 0.004 | 0.001 | 0.017 | 0.017 |
| 27 | 0.004 | 0.004 | 0.004 | 0.004 | 0.007 | 0.007 | 0.009 | 0.008 | 0.011 | 0.004 | 0.010 | 0.051 | 0.051 |
| 28 | 0.005 | 0.005 | 0.003 | 0.005 | 0.002 | 0.001 | 0.003 | 0.003 | 0.002 | 0.004 | 0.005 | 0.028 | 0.028 |
| 29 | 0.031 | 0.063 | 0.013 | 0.038 | 0.043 | 0.055 | 0.055 | 0.056 | 0.048 | 0.038 | 0.043 | 0.065 | 0.065 |
| 30 | 0.013 | 0.004 | 0.002 | 0.001 | 0.001 | 0.002 | 0.002 | 0.001 | 0.001 | 0.004 | 0.002 | 0.014 | 0.014 |
| 31 | 0.075 | 0.046 | 0.014 | 0.033 | 0.030 | 0.047 | 0.051 | 0.054 | 0.047 | 0.043 | 0.042 | 0.188 | 0.188 |
| 32 | 0.013 | 0.002 | 0.003 | 0.003 | 0.004 | 0.005 | 0.003 | 0.004 | 0.005 | 0.001 | 0.004 | 0.015 | 0.015 |
| 33 | 0.010 | 0.007 | 0.003 | 0.002 | 0.006 | 0.010 | 0.011 | 0.010 | 0.006 | 0.019 | 0.016 | 0.035 | 0.035 |
| 34 | 0.006 | 0.002 | 0.001 | 0.002 | 0.004 | 0.003 | 0.002 | 0.001 | 0.001 | 0.006 | 0.001 | 0.033 | 0.033 |
| 35 | 0.018 | 0.021 | 0.018 | 0.035 | 0.030 | 0.043 | 0.048 | 0.049 | 0.052 | 0.044 | 0.047 | 0.039 | 0.052 |
| 36 | 0.011 | 0.003 | 0.002 | 0.001 | 0.004 | 0.002 | 0.002 | 0.002 | 0.002 | 0.003 | 0.003 | 0.013 | 0.013 |
| 37 | 0.052 | 0.016 | 0.026 | 0.031 | 0.025 | 0.038 | 0.037 | 0.034 | 0.030 | 0.031 | 0.029 | 0.147 | 0.147 |
| 38 | 0.015 | 0.005 | 0.004 | 0.001 | 0.004 | 0.002 | 0.002 | 0.003 | 0.005 | 0.001 | 0.004 | 0.014 | 0.015 |
| 39 | 0.003 | 0.003 | 0.002 | 0.003 | 0.002 | 0.003 | 0.006 | 0.006 | 0.005 | 0.006 | 0.007 | 0.028 | 0.028 |
| 40 | 0.008 | 0.004 | 0.003 | 0.004 | 0.002 | 0.007 | 0.003 | 0.002 | 0.000 | 0.003 | 0.003 | 0.032 | 0.032 |
| 41 | 0.012 | 0.044 | 0.026 | 0.031 | 0.031 | 0.041 | 0.041 | 0.040 | 0.040 | 0.033 | 0.035 | 0.028 | 0.044 |
| 42 | 0.017 | 0.004 | 0.001 | 0.000 | 0.002 | 0.003 | 0.002 | 0.001 | 0.002 | 0.001 | 0.005 | 0.015 | 0.017 |
| 43 | 0.040 | 0.043 | 0.031 | 0.029 | 0.013 | 0.031 | 0.035 | 0.043 | 0.039 | 0.037 | 0.038 | 0.117 | 0.117 |
| 44 | 0.015 | 0.002 | 0.002 | 0.000 | 0.003 | 0.002 | 0.001 | 0.003 | 0.002 | 0.003 | 0.001 | 0.020 | 0.020 |
| 45 | 0.004 | 0.002 | 0.004 | 0.002 | 0.004 | 0.005 | 0.003 | 0.006 | 0.008 | 0.008 | 0.004 | 0.020 | 0.020 |
| 46 | 0.004 | 0.004 | 0.001 | 0.001 | 0.005 | 0.002 | 0.001 | 0.003 | 0.002 | 0.004 | 0.004 | 0.051 | 0.051 |
| 47 | 0.012 | 0.046 | 0.024 | 0.029 | 0.022 | 0.034 | 0.040 | 0.046 | 0.049 | 0.038 | 0.042 | 0.049 | 0.049 |
| 48 | 0.017 | 0.002 | 0.001 | 0.001 | 0.004 | 0.001 | 0.002 | 0.000 | 0.001 | 0.002 | 0.004 | 0.048 | 0.048 |
| 49 | 0.028 | 0.033 | 0.016 | 0.022 | 0.016 | 0.032 | 0.034 | 0.032 | 0.028 | 0.028 | 0.026 | 0.094 | 0.094 |
| 50 | 0.013 | 0.002 | 0.001 | 0.002 | 0.003 | 0.003 | 0.002 | 0.002 | 0.002 | 0.002 | 0.001 | 0.024 | 0.024 |
| $\begin{aligned} & \hline \text { TDC } \\ & (\%) \end{aligned}$ | 0.723 | 0.187 | 0.049 | 0.061 | 0.214 | 0.310 | 0.366 | 0.383 | 0.435 | 0.474 | 0.549 | 0.413 | 0.723 |






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### 4.3.3.2 Voltage harmonics

Measurements of voltage harmonics at continuous operation are done according to IEC 61000-4-7:2002

| Phase A |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{P}_{\mathrm{n}}$ (\%) | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 | 110 |  |
| Nr./ Order | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | (\%) |
| 2 | 0.001 | 0.012 | 0.020 | 0.019 | 0.022 | 0.014 | 0.009 | 0.005 | 0.019 | 0.012 | 0.004 | 0.020 | 0.022 |
| 3 | 0.014 | 0.021 | 0.032 | 0.018 | 0.081 | 0.128 | 0.162 | 0.226 | 0.250 | 0.284 | 0.288 | 0.137 | 0.288 |
| 4 | 0.003 | 0.005 | 0.003 | 0.009 | 0.016 | 0.013 | 0.019 | 0.014 | 0.015 | 0.017 | 0.024 | 0.021 | 0.024 |
| 5 | 0.105 | 0.016 | 0.018 | 0.058 | 0.087 | 0.072 | 0.046 | 0.009 | 0.013 | 0.036 | 0.047 | 0.033 | 0.105 |
| 6 | 0.005 | 0.005 | 0.006 | 0.007 | 0.000 | 0.010 | 0.017 | 0.011 | 0.016 | 0.015 | 0.014 | 0.018 | 0.018 |
| 7 | 0.048 | 0.050 | 0.012 | 0.024 | 0.091 | 0.115 | 0.117 | 0.101 | 0.093 | 0.075 | 0.084 | 0.041 | 0.117 |
| 8 | 0.007 | 0.002 | 0.004 | 0.001 | 0.006 | 0.004 | 0.009 | 0.009 | 0.013 | 0.014 | 0.029 | 0.014 | 0.029 |
| 9 | 0.008 | 0.004 | 0.017 | 0.004 | 0.006 | 0.031 | 0.046 | 0.056 | 0.044 | 0.027 | 0.015 | 0.034 | 0.056 |
| 10 | 0.005 | 0.001 | 0.001 | 0.001 | 0.007 | 0.004 | 0.003 | 0.004 | 0.002 | 0.004 | 0.007 | 0.015 | 0.015 |
| 11 | 0.161 | 0.094 | 0.022 | 0.039 | 0.053 | 0.064 | 0.084 | 0.101 | 0.115 | 0.112 | 0.117 | 0.031 | 0.161 |
| 12 | 0.003 | 0.004 | 0.007 | 0.002 | 0.008 | 0.006 | 0.010 | 0.004 | 0.006 | 0.003 | 0.008 | 0.013 | 0.013 |
| 13 | 0.071 | 0.076 | 0.033 | 0.034 | 0.071 | 0.070 | 0.072 | 0.088 | 0.106 | 0.119 | 0.121 | 0.017 | 0.121 |
| 14 | 0.011 | 0.005 | 0.003 | 0.001 | 0.002 | 0.001 | 0.008 | 0.007 | 0.005 | 0.006 | 0.004 | 0.014 | 0.014 |
| 15 | 0.010 | 0.014 | 0.011 | 0.006 | 0.029 | 0.014 | 0.006 | 0.003 | 0.016 | 0.030 | 0.039 | 0.020 | 0.039 |
| 16 | 0.007 | 0.000 | 0.003 | 0.001 | 0.002 | 0.002 | 0.006 | 0.004 | 0.007 | 0.006 | 0.001 | 0.014 | 0.014 |
| 17 | 0.069 | 0.038 | 0.031 | 0.018 | 0.015 | 0.028 | 0.027 | 0.021 | 0.018 | 0.023 | 0.027 | 0.034 | 0.069 |
| 18 | 0.004 | 0.002 | 0.003 | 0.004 | 0.000 | 0.004 | 0.004 | 0.006 | 0.005 | 0.006 | 0.006 | 0.013 | 0.013 |
| 19 | 0.063 | 0.016 | 0.034 | 0.007 | 0.014 | 0.023 | 0.029 | 0.026 | 0.027 | 0.017 | 0.030 | 0.038 | 0.063 |
| 20 | 0.009 | 0.002 | 0.002 | 0.002 | 0.005 | 0.004 | 0.002 | 0.005 | 0.005 | 0.008 | 0.009 | 0.013 | 0.013 |
| 21 | 0.003 | 0.005 | 0.010 | 0.011 | 0.008 | 0.007 | 0.016 | 0.004 | 0.011 | 0.017 | 0.011 | 0.022 | 0.022 |
| 22 | 0.008 | 0.003 | 0.002 | 0.003 | 0.002 | 0.001 | 0.001 | 0.004 | 0.001 | 0.002 | 0.006 | 0.014 | 0.014 |
| 23 | 0.034 | 0.024 | 0.027 | 0.017 | 0.014 | 0.022 | 0.022 | 0.024 | 0.027 | 0.026 | 0.026 | 0.025 | 0.034 |
| 24 | 0.004 | 0.002 | 0.008 | 0.009 | 0.010 | 0.007 | 0.001 | 0.003 | 0.001 | 0.001 | 0.004 | 0.013 | 0.013 |
| 25 | 0.048 | 0.032 | 0.019 | 0.023 | 0.015 | 0.028 | 0.025 | 0.013 | 0.025 | 0.022 | 0.024 | 0.038 | 0.048 |
| 26 | 0.009 | 0.001 | 0.002 | 0.003 | 0.005 | 0.004 | 0.004 | 0.003 | 0.002 | 0.001 | 0.003 | 0.013 | 0.013 |
| 27 | 0.007 | 0.009 | 0.011 | 0.007 | 0.009 | 0.005 | 0.004 | 0.029 | 0.036 | 0.025 | 0.001 | 0.015 | 0.036 |
| 28 | 0.004 | 0.005 | 0.006 | 0.004 | 0.006 | 0.002 | 0.004 | 0.002 | 0.005 | 0.005 | 0.006 | 0.014 | 0.014 |
| 29 | 0.015 | 0.020 | 0.009 | 0.019 | 0.015 | 0.025 | 0.020 | 0.013 | 0.013 | 0.018 | 0.016 | 0.020 | 0.025 |
| 30 | 0.007 | 0.007 | 0.002 | 0.005 | 0.003 | 0.011 | 0.005 | 0.003 | 0.006 | 0.009 | 0.007 | 0.013 | 0.013 |
| 31 | 0.033 | 0.020 | 0.005 | 0.025 | 0.012 | 0.018 | 0.018 | 0.018 | 0.021 | 0.022 | 0.029 | 0.036 | 0.036 |
| 32 | 0.013 | 0.016 | 0.001 | 0.005 | 0.005 | 0.007 | 0.008 | 0.005 | 0.011 | 0.012 | 0.011 | 0.013 | 0.016 |
| 33 | 0.011 | 0.003 | 0.014 | 0.013 | 0.009 | 0.025 | 0.015 | 0.012 | 0.020 | 0.048 | 0.048 | 0.015 | 0.048 |
| 34 | 0.045 | 0.084 | 0.019 | 0.033 | 0.018 | 0.057 | 0.045 | 0.038 | 0.040 | 0.073 | 0.061 | 0.014 | 0.084 |
| 35 | 0.010 | 0.007 | 0.010 | 0.017 | 0.016 | 0.021 | 0.014 | 0.018 | 0.011 | 0.011 | 0.016 | 0.020 | 0.021 |
| 36 | 0.014 | 0.019 | 0.004 | 0.008 | 0.007 | 0.017 | 0.013 | 0.009 | 0.006 | 0.019 | 0.020 | 0.013 | 0.020 |
| 37 | 0.026 | 0.005 | 0.016 | 0.019 | 0.019 | 0.020 | 0.015 | 0.018 | 0.023 | 0.013 | 0.016 | 0.031 | 0.031 |
| 38 | 0.017 | 0.020 | 0.006 | 0.010 | 0.007 | 0.021 | 0.023 | 0.011 | 0.008 | 0.023 | 0.028 | 0.013 | 0.028 |
| 39 | 0.008 | 0.006 | 0.004 | 0.004 | 0.002 | 0.002 | 0.006 | 0.006 | 0.003 | 0.001 | 0.011 | 0.015 | 0.015 |
| 40 | 0.082 | 0.166 | 0.050 | 0.060 | 0.013 | 0.084 | 0.071 | 0.081 | 0.070 | 0.138 | 0.087 | 0.015 | 0.166 |
| 41 | 0.010 | 0.018 | 0.018 | 0.021 | 0.013 | 0.023 | 0.020 | 0.019 | 0.013 | 0.012 | 0.014 | 0.019 | 0.023 |
| 42 | 0.013 | 0.018 | 0.005 | 0.008 | 0.005 | 0.019 | 0.016 | 0.007 | 0.012 | 0.016 | 0.023 | 0.014 | 0.023 |
| 43 | 0.020 | 0.029 | 0.014 | 0.018 | 0.016 | 0.022 | 0.025 | 0.024 | 0.020 | 0.025 | 0.018 | 0.027 | 0.029 |
| 44 | 0.009 | 0.022 | 0.005 | 0.009 | 0.006 | 0.021 | 0.014 | 0.014 | 0.011 | 0.022 | 0.024 | 0.014 | 0.024 |
| 45 | 0.006 | 0.005 | 0.008 | 0.004 | 0.004 | 0.007 | 0.004 | 0.007 | 0.009 | 0.004 | 0.005 | 0.014 | 0.014 |
| 46 | 0.035 | 0.081 | 0.018 | 0.029 | 0.017 | 0.057 | 0.053 | 0.037 | 0.042 | 0.070 | 0.066 | 0.029 | 0.081 |
| 47 | 0.007 | 0.028 | 0.015 | 0.014 | 0.010 | 0.020 | 0.023 | 0.024 | 0.017 | 0.017 | 0.020 | 0.020 | 0.028 |
| 48 | 0.003 | 0.010 | 0.003 | 0.005 | 0.004 | 0.009 | 0.007 | 0.006 | 0.004 | 0.012 | 0.007 | 0.030 | 0.030 |
| 49 | 0.017 | 0.025 | 0.008 | 0.013 | 0.022 | 0.031 | 0.021 | 0.019 | 0.019 | 0.020 | 0.017 | 0.026 | 0.031 |
| 50 | 0.010 | 0.011 | 0.001 | 0.005 | 0.002 | 0.004 | 0.004 | 0.006 | 0.004 | 0.007 | 0.007 | 0.015 | 0.015 |
| $\begin{aligned} & \text { TDC } \\ & \text { (\%) } \end{aligned}$ | 0.072 | 0.069 | 0.012 | 0.018 | 0.036 | 0.069 | 0.075 | 0.099 | 0.115 | 0.156 | 0.151 | 0.042 | 0.156 |


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| Phase B |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{P}_{\mathrm{n}}$ (\%) | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 | 110 |  |
| Nr./ Order | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | (\%) |
| 2 | 0.008 | 0.010 | 0.014 | 0.004 | 0.008 | 0.008 | 0.011 | 0.005 | 0.008 | 0.006 | 0.008 | 0.014 | 0.014 |
| 3 | 0.017 | 0.024 | 0.032 | 0.018 | 0.074 | 0.137 | 0.179 | 0.228 | 0.255 | 0.281 | 0.323 | 0.131 | 0.323 |
| 4 | 0.005 | 0.004 | 0.004 | 0.004 | 0.004 | 0.006 | 0.006 | 0.004 | 0.005 | 0.003 | 0.007 | 0.015 | 0.015 |
| 5 | 0.114 | 0.030 | 0.004 | 0.065 | 0.084 | 0.064 | 0.040 | 0.013 | 0.032 | 0.048 | 0.078 | 0.020 | 0.114 |
| 6 | 0.009 | 0.006 | 0.001 | 0.003 | 0.003 | 0.004 | 0.007 | 0.008 | 0.006 | 0.006 | 0.001 | 0.009 | 0.009 |
| 7 | 0.047 | 0.047 | 0.016 | 0.038 | 0.095 | 0.124 | 0.121 | 0.095 | 0.084 | 0.080 | 0.048 | 0.038 | 0.124 |
| 8 | 0.003 | 0.003 | 0.004 | 0.010 | 0.003 | 0.002 | 0.000 | 0.004 | 0.003 | 0.007 | 0.003 | 0.007 | 0.010 |
| 9 | 0.010 | 0.014 | 0.017 | 0.011 | 0.011 | 0.037 | 0.044 | 0.045 | 0.040 | 0.030 | 0.014 | 0.034 | 0.045 |
| 10 | 0.008 | 0.005 | 0.003 | 0.006 | 0.007 | 0.006 | 0.003 | 0.007 | 0.002 | 0.004 | 0.007 | 0.004 | 0.008 |
| 11 | 0.145 | 0.070 | 0.044 | 0.054 | 0.067 | 0.074 | 0.092 | 0.108 | 0.120 | 0.124 | 0.112 | 0.022 | 0.145 |
| 12 | 0.016 | 0.002 | 0.003 | 0.006 | 0.005 | 0.005 | 0.006 | 0.006 | 0.004 | 0.003 | 0.003 | 0.009 | 0.016 |
| 13 | 0.067 | 0.059 | 0.031 | 0.035 | 0.066 | 0.062 | 0.067 | 0.081 | 0.103 | 0.121 | 0.109 | 0.006 | 0.121 |
| 14 | 0.007 | 0.002 | 0.001 | 0.005 | 0.005 | 0.007 | 0.004 | 0.007 | 0.003 | 0.007 | 0.005 | 0.004 | 0.007 |
| 15 | 0.003 | 0.004 | 0.004 | 0.004 | 0.036 | 0.017 | 0.017 | 0.013 | 0.023 | 0.038 | 0.037 | 0.012 | 0.038 |
| 16 | 0.007 | 0.001 | 0.003 | 0.004 | 0.003 | 0.001 | 0.004 | 0.005 | 0.004 | 0.003 | 0.004 | 0.005 | 0.007 |
| 17 | 0.060 | 0.035 | 0.033 | 0.012 | 0.024 | 0.034 | 0.026 | 0.020 | 0.017 | 0.025 | 0.033 | 0.021 | 0.060 |
| 18 | 0.017 | 0.001 | 0.003 | 0.001 | 0.005 | 0.003 | 0.002 | 0.003 | 0.003 | 0.002 | 0.003 | 0.005 | 0.017 |
| 19 | 0.068 | 0.018 | 0.037 | 0.003 | 0.022 | 0.026 | 0.029 | 0.023 | 0.022 | 0.019 | 0.016 | 0.036 | 0.068 |
| 20 | 0.008 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.001 | 0.002 | 0.002 | 0.004 | 0.007 | 0.005 | 0.008 |
| 21 | 0.004 | 0.010 | 0.007 | 0.013 | 0.007 | 0.013 | 0.029 | 0.013 | 0.008 | 0.013 | 0.016 | 0.019 | 0.029 |
| 22 | 0.005 | 0.005 | 0.005 | 0.001 | 0.005 | 0.002 | 0.004 | 0.003 | 0.003 | 0.004 | 0.003 | 0.004 | 0.005 |
| 23 | 0.026 | 0.022 | 0.019 | 0.020 | 0.020 | 0.028 | 0.020 | 0.025 | 0.030 | 0.027 | 0.021 | 0.017 | 0.030 |
| 24 | 0.011 | 0.002 | 0.002 | 0.010 | 0.002 | 0.007 | 0.002 | 0.003 | 0.003 | 0.004 | 0.002 | 0.004 | 0.011 |
| 25 | 0.044 | 0.024 | 0.020 | 0.010 | 0.015 | 0.028 | 0.009 | 0.025 | 0.017 | 0.022 | 0.016 | 0.034 | 0.044 |
| 26 | 0.009 | 0.006 | 0.003 | 0.004 | 0.003 | 0.008 | 0.005 | 0.005 | 0.002 | 0.001 | 0.002 | 0.003 | 0.009 |
| 27 | 0.005 | 0.004 | 0.011 | 0.011 | 0.003 | 0.008 | 0.007 | 0.034 | 0.045 | 0.039 | 0.012 | 0.004 | 0.045 |
| 28 | 0.005 | 0.006 | 0.003 | 0.003 | 0.004 | 0.005 | 0.007 | 0.003 | 0.004 | 0.009 | 0.006 | 0.005 | 0.009 |
| 29 | 0.008 | 0.031 | 0.008 | 0.019 | 0.019 | 0.020 | 0.014 | 0.010 | 0.015 | 0.023 | 0.018 | 0.009 | 0.031 |
| 30 | 0.010 | 0.007 | 0.002 | 0.002 | 0.005 | 0.007 | 0.007 | 0.005 | 0.007 | 0.005 | 0.006 | 0.003 | 0.010 |
| 31 | 0.035 | 0.026 | 0.009 | 0.015 | 0.017 | 0.013 | 0.017 | 0.013 | 0.009 | 0.016 | 0.016 | 0.033 | 0.035 |
| 32 | 0.014 | 0.017 | 0.002 | 0.003 | 0.006 | 0.005 | 0.011 | 0.005 | 0.011 | 0.011 | 0.009 | 0.004 | 0.017 |
| 33 | 0.009 | 0.012 | 0.017 | 0.015 | 0.016 | 0.019 | 0.006 | 0.008 | 0.016 | 0.050 | 0.055 | 0.010 | 0.055 |
| 34 | 0.038 | 0.080 | 0.018 | 0.029 | 0.020 | 0.053 | 0.047 | 0.037 | 0.041 | 0.070 | 0.064 | 0.007 | 0.080 |
| 35 | 0.002 | 0.006 | 0.009 | 0.018 | 0.016 | 0.015 | 0.009 | 0.019 | 0.026 | 0.016 | 0.010 | 0.016 | 0.026 |
| 36 | 0.018 | 0.019 | 0.001 | 0.007 | 0.009 | 0.015 | 0.011 | 0.009 | 0.009 | 0.016 | 0.021 | 0.004 | 0.021 |
| 37 | 0.021 | 0.011 | 0.013 | 0.017 | 0.011 | 0.017 | 0.015 | 0.016 | 0.012 | 0.007 | 0.009 | 0.029 | 0.029 |
| 38 | 0.005 | 0.020 | 0.008 | 0.011 | 0.010 | 0.020 | 0.022 | 0.009 | 0.007 | 0.024 | 0.030 | 0.004 | 0.030 |
| 39 | 0.010 | 0.002 | 0.001 | 0.006 | 0.012 | 0.008 | 0.004 | 0.001 | 0.009 | 0.006 | 0.010 | 0.013 | 0.013 |
| 40 | 0.086 | 0.167 | 0.052 | 0.058 | 0.013 | 0.084 | 0.070 | 0.083 | 0.067 | 0.138 | 0.089 | 0.007 | 0.167 |
| 41 | 0.002 | 0.020 | 0.011 | 0.016 | 0.016 | 0.019 | 0.014 | 0.014 | 0.015 | 0.017 | 0.014 | 0.014 | 0.020 |
| 42 | 0.004 | 0.015 | 0.006 | 0.011 | 0.008 | 0.019 | 0.017 | 0.007 | 0.010 | 0.015 | 0.022 | 0.004 | 0.022 |
| 43 | 0.018 | 0.027 | 0.017 | 0.017 | 0.015 | 0.021 | 0.015 | 0.015 | 0.019 | 0.014 | 0.016 | 0.025 | 0.027 |
| 44 | 0.019 | 0.021 | 0.005 | 0.005 | 0.010 | 0.021 | 0.018 | 0.014 | 0.012 | 0.023 | 0.024 | 0.006 | 0.024 |
| 45 | 0.005 | 0.005 | 0.007 | 0.005 | 0.009 | 0.011 | 0.010 | 0.007 | 0.009 | 0.001 | 0.004 | 0.009 | 0.011 |
| 46 | 0.048 | 0.081 | 0.020 | 0.028 | 0.021 | 0.058 | 0.055 | 0.039 | 0.041 | 0.071 | 0.064 | 0.026 | 0.081 |
| 47 | 0.004 | 0.025 | 0.010 | 0.017 | 0.015 | 0.019 | 0.020 | 0.017 | 0.017 | 0.020 | 0.020 | 0.014 | 0.025 |
| 48 | 0.007 | 0.014 | 0.003 | 0.003 | 0.003 | 0.009 | 0.010 | 0.005 | 0.005 | 0.010 | 0.008 | 0.026 | 0.026 |
| 49 | 0.017 | 0.023 | 0.013 | 0.015 | 0.017 | 0.026 | 0.021 | 0.019 | 0.013 | 0.010 | 0.014 | 0.022 | 0.026 |
| 50 | 0.012 | 0.012 | 0.003 | 0.004 | 0.002 | 0.007 | 0.004 | 0.003 | 0.005 | 0.010 | 0.005 | 0.008 | 0.012 |
| TDC <br> (\%) | 0.068 | 0.063 | 0.013 | 0.020 | 0.038 | 0.071 | 0.081 | 0.098 | 0.116 | 0.160 | 0.165 | 0.031 | 0.165 |


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| Phase C |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{P}_{\mathrm{n}}$ (\%) | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 | 110 |  |
| Nr./ Order | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | (\%) |
| 2 | 0.004 | 0.011 | 0.019 | 0.015 | 0.023 | 0.016 | 0.016 | 0.013 | 0.008 | 0.022 | 0.020 | 0.006 | 0.023 |
| 3 | 0.019 | 0.018 | 0.036 | 0.044 | 0.103 | 0.154 | 0.185 | 0.244 | 0.261 | 0.283 | 0.331 | 0.123 | 0.331 |
| 4 | 0.001 | 0.002 | 0.004 | 0.005 | 0.010 | 0.007 | 0.006 | 0.010 | 0.010 | 0.014 | 0.016 | 0.008 | 0.016 |
| 5 | 0.104 | 0.042 | 0.002 | 0.049 | 0.068 | 0.055 | 0.023 | 0.004 | 0.028 | 0.045 | 0.075 | 0.026 | 0.104 |
| 6 | 0.004 | 0.005 | 0.005 | 0.005 | 0.002 | 0.002 | 0.004 | 0.009 | 0.007 | 0.008 | 0.011 | 0.008 | 0.011 |
| 7 | 0.043 | 0.049 | 0.005 | 0.033 | 0.076 | 0.108 | 0.110 | 0.094 | 0.086 | 0.075 | 0.067 | 0.034 | 0.110 |
| 8 | 0.007 | 0.005 | 0.003 | 0.009 | 0.003 | 0.005 | 0.006 | 0.005 | 0.002 | 0.005 | 0.016 | 0.004 | 0.016 |
| 9 | 0.012 | 0.011 | 0.021 | 0.019 | 0.019 | 0.012 | 0.038 | 0.045 | 0.041 | 0.030 | 0.016 | 0.035 | 0.045 |
| 10 | 0.005 | 0.005 | 0.005 | 0.004 | 0.001 | 0.003 | 0.007 | 0.004 | 0.006 | 0.015 | 0.013 | 0.004 | 0.015 |
| 11 | 0.162 | 0.074 | 0.043 | 0.028 | 0.049 | 0.063 | 0.086 | 0.109 | 0.120 | 0.127 | 0.124 | 0.020 | 0.162 |
| 12 | 0.002 | 0.003 | 0.002 | 0.002 | 0.003 | 0.002 | 0.002 | 0.005 | 0.005 | 0.005 | 0.006 | 0.004 | 0.006 |
| 13 | 0.069 | 0.059 | 0.038 | 0.028 | 0.068 | 0.065 | 0.065 | 0.083 | 0.098 | 0.109 | 0.117 | 0.007 | 0.117 |
| 14 | 0.002 | 0.004 | 0.005 | 0.004 | 0.002 | 0.004 | 0.008 | 0.004 | 0.005 | 0.006 | 0.001 | 0.005 | 0.008 |
| 15 | 0.007 | 0.009 | 0.006 | 0.013 | 0.019 | 0.010 | 0.014 | 0.009 | 0.013 | 0.028 | 0.036 | 0.018 | 0.036 |
| 16 | 0.001 | 0.003 | 0.003 | 0.003 | 0.003 | 0.001 | 0.002 | 0.004 | 0.001 | 0.003 | 0.001 | 0.005 | 0.005 |
| 17 | 0.066 | 0.035 | 0.038 | 0.023 | 0.022 | 0.035 | 0.030 | 0.030 | 0.023 | 0.022 | 0.034 | 0.027 | 0.066 |
| 18 | 0.003 | 0.003 | 0.003 | 0.001 | 0.000 | 0.003 | 0.002 | 0.003 | 0.001 | 0.002 | 0.004 | 0.004 | 0.004 |
| 19 | 0.064 | 0.020 | 0.035 | 0.007 | 0.020 | 0.022 | 0.029 | 0.021 | 0.020 | 0.018 | 0.019 | 0.039 | 0.064 |
| 20 | 0.005 | 0.005 | 0.001 | 0.001 | 0.002 | 0.002 | 0.004 | 0.001 | 0.001 | 0.002 | 0.004 | 0.004 | 0.005 |
| 21 | 0.003 | 0.010 | 0.016 | 0.009 | 0.011 | 0.011 | 0.021 | 0.010 | 0.006 | 0.021 | 0.017 | 0.027 | 0.027 |
| 22 | 0.002 | 0.005 | 0.001 | 0.004 | 0.002 | 0.002 | 0.003 | 0.003 | 0.001 | 0.001 | 0.003 | 0.005 | 0.005 |
| 23 | 0.030 | 0.018 | 0.023 | 0.014 | 0.017 | 0.026 | 0.021 | 0.030 | 0.029 | 0.024 | 0.026 | 0.012 | 0.030 |
| 24 | 0.005 | 0.003 | 0.001 | 0.006 | 0.001 | 0.004 | 0.001 | 0.005 | 0.000 | 0.003 | 0.001 | 0.004 | 0.006 |
| 25 | 0.048 | 0.033 | 0.013 | 0.018 | 0.011 | 0.020 | 0.021 | 0.018 | 0.020 | 0.019 | 0.014 | 0.041 | 0.048 |
| 26 | 0.004 | 0.001 | 0.002 | 0.002 | 0.005 | 0.003 | 0.003 | 0.003 | 0.004 | 0.002 | 0.004 | 0.004 | 0.005 |
| 27 | 0.004 | 0.004 | 0.013 | 0.006 | 0.011 | 0.003 | 0.007 | 0.025 | 0.032 | 0.024 | 0.004 | 0.012 | 0.032 |
| 28 | 0.005 | 0.007 | 0.004 | 0.000 | 0.006 | 0.003 | 0.002 | 0.001 | 0.004 | 0.006 | 0.006 | 0.006 | 0.007 |
| 29 | 0.008 | 0.029 | 0.006 | 0.023 | 0.014 | 0.015 | 0.029 | 0.023 | 0.016 | 0.012 | 0.020 | 0.013 | 0.029 |
| 30 | 0.010 | 0.006 | 0.003 | 0.003 | 0.003 | 0.009 | 0.003 | 0.004 | 0.006 | 0.006 | 0.003 | 0.004 | 0.010 |
| 31 | 0.031 | 0.018 | 0.008 | 0.015 | 0.016 | 0.019 | 0.028 | 0.031 | 0.017 | 0.019 | 0.012 | 0.036 | 0.036 |
| 32 | 0.004 | 0.015 | 0.002 | 0.004 | 0.005 | 0.009 | 0.011 | 0.008 | 0.013 | 0.015 | 0.009 | 0.004 | 0.015 |
| 33 | 0.012 | 0.009 | 0.017 | 0.011 | 0.012 | 0.025 | 0.018 | 0.016 | 0.018 | 0.051 | 0.050 | 0.011 | 0.051 |
| 34 | 0.041 | 0.080 | 0.016 | 0.032 | 0.020 | 0.055 | 0.046 | 0.037 | 0.041 | 0.073 | 0.063 | 0.007 | 0.080 |
| 35 | 0.006 | 0.011 | 0.008 | 0.018 | 0.012 | 0.014 | 0.023 | 0.021 | 0.022 | 0.016 | 0.023 | 0.009 | 0.023 |
| 36 | 0.006 | 0.018 | 0.002 | 0.006 | 0.012 | 0.016 | 0.012 | 0.013 | 0.008 | 0.018 | 0.023 | 0.004 | 0.023 |
| 37 | 0.031 | 0.005 | 0.012 | 0.018 | 0.015 | 0.020 | 0.014 | 0.011 | 0.012 | 0.010 | 0.002 | 0.032 | 0.032 |
| 38 | 0.017 | 0.025 | 0.007 | 0.014 | 0.005 | 0.023 | 0.025 | 0.011 | 0.007 | 0.025 | 0.031 | 0.004 | 0.031 |
| 39 | 0.006 | 0.007 | 0.003 | 0.005 | 0.003 | 0.004 | 0.005 | 0.005 | 0.003 | 0.006 | 0.012 | 0.013 | 0.013 |
| 40 | 0.081 | 0.166 | 0.053 | 0.059 | 0.014 | 0.083 | 0.071 | 0.081 | 0.068 | 0.135 | 0.087 | 0.008 | 0.166 |
| 41 | 0.006 | 0.024 | 0.013 | 0.015 | 0.021 | 0.022 | 0.021 | 0.015 | 0.021 | 0.016 | 0.009 | 0.010 | 0.024 |
| 42 | 0.012 | 0.014 | 0.004 | 0.010 | 0.005 | 0.019 | 0.018 | 0.006 | 0.012 | 0.016 | 0.025 | 0.005 | 0.025 |
| 43 | 0.026 | 0.020 | 0.016 | 0.014 | 0.011 | 0.016 | 0.014 | 0.016 | 0.017 | 0.017 | 0.020 | 0.028 | 0.028 |
| 44 | 0.023 | 0.020 | 0.005 | 0.008 | 0.006 | 0.021 | 0.013 | 0.010 | 0.012 | 0.022 | 0.024 | 0.006 | 0.024 |
| 45 | 0.001 | 0.002 | 0.005 | 0.002 | 0.003 | 0.003 | 0.003 | 0.009 | 0.008 | 0.008 | 0.005 | 0.009 | 0.009 |
| 46 | 0.033 | 0.078 | 0.019 | 0.029 | 0.018 | 0.055 | 0.053 | 0.033 | 0.042 | 0.075 | 0.067 | 0.027 | 0.078 |
| 47 | 0.009 | 0.031 | 0.013 | 0.019 | 0.019 | 0.022 | 0.025 | 0.026 | 0.024 | 0.018 | 0.022 | 0.013 | 0.031 |
| 48 | 0.019 | 0.013 | 0.001 | 0.005 | 0.008 | 0.010 | 0.007 | 0.006 | 0.004 | 0.008 | 0.005 | 0.027 | 0.027 |
| 49 | 0.017 | 0.022 | 0.009 | 0.014 | 0.015 | 0.020 | 0.025 | 0.017 | 0.012 | 0.011 | 0.012 | 0.025 | 0.025 |
| 50 | 0.005 | 0.011 | 0.001 | 0.002 | 0.001 | 0.004 | 0.007 | 0.005 | 0.005 | 0.009 | 0.007 | 0.008 | 0.011 |
| TDC <br> (\%) | 0.070 | 0.063 | 0.014 | 0.018 | 0.034 | 0.068 | 0.080 | 0.107 | 0.118 | 0.157 | 0.178 | 0.031 | 0.178 |


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Total Voltage Distortion


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| FGW-TG3+SP1 |  |

### 4.3.3.3 Interharmonics at continuous operation

Test performed according to point 4.3.4 of the standard.
Measurements of interharmonics at continuous operation are done according to IEC 61000-4-7:2002.

| Phase A |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \mathbf{P}_{\mathrm{n}} \\ (\%) \\ \hline \end{gathered}$ | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 | 110 | MAX |
| $\begin{gathered} \mathbf{F} \\ {[\mathrm{Hz}]} \end{gathered}$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}$ (\%) | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $I_{\text {L }}(\%)$ | (\%) |
| 75 | 0.013 | 0.015 | 0.014 | 0.014 | 0.014 | 0.016 | 0.019 | 0.020 | 0.021 | 0.024 | 0.025 | 0.035 | 0.035 |
| 125 | 0.012 | 0.017 | 0.016 | 0.020 | 0.019 | 0.014 | 0.015 | 0.014 | 0.017 | 0.016 | 0.015 | 0.017 | 0.020 |
| 175 | 0.012 | 0.021 | 0.023 | 0.024 | 0.022 | 0.021 | 0.022 | 0.020 | 0.019 | 0.019 | 0.024 | 0.021 | 0.024 |
| 225 | 0.015 | 0.022 | 0.024 | 0.024 | 0.024 | 0.024 | 0.026 | 0.023 | 0.022 | 0.021 | 0.025 | 0.024 | 0.026 |
| 275 | 0.015 | 0.019 | 0.021 | 0.021 | 0.020 | 0.021 | 0.024 | 0.021 | 0.020 | 0.024 | 0.025 | 0.028 | 0.028 |
| 325 | 0.015 | 0.017 | 0.018 | 0.019 | 0.019 | 0.019 | 0.022 | 0.021 | 0.021 | 0.023 | 0.024 | 0.025 | 0.025 |
| 375 | 0.014 | 0.013 | 0.014 | 0.015 | 0.015 | 0.018 | 0.020 | 0.019 | 0.019 | 0.022 | 0.024 | 0.022 | 0.024 |
| 425 | 0.010 | 0.011 | 0.013 | 0.012 | 0.012 | 0.013 | 0.016 | 0.016 | 0.017 | 0.020 | 0.021 | 0.019 | 0.021 |
| 475 | 0.010 | 0.010 | 0.011 | 0.011 | 0.010 | 0.012 | 0.014 | 0.014 | 0.015 | 0.018 | 0.019 | 0.017 | 0.019 |
| 525 | 0.013 | 0.010 | 0.010 | 0.009 | 0.010 | 0.011 | 0.012 | 0.014 | 0.015 | 0.015 | 0.016 | 0.015 | 0.016 |
| 575 | 0.013 | 0.008 | 0.009 | 0.008 | 0.008 | 0.010 | 0.012 | 0.012 | 0.012 | 0.013 | 0.015 | 0.013 | 0.015 |
| 625 | 0.013 | 0.008 | 0.007 | 0.007 | 0.007 | 0.008 | 0.009 | 0.010 | 0.011 | 0.012 | 0.013 | 0.012 | 0.013 |
| 675 | 0.012 | 0.008 | 0.007 | 0.008 | 0.008 | 0.008 | 0.009 | 0.010 | 0.011 | 0.010 | 0.012 | 0.012 | 0.012 |
| 725 | 0.010 | 0.007 | 0.006 | 0.006 | 0.006 | 0.008 | 0.008 | 0.008 | 0.008 | 0.009 | 0.011 | 0.010 | 0.011 |
| 775 | 0.009 | 0.007 | 0.006 | 0.006 | 0.005 | 0.006 | 0.007 | 0.007 | 0.008 | 0.009 | 0.010 | 0.010 | 0.010 |
| 825 | 0.011 | 0.006 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.007 | 0.008 | 0.009 | 0.009 | 0.011 |
| 875 | 0.011 | 0.006 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 | 0.008 | 0.008 | 0.011 |
| 925 | 0.010 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.007 | 0.008 | 0.009 | 0.010 |
| 975 | 0.010 | 0.006 | 0.005 | 0.006 | 0.006 | 0.005 | 0.006 | 0.006 | 0.008 | 0.007 | 0.007 | 0.008 | 0.010 |
| 1025 | 0.008 | 0.006 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 | 0.008 |
| 1075 | 0.008 | 0.005 | 0.004 | 0.004 | 0.005 | 0.006 | 0.007 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 | 0.008 |
| 1125 | 0.009 | 0.005 | 0.004 | 0.004 | 0.004 | 0.006 | 0.010 | 0.007 | 0.006 | 0.012 | 0.010 | 0.007 | 0.012 |
| 1175 | 0.009 | 0.008 | 0.008 | 0.008 | 0.009 | 0.006 | 0.005 | 0.006 | 0.011 | 0.006 | 0.007 | 0.007 | 0.011 |
| 1225 | 0.009 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.007 | 0.009 |
| 1275 | 0.008 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 | 0.005 | 0.006 | 0.007 | 0.008 |
| 1325 | 0.008 | 0.005 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.007 | 0.007 | 0.008 |
| 1375 | 0.007 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 | 0.005 | 0.007 | 0.006 | 0.007 |
| 1425 | 0.008 | 0.005 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 | 0.007 | 0.006 | 0.007 | 0.008 |
| 1475 | 0.007 | 0.004 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.006 | 0.007 |
| 1525 | 0.008 | 0.004 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.006 | 0.008 |
| 1575 | 0.007 | 0.004 | 0.004 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.013 | 0.013 |
| 1625 | 0.007 | 0.004 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.006 | 0.007 |
| 1675 | 0.007 | 0.004 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.013 | 0.013 |
| 1725 | 0.007 | 0.004 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.006 | 0.007 |
| 1775 | 0.007 | 0.004 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.006 | 0.007 |
| 1825 | 0.007 | 0.004 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.006 | 0.007 |
| 1875 | 0.007 | 0.004 | 0.003 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.006 | 0.007 |
| 1925 | 0.006 | 0.004 | 0.003 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.006 | 0.006 |
| 1975 | 0.007 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.006 | 0.007 |


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| Phase B |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \mathbf{P}_{\mathrm{n}} \\ (\%) \\ \hline \end{gathered}$ | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 | 110 | MAX <br> (\%) |
| $\begin{gathered} F \\ {[\mathrm{~Hz}]} \end{gathered}$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ |  |
| 75 | 0.016 | 0.018 | 0.017 | 0.015 | 0.016 | 0.018 | 0.019 | 0.023 | 0.023 | 0.024 | 0.029 | 0.032 | 0.032 |
| 125 | 0.014 | 0.019 | 0.019 | 0.020 | 0.019 | 0.016 | 0.017 | 0.016 | 0.017 | 0.017 | 0.018 | 0.015 | 0.020 |
| 175 | 0.013 | 0.021 | 0.022 | 0.021 | 0.020 | 0.019 | 0.020 | 0.019 | 0.018 | 0.019 | 0.024 | 0.020 | 0.024 |
| 225 | 0.017 | 0.023 | 0.024 | 0.024 | 0.023 | 0.023 | 0.024 | 0.023 | 0.021 | 0.022 | 0.025 | 0.024 | 0.025 |
| 275 | 0.014 | 0.021 | 0.022 | 0.021 | 0.021 | 0.022 | 0.024 | 0.023 | 0.021 | 0.025 | 0.026 | 0.026 | 0.026 |
| 325 | 0.014 | 0.020 | 0.020 | 0.021 | 0.022 | 0.019 | 0.021 | 0.023 | 0.026 | 0.024 | 0.025 | 0.024 | 0.026 |
| 375 | 0.015 | 0.013 | 0.014 | 0.015 | 0.015 | 0.017 | 0.024 | 0.019 | 0.019 | 0.023 | 0.027 | 0.022 | 0.027 |
| 425 | 0.011 | 0.011 | 0.013 | 0.012 | 0.012 | 0.014 | 0.016 | 0.017 | 0.018 | 0.021 | 0.022 | 0.019 | 0.022 |
| 475 | 0.011 | 0.010 | 0.010 | 0.010 | 0.010 | 0.012 | 0.015 | 0.014 | 0.015 | 0.018 | 0.020 | 0.016 | 0.020 |
| 525 | 0.014 | 0.010 | 0.010 | 0.009 | 0.009 | 0.010 | 0.012 | 0.013 | 0.014 | 0.016 | 0.017 | 0.014 | 0.017 |
| 575 | 0.013 | 0.008 | 0.009 | 0.008 | 0.008 | 0.009 | 0.011 | 0.011 | 0.012 | 0.013 | 0.015 | 0.013 | 0.015 |
| 625 | 0.013 | 0.008 | 0.007 | 0.007 | 0.007 | 0.008 | 0.009 | 0.010 | 0.011 | 0.012 | 0.013 | 0.012 | 0.013 |
| 675 | 0.013 | 0.008 | 0.006 | 0.007 | 0.007 | 0.008 | 0.009 | 0.009 | 0.010 | 0.011 | 0.012 | 0.011 | 0.013 |
| 725 | 0.011 | 0.007 | 0.006 | 0.006 | 0.006 | 0.007 | 0.008 | 0.008 | 0.008 | 0.009 | 0.011 | 0.010 | 0.011 |
| 775 | 0.010 | 0.006 | 0.006 | 0.006 | 0.005 | 0.006 | 0.007 | 0.007 | 0.008 | 0.009 | 0.010 | 0.009 | 0.010 |
| 825 | 0.012 | 0.006 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.007 | 0.007 | 0.008 | 0.009 | 0.009 | 0.012 |
| 875 | 0.010 | 0.006 | 0.005 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.007 | 0.007 | 0.008 | 0.008 | 0.010 |
| 925 | 0.010 | 0.006 | 0.005 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.007 | 0.008 | 0.008 | 0.010 |
| 975 | 0.010 | 0.006 | 0.005 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.007 | 0.007 | 0.007 | 0.008 | 0.010 |
| 1025 | 0.009 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 | 0.008 | 0.009 |
| 1075 | 0.008 | 0.005 | 0.004 | 0.004 | 0.004 | 0.005 | 0.006 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 | 0.008 |
| 1125 | 0.010 | 0.005 | 0.004 | 0.004 | 0.004 | 0.005 | 0.006 | 0.005 | 0.006 | 0.006 | 0.007 | 0.007 | 0.010 |
| 1175 | 0.009 | 0.005 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.006 | 0.006 | 0.007 | 0.007 | 0.009 |
| 1225 | 0.008 | 0.005 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.008 |
| 1275 | 0.008 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.008 |
| 1325 | 0.008 | 0.005 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.007 | 0.007 | 0.008 |
| 1375 | 0.008 | 0.004 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.008 |
| 1425 | 0.009 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.009 |
| 1475 | 0.008 | 0.004 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.006 | 0.008 |
| 1525 | 0.007 | 0.004 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.006 | 0.007 |
| 1575 | 0.007 | 0.004 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.009 | 0.009 |
| 1625 | 0.008 | 0.004 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.006 | 0.008 |
| 1675 | 0.007 | 0.004 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.009 | 0.009 |
| 1725 | 0.007 | 0.004 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.006 | 0.007 |
| 1775 | 0.007 | 0.004 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.006 | 0.007 |
| 1825 | 0.007 | 0.004 | 0.003 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.006 | 0.007 |
| 1875 | 0.007 | 0.004 | 0.003 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.006 | 0.007 |
| 1925 | 0.007 | 0.004 | 0.003 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.006 | 0.007 |
| 1975 | 0.007 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.006 | 0.007 |


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| Phase C |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \mathbf{P}_{\mathrm{n}} \\ (\%) \\ \hline \end{gathered}$ | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 | 110 | MAX |
| $\begin{gathered} \mathrm{F} \\ {[\mathrm{~Hz}]} \end{gathered}$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | (\%) |
| 75 | 0.014 | 0.014 | 0.013 | 0.013 | 0.014 | 0.015 | 0.019 | 0.019 | 0.019 | 0.024 | 0.027 | 0.036 | 0.036 |
| 125 | 0.014 | 0.016 | 0.017 | 0.018 | 0.016 | 0.015 | 0.016 | 0.015 | 0.015 | 0.017 | 0.018 | 0.017 | 0.018 |
| 175 | 0.014 | 0.022 | 0.023 | 0.024 | 0.023 | 0.021 | 0.022 | 0.020 | 0.019 | 0.020 | 0.024 | 0.021 | 0.024 |
| 225 | 0.017 | 0.022 | 0.024 | 0.023 | 0.023 | 0.024 | 0.024 | 0.023 | 0.022 | 0.022 | 0.025 | 0.025 | 0.025 |
| 275 | 0.013 | 0.020 | 0.022 | 0.021 | 0.021 | 0.022 | 0.025 | 0.023 | 0.022 | 0.025 | 0.026 | 0.026 | 0.026 |
| 325 | 0.013 | 0.020 | 0.020 | 0.021 | 0.021 | 0.020 | 0.023 | 0.023 | 0.025 | 0.025 | 0.026 | 0.024 | 0.026 |
| 375 | 0.014 | 0.014 | 0.015 | 0.015 | 0.015 | 0.019 | 0.024 | 0.020 | 0.019 | 0.023 | 0.027 | 0.022 | 0.027 |
| 425 | 0.012 | 0.012 | 0.013 | 0.012 | 0.012 | 0.013 | 0.016 | 0.017 | 0.018 | 0.021 | 0.022 | 0.020 | 0.022 |
| 475 | 0.011 | 0.011 | 0.011 | 0.011 | 0.010 | 0.011 | 0.014 | 0.015 | 0.015 | 0.018 | 0.020 | 0.017 | 0.020 |
| 525 | 0.014 | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 | 0.012 | 0.013 | 0.015 | 0.016 | 0.017 | 0.014 | 0.017 |
| 575 | 0.013 | 0.009 | 0.009 | 0.008 | 0.008 | 0.010 | 0.012 | 0.012 | 0.012 | 0.014 | 0.016 | 0.013 | 0.016 |
| 625 | 0.012 | 0.008 | 0.007 | 0.007 | 0.007 | 0.008 | 0.009 | 0.010 | 0.011 | 0.012 | 0.013 | 0.012 | 0.013 |
| 675 | 0.013 | 0.008 | 0.007 | 0.007 | 0.007 | 0.008 | 0.009 | 0.009 | 0.010 | 0.011 | 0.012 | 0.011 | 0.013 |
| 725 | 0.011 | 0.007 | 0.006 | 0.006 | 0.006 | 0.007 | 0.008 | 0.008 | 0.009 | 0.010 | 0.011 | 0.011 | 0.011 |
| 775 | 0.010 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.007 | 0.008 | 0.008 | 0.009 | 0.010 | 0.010 | 0.010 |
| 825 | 0.012 | 0.007 | 0.005 | 0.005 | 0.005 | 0.006 | 0.007 | 0.007 | 0.007 | 0.008 | 0.009 | 0.009 | 0.012 |
| 875 | 0.012 | 0.006 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.007 | 0.008 | 0.008 | 0.008 | 0.012 |
| 925 | 0.010 | 0.006 | 0.005 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.007 | 0.008 | 0.008 | 0.010 |
| 975 | 0.010 | 0.006 | 0.005 | 0.006 | 0.005 | 0.005 | 0.006 | 0.006 | 0.007 | 0.007 | 0.007 | 0.008 | 0.010 |
| 1025 | 0.009 | 0.006 | 0.005 | 0.005 | 0.005 | 0.005 | 0.006 | 0.007 | 0.007 | 0.007 | 0.007 | 0.008 | 0.009 |
| 1075 | 0.008 | 0.005 | 0.004 | 0.004 | 0.004 | 0.005 | 0.006 | 0.006 | 0.006 | 0.006 | 0.008 | 0.007 | 0.008 |
| 1125 | 0.009 | 0.005 | 0.004 | 0.004 | 0.004 | 0.005 | 0.008 | 0.006 | 0.006 | 0.010 | 0.009 | 0.007 | 0.010 |
| 1175 | 0.010 | 0.007 | 0.006 | 0.007 | 0.007 | 0.005 | 0.005 | 0.006 | 0.009 | 0.006 | 0.007 | 0.007 | 0.010 |
| 1225 | 0.009 | 0.005 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.007 | 0.009 |
| 1275 | 0.008 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 | 0.005 | 0.006 | 0.007 | 0.008 |
| 1325 | 0.008 | 0.005 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.007 | 0.008 |
| 1375 | 0.007 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.007 |
| 1425 | 0.009 | 0.005 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.007 | 0.009 |
| 1475 | 0.008 | 0.004 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.006 | 0.006 | 0.008 |
| 1525 | 0.008 | 0.004 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.006 | 0.008 |
| 1575 | 0.008 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 | 0.009 | 0.009 |
| 1625 | 0.007 | 0.004 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.006 | 0.007 |
| 1675 | 0.007 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.009 | 0.009 |
| 1725 | 0.008 | 0.004 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.006 | 0.008 |
| 1775 | 0.007 | 0.004 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.006 | 0.007 |
| 1825 | 0.007 | 0.004 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.006 | 0.007 |
| 1875 | 0.007 | 0.004 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.006 | 0.007 |
| 1925 | 0.007 | 0.004 | 0.003 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.006 | 0.007 |
| 1975 | 0.006 | 0.004 | 0.003 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.006 | 0.006 |


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### 4.3.3.4 Higher frequency components

Test performed according to point 4.3.4 of the standard.
Measurements of Higher frequency are done according to IEC 61000-4-7:2002.

| Phase A |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{P}_{\text {bin }}$ (\%) | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 | 110 | AX |
| F [kHz] | l (\%) | l (\%) | l (\%) | l (\%) | l (\%) | l (\%) | $\mathrm{ln}(\%)$ | l (\%) | l (\%) | l (\%) | l (\%) | l (\%) | (\%) |
| 2.1 | 0.043 | 0.037 | 0.023 | 0.018 | 0.054 | 0.053 | 0.054 | 0.067 | 0.068 | 0.078 | 0.085 | 0.060 | 0.085 |
| 2.3 | 0.038 | 0.025 | 0.024 | 0.019 | 0.036 | 0.034 | 0.033 | 0.040 | 0.046 | 0.054 | 0.059 | 0.042 | 0.059 |
| 2.5 | 0.033 | 0.026 | 0.032 | 0.019 | 0.033 | 0.045 | 0.048 | 0.052 | 0.053 | 0.061 | 0.067 | 0.053 | 0.067 |
| 2.7 | 0.045 | 0.049 | 0.056 | 0.037 | 0.042 | 0.055 | 0.056 | 0.062 | 0.067 | 0.076 | 0.084 | 0.063 | 0.084 |
| 2.9 | 0.033 | 0.045 | 0.044 | 0.038 | 0.031 | 0.038 | 0.035 | 0.041 | 0.048 | 0.054 | 0.059 | 0.062 | 0.062 |
| 3.1 | 0.051 | 0.039 | 0.027 | 0.025 | 0.016 | 0.054 | 0.063 | 0.067 | 0.063 | 0.066 | 0.073 | 0.059 | 0.073 |
| 3.3 | 0.050 | 0.027 | 0.034 | 0.034 | 0.060 | 0.124 | 0.096 | 0.077 | 0.086 | 0.093 | 0.103 | 0.075 | 0.124 |
| 3.5 | 0.029 | 0.033 | 0.052 | 0.032 | 0.086 | 0.131 | 0.063 | 0.065 | 0.098 | 0.094 | 0.105 | 0.077 | 0.131 |
| 3.7 | 0.022 | 0.031 | 0.053 | 0.037 | 0.042 | 0.060 | 0.147 | 0.126 | 0.115 | 0.094 | 0.105 | 0.058 | 0.147 |
| 3.9 | 0.014 | 0.024 | 0.037 | 0.023 | 0.030 | 0.038 | 0.096 | 0.108 | 0.094 | 0.073 | 0.081 | 0.027 | 0.108 |
| 4.1 | 0.010 | 0.016 | 0.016 | 0.016 | 0.017 | 0.020 | 0.022 | 0.029 | 0.024 | 0.025 | 0.028 | 0.018 | 0.029 |
| 4.3 | 0.010 | 0.012 | 0.012 | 0.013 | 0.014 | 0.015 | 0.014 | 0.021 | 0.047 | 0.038 | 0.041 | 0.014 | 0.047 |
| 4.5 | 0.008 | 0.009 | 0.010 | 0.010 | 0.011 | 0.012 | 0.012 | 0.014 | 0.026 | 0.024 | 0.026 | 0.012 | 0.026 |
| 4.7 | 0.013 | 0.015 | 0.016 | 0.016 | 0.016 | 0.016 | 0.016 | 0.017 | 0.017 | 0.018 | 0.020 | 0.017 | 0.020 |
| 4.9 | 0.006 | 0.007 | 0.008 | 0.008 | 0.008 | 0.009 | 0.009 | 0.009 | 0.010 | 0.011 | 0.013 | 0.009 | 0.013 |
| 5.1 | 0.006 | 0.007 | 0.008 | 0.008 | 0.008 | 0.008 | 0.009 | 0.009 | 0.009 | 0.010 | 0.011 | 0.008 | 0.011 |
| 5.3 | 0.006 | 0.006 | 0.007 | 0.007 | 0.007 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 | 0.009 | 0.007 | 0.009 |
| 5.5 | 0.005 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 | 0.008 | 0.009 | 0.007 | 0.009 |
| 5.7 | 0.005 | 0.006 | 0.007 | 0.006 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 | 0.008 | 0.009 | 0.006 | 0.009 |
| 5.9 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 | 0.006 | 0.007 |
| 6.1 | 0.006 | 0.006 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 | 0.008 | 0.009 | 0.007 | 0.009 |
| 6.3 | 0.005 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 | 0.008 | 0.005 | 0.008 |
| 6.5 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.007 | 0.005 | 0.007 |
| 6.7 | 0.009 | 0.005 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 | 0.008 | 0.009 | 0.008 | 0.009 | 0.005 | 0.009 |
| 6.9 | 0.005 | 0.004 | 0.005 | 0.005 | 0.005 | 0.007 | 0.006 | 0.006 | 0.006 | 0.007 | 0.008 | 0.005 | 0.008 |
| 7.1 | 0.007 | 0.007 | 0.007 | 0.007 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 | 0.009 | 0.007 | 0.009 |
| 7.3 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.007 | 0.005 | 0.007 |
| 7.5 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 | 0.007 | 0.007 | 0.006 | 0.006 | 0.006 | 0.007 | 0.005 | 0.007 |
| 7.7 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.006 | 0.006 | 0.005 | 0.005 | 0.005 | 0.006 | 0.004 | 0.006 |
| 7.9 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.006 | 0.006 | 0.005 | 0.005 | 0.005 | 0.006 | 0.004 | 0.006 |
| 8.1 | 0.004 | 0.005 | 0.005 | 0.005 | 0.005 | 0.007 | 0.007 | 0.007 | 0.006 | 0.006 | 0.007 | 0.004 | 0.007 |
| 8.3 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 | 0.007 | 0.006 | 0.006 | 0.007 | 0.005 | 0.007 |
| 8.5 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 | 0.007 | 0.006 | 0.006 | 0.007 | 0.005 | 0.007 |
| 8.7 | 0.004 | 0.004 | 0.005 | 0.004 | 0.005 | 0.007 | 0.007 | 0.007 | 0.006 | 0.006 | 0.006 | 0.004 | 0.007 |
| 8.9 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.006 | 0.007 | 0.006 | 0.005 | 0.005 | 0.006 | 0.004 | 0.007 |


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| Phase B |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{P b}_{\text {bin }}$ (\%) | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 | 110 |  |
| F [kHz] | l (\%) | I (\%) | l (\%) | $\mathrm{lh}(\%)$ | l (\%) | l (\%) | l (\%) | I (\%) | l (\%) | l (\%) | l (\%) | l (\%) | (\%) |
| 2.1 | 0.040 | 0.037 | 0.022 | 0.018 | 0.051 | 0.052 | 0.053 | 0.064 | 0.067 | 0.078 | 0.085 | 0.059 | 0.085 |
| 2.3 | 0.040 | 0.024 | 0.023 | 0.018 | 0.037 | 0.037 | 0.035 | 0.044 | 0.049 | 0.057 | 0.062 | 0.042 | 0.062 |
| 2.5 | 0.036 | 0.026 | 0.034 | 0.019 | 0.031 | 0.042 | 0.044 | 0.048 | 0.049 | 0.056 | 0.062 | 0.055 | 0.062 |
| 2.7 | 0.043 | 0.049 | 0.056 | 0.034 | 0.040 | 0.056 | 0.056 | 0.061 | 0.066 | 0.076 | 0.083 | 0.064 | 0.083 |
| 2.9 | 0.036 | 0.045 | 0.043 | 0.035 | 0.032 | 0.040 | 0.037 | 0.046 | 0.052 | 0.059 | 0.064 | 0.065 | 0.065 |
| 3.1 | 0.050 | 0.040 | 0.028 | 0.024 | 0.017 | 0.056 | 0.059 | 0.061 | 0.060 | 0.062 | 0.068 | 0.058 | 0.068 |
| 3.3 | 0.050 | 0.027 | 0.033 | 0.032 | 0.060 | 0.128 | 0.097 | 0.079 | 0.085 | 0.094 | 0.104 | 0.083 | 0.128 |
| 3.5 | 0.028 | 0.034 | 0.048 | 0.034 | 0.082 | 0.133 | 0.056 | 0.073 | 0.112 | 0.102 | 0.113 | 0.087 | 0.133 |
| 3.7 | 0.023 | 0.033 | 0.058 | 0.038 | 0.043 | 0.066 | 0.153 | 0.125 | 0.110 | 0.088 | 0.097 | 0.062 | 0.153 |
| 3.9 | 0.015 | 0.024 | 0.038 | 0.024 | 0.031 | 0.041 | 0.105 | 0.121 | 0.094 | 0.079 | 0.087 | 0.029 | 0.121 |
| 4.1 | 0.011 | 0.017 | 0.017 | 0.017 | 0.019 | 0.022 | 0.024 | 0.029 | 0.027 | 0.032 | 0.035 | 0.019 | 0.035 |
| 4.3 | 0.009 | 0.013 | 0.013 | 0.013 | 0.014 | 0.015 | 0.015 | 0.021 | 0.047 | 0.035 | 0.038 | 0.015 | 0.047 |
| 4.5 | 0.008 | 0.009 | 0.010 | 0.011 | 0.011 | 0.013 | 0.012 | 0.015 | 0.032 | 0.030 | 0.033 | 0.012 | 0.033 |
| 4.7 | 0.013 | 0.015 | 0.016 | 0.016 | 0.016 | 0.017 | 0.017 | 0.017 | 0.017 | 0.019 | 0.021 | 0.018 | 0.021 |
| 4.9 | 0.006 | 0.007 | 0.008 | 0.008 | 0.008 | 0.009 | 0.009 | 0.009 | 0.009 | 0.010 | 0.012 | 0.009 | 0.012 |
| 5.1 | 0.006 | 0.007 | 0.008 | 0.008 | 0.008 | 0.009 | 0.009 | 0.009 | 0.009 | 0.010 | 0.010 | 0.008 | 0.010 |
| 5.3 | 0.006 | 0.006 | 0.007 | 0.007 | 0.007 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 | 0.009 | 0.007 | 0.009 |
| 5.5 | 0.005 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 | 0.008 | 0.008 | 0.007 | 0.008 |
| 5.7 | 0.005 | 0.006 | 0.007 | 0.006 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 | 0.008 | 0.008 | 0.006 | 0.008 |
| 5.9 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 | 0.006 | 0.007 |
| 6.1 | 0.006 | 0.006 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 | 0.008 | 0.008 | 0.007 | 0.008 |
| 6.3 | 0.005 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.007 | 0.006 | 0.007 | 0.007 | 0.005 | 0.007 |
| 6.5 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.007 | 0.005 | 0.007 |
| 6.7 | 0.009 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 | 0.008 | 0.009 | 0.010 | 0.008 | 0.009 | 0.005 | 0.010 |
| 6.9 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 | 0.005 | 0.007 |
| 7.1 | 0.008 | 0.007 | 0.007 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 | 0.009 | 0.009 | 0.007 | 0.009 |
| 7.3 | 0.005 | 0.004 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.005 | 0.006 |
| 7.5 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 | 0.007 | 0.007 | 0.006 | 0.006 | 0.007 | 0.007 | 0.005 | 0.007 |
| 7.7 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.004 | 0.006 |
| 7.9 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.006 | 0.006 | 0.005 | 0.005 | 0.005 | 0.006 | 0.004 | 0.006 |
| 8.1 | 0.004 | 0.005 | 0.005 | 0.005 | 0.005 | 0.007 | 0.007 | 0.006 | 0.006 | 0.006 | 0.007 | 0.004 | 0.007 |
| 8.3 | 0.005 | 0.006 | 0.006 | 0.006 | 0.006 | 0.007 | 0.008 | 0.007 | 0.006 | 0.007 | 0.007 | 0.005 | 0.008 |
| 8.5 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 | 0.007 | 0.006 | 0.007 | 0.007 | 0.005 | 0.007 |
| 8.7 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.007 | 0.007 | 0.007 | 0.006 | 0.006 | 0.007 | 0.004 | 0.007 |
| 8.9 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.006 | 0.007 | 0.007 | 0.005 | 0.005 | 0.006 | 0.004 | 0.007 |


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| Phase C |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{P}_{\text {bin }}$ (\%) | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 | 110 |  |
| F [kHz] | $\mathrm{I}_{\mathrm{h}}(\%)$ | l (\%) | $\mathrm{I}_{\mathrm{h}}(\%)$ | l (\%) | l (\%) | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathrm{I}_{\mathrm{h}}(\%)$ | $\mathbf{l h}(\%)$ | Ih(\%) | lh(\%) | (\%) |
| 2.1 | 0.042 | 0.038 | 0.023 | 0.016 | 0.053 | 0.055 | 0.058 | 0.068 | 0.071 | 0.083 | 0.090 | 0.060 | 0.090 |
| 2.3 | 0.039 | 0.025 | 0.024 | 0.019 | 0.038 | 0.038 | 0.038 | 0.046 | 0.052 | 0.059 | 0.065 | 0.041 | 0.065 |
| 2.5 | 0.032 | 0.026 | 0.033 | 0.019 | 0.030 | 0.042 | 0.047 | 0.049 | 0.050 | 0.059 | 0.064 | 0.058 | 0.064 |
| 2.7 | 0.042 | 0.049 | 0.057 | 0.037 | 0.040 | 0.055 | 0.058 | 0.063 | 0.068 | 0.079 | 0.086 | 0.064 | 0.086 |
| 2.9 | 0.026 | 0.046 | 0.045 | 0.037 | 0.029 | 0.040 | 0.039 | 0.048 | 0.055 | 0.061 | 0.067 | 0.065 | 0.067 |
| 3.1 | 0.053 | 0.040 | 0.028 | 0.027 | 0.017 | 0.052 | 0.060 | 0.061 | 0.059 | 0.061 | 0.068 | 0.064 | 0.068 |
| 3.3 | 0.046 | 0.026 | 0.033 | 0.033 | 0.064 | 0.122 | 0.099 | 0.080 | 0.086 | 0.094 | 0.103 | 0.074 | 0.122 |
| 3.5 | 0.028 | 0.034 | 0.050 | 0.035 | 0.087 | 0.126 | 0.055 | 0.071 | 0.106 | 0.103 | 0.114 | 0.078 | 0.126 |
| 3.7 | 0.021 | 0.031 | 0.053 | 0.037 | 0.040 | 0.062 | 0.143 | 0.118 | 0.110 | 0.085 | 0.094 | 0.055 | 0.143 |
| 3.9 | 0.015 | 0.023 | 0.037 | 0.023 | 0.029 | 0.037 | 0.098 | 0.106 | 0.095 | 0.074 | 0.082 | 0.026 | 0.106 |
| 4.1 | 0.011 | 0.016 | 0.016 | 0.016 | 0.018 | 0.021 | 0.022 | 0.029 | 0.030 | 0.026 | 0.029 | 0.017 | 0.030 |
| 4.3 | 0.009 | 0.012 | 0.012 | 0.013 | 0.013 | 0.015 | 0.014 | 0.020 | 0.042 | 0.034 | 0.037 | 0.014 | 0.042 |
| 4.5 | 0.008 | 0.009 | 0.010 | 0.011 | 0.011 | 0.013 | 0.012 | 0.014 | 0.030 | 0.026 | 0.029 | 0.011 | 0.030 |
| 4.7 | 0.013 | 0.015 | 0.016 | 0.016 | 0.016 | 0.017 | 0.016 | 0.017 | 0.017 | 0.018 | 0.020 | 0.017 | 0.020 |
| 4.9 | 0.006 | 0.007 | 0.008 | 0.008 | 0.008 | 0.009 | 0.009 | 0.009 | 0.010 | 0.011 | 0.012 | 0.009 | 0.012 |
| 5.1 | 0.006 | 0.007 | 0.008 | 0.008 | 0.008 | 0.009 | 0.009 | 0.009 | 0.009 | 0.010 | 0.011 | 0.008 | 0.011 |
| 5.3 | 0.006 | 0.006 | 0.007 | 0.007 | 0.007 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 | 0.009 | 0.007 | 0.009 |
| 5.5 | 0.005 | 0.006 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 | 0.008 | 0.008 | 0.006 | 0.008 |
| 5.7 | 0.005 | 0.006 | 0.007 | 0.006 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 | 0.008 | 0.009 | 0.006 | 0.009 |
| 5.9 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 | 0.008 | 0.006 | 0.008 |
| 6.1 | 0.006 | 0.006 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 | 0.008 | 0.008 | 0.007 | 0.008 |
| 6.3 | 0.005 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 | 0.007 | 0.008 | 0.005 | 0.008 |
| 6.5 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.007 | 0.005 | 0.007 |
| 6.7 | 0.009 | 0.006 | 0.006 | 0.006 | 0.007 | 0.008 | 0.008 | 0.009 | 0.010 | 0.008 | 0.009 | 0.005 | 0.010 |
| 6.9 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.007 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 | 0.005 | 0.007 |
| 7.1 | 0.008 | 0.007 | 0.007 | 0.007 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 | 0.009 | 0.010 | 0.007 | 0.010 |
| 7.3 | 0.005 | 0.004 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.005 | 0.006 | 0.006 | 0.005 | 0.006 |
| 7.5 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 | 0.007 | 0.007 | 0.006 | 0.006 | 0.007 | 0.007 | 0.005 | 0.007 |
| 7.7 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 | 0.006 | 0.007 | 0.006 | 0.006 | 0.006 | 0.007 | 0.004 | 0.007 |
| 7.9 | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | 0.006 | 0.006 | 0.005 | 0.005 | 0.005 | 0.006 | 0.004 | 0.006 |
| 8.1 | 0.004 | 0.005 | 0.005 | 0.005 | 0.005 | 0.007 | 0.007 | 0.007 | 0.006 | 0.006 | 0.007 | 0.004 | 0.007 |
| 8.3 | 0.005 | 0.006 | 0.006 | 0.006 | 0.006 | 0.007 | 0.008 | 0.007 | 0.007 | 0.007 | 0.007 | 0.005 | 0.008 |
| 8.5 | 0.005 | 0.006 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 | 0.007 | 0.006 | 0.006 | 0.007 | 0.005 | 0.007 |
| 8.7 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 | 0.007 | 0.007 | 0.007 | 0.006 | 0.006 | 0.007 | 0.004 | 0.007 |
| 8.9 | 0.004 | 0.004 | 0.004 | 0.005 | 0.005 | 0.006 | 0.007 | 0.007 | 0.006 | 0.005 | 0.006 | 0.004 | 0.007 |

Current high frequency harmonics (Phase A)


Current high frequency harmonics (Phase B)


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|  | FGW-TG3+SP1 |  |

### 4.3.4 Unbalances

The aim of this test is to determinate the unbalance in the PGU's fed-in current.
This test was performed according to point 4.3.5 of the standard.
They have been determined the unbalance between positive and negative sequences for currents $\left(U_{i}\right)$ using following equation:

$$
U_{i}=\left(I_{1-} / I_{1+}\right) \cdot 100 \%
$$

They have been measured currents and voltages at each power level, taking into account the positive and negative phase sequence system components, as well as the active power positive sequence.

All measurements have been recorded, at least 2 minutes per power level.
Additional information about the testing is provided below:

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| DEWE2-A4 | $2020 / 03 / 13,2020 / 8 / 19$ | 100 ms values | 10 kHz |

Test results represented in the table below are calculated as 1 minute mean values and they represent the maximum unbalance. Voltage calculations are represented as line values.

| $\begin{gathered} \mathbf{P}_{\mathbf{n}} \\ (\% S n) \end{gathered}$ | $\begin{aligned} & \text { P Measured } \\ & (\% S n) \end{aligned}$ | $\mathrm{V}_{1+}(\mathrm{V})$ | $\mathrm{V}_{1-}(\mathrm{V})$ | $\mathrm{I}_{1+}(\mathrm{A})$ | $I_{1-}(\mathrm{A})$ | $\mathrm{U}_{\mathrm{i}}(\%)$ | Number of records |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0\% | 83.6 | 230.0 | 0.2 | 1.4 | 0.1 | 4.7 | 1 |
| 10\% | 10.5 | 230.0 | 0.2 | 5.1 | 0.1 | 1.4 | 1 |
| 20\% | 19.8 | 230.0 | 0.2 | 9.5 | 0.1 | 0.8 | 1 |
| 30\% | 30.2 | 230.1 | 0.2 | 14.5 | 0.1 | 0.5 | 1 |
| 40\% | 40.0 | 230.1 | 0.2 | 19.1 | 0.1 | 0.4 | 1 |
| 50\% | 50.3 | 230.1 | 0.2 | 24.0 | 0.1 | 0.3 | 1 |
| 60\% | 60.5 | 230.1 | 0.2 | 28.9 | 0.1 | 0.3 | 1 |
| 70\% | 70.5 | 230.1 | 0.2 | 33.7 | 0.1 | 0.2 | 1 |
| 80\% | 80.6 | 230.1 | 0.2 | 38.5 | 0.1 | 0.2 | 1 |
| 90\% | 90.6 | 230.2 | 0.2 | 43.3 | 0.1 | 0.1 | 1 |
| 100\% | 100.4 | 230.2 | 0.2 | 48.0 | 0.1 | 0.1 | 1 |
| 110\% | 109.5 | 230.8 | 1.7 | 52.2 | 0.7 | 1.4 | 1 |

According to VDE-AR-N 4110: 2018-11, from the $10 \% \mathrm{Pn}$, the generating unit shall not exceed a maximum limit defined at 1.5\% for VDE-AR-N 4110: 2018-11.

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### 4.4 Disconnecting the PGU from the grid

These tests have been performed according to point 4.4 of the standard.
The aim of this test is to determine the functional capability of the grid protection and the operating range of the PGU-protection for type testing purposes.

Two different levels of voltage and frequency have been set (In overvoltage, undervoltage, overfrequency and underfrequency) in order to see that this value is configurable and all the values are in compliance with the trip limits, according to the mínimum and máximum possible trigger values and times.

Measurement for determination of under and overvoltage as well as under- and over-frequency characteristics (release values, release times and disengaging ratio) of EUT's grid protection unit are carried out as described subsequent. The settings of internal variable for the grid protection unit are given by the manufacturer.

The under and overvoltage conditions have been applied to each phase alone and to all the phases at the same time in order to see that the place of the fault is not a condition for the inverter to trip.

This test has been done performing two different tests:

- Trip voltage or frequency test, to asses that the protection function of the inverter works as the voltage and frequency levels stated by the standard.
- Trip time test, to asses that the disconnection of the inverter takes place into the time limits established by the standard.

In accordance with the table 4-49 of the standard, recommended grid protection parameters for compliance with standards VDE AR-N 4110:2018 are presented below:

| Function | Test case | Trigger threshold | Trigger time |
| :---: | :---: | :---: | :---: |
| Overvoltage U> | U1 | Min. threshold | Max. time |
|  |  | 100\% Un | 180.00 s |
|  | U2 | Max. threshold | Min. time |
|  |  | 130\% Un | 0.00 s |
| Overvoltage U>> | U3 | Min. threshold | Max. time |
|  |  | 100\% Un | 0.10 s |
|  | U4 | Max. threshold | Min. time |
|  |  | 130\% Un | 0.10 s |
| Undervoltage U< | U5 | Min. threshold | Min. time |
|  |  | 10\% Un | 0.00 s |
|  | U6 | Max. threshold | Max. time |
|  |  | 100\% Un | 2.40 s |
| Undervoltage U<< | U7 | Min. threshold | Min. time |
|  |  | 10\% Un | 0.00 s |
|  | U8 | Max. threshold | Max. time |
|  |  | 100\%Un | 0.80 s |


| Function | Test case | Trigger threshold | Trigger time |
| :---: | :---: | :---: | :---: |
| Overfrequency F> | F1 | Min. threshold | Max. time |
|  |  | 50 Hz | 5.00 s |
|  | F2 | Max. threshold | Min. time |
|  |  | 55 Hz | 0.00 s |
|  | F3 | Min. threshold | Min. time |
|  |  | 50 Hz | 0.00 s |
|  | F4 | Max. threshold | Max. time |
|  |  | 55 Hz | 5.00 s |
| Overfrequency F>> | F5 | Min. threshold | Min. time |
|  |  | 50 Hz | 0.00 s |
|  | F6 | Max. threshold | Max. time |
|  |  | 55 Hz | 0.10 s |
|  | F7 | Min. threshold | Max. time |
|  |  | 50 Hz | 0.10 s |
|  | F8 | Max. threshold | Min. time |
|  |  | 55 Hz | 0.00 s |
| Underfrequency F< | F9 | Min. threshold | Min. time |
|  |  | 45 Hz | 0.00 s |
|  | F10 | Max. threshold | Max. time |
|  |  | 50 Hz | 0.10 s |
|  | F11 | Min. threshold | Max. time |
|  |  | 45 Hz | 0.10 s |
|  | F12 | Max. threshold | Min. time |
|  |  | 50 Hz | 0.00 s |


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Following indications shall be taken into account to for test results offered.


For testing the accuracy of trigger value, the procedure followed has been the following:

- For undervoltage protection: Starting from a voltage level $2 \%$ Un above the trip value of the protection function to be tested, the voltage is decreased $0.5 \%$ Un in steps of at least $150 \%$ of the trip time delay stated in the protection function to be tested, with a minimum step time of 0,1 seconds.
- For overvoltage protection: Starting from a voltage level 2\% Un below the trip value of the protection function to be tested, the voltage is increased $0.5 \%$ Un in steps of at least $150 \%$ of the trip time delay stated in the protection function to be tested, with a minimum step time of 0,1 seconds.
- For underfrequency protection: Starting from a frequency level 0.2 Hz above the trip value of the protection function to be tested, the frequency is decreased 0.05 Hz in steps of at least $150 \%$ of the trip time delay stated in the protection function to be tested, with a minimum step time of 0,1 seconds.
- For overfrequency protection: Starting from a frequency level 0.2 Hz below the trip value of the protection function to be tested, the frequency is increased 0.05 Hz in steps of at least $150 \%$ of the trip time delay stated in the protection function to be tested, with a minimum step time of 0,1 seconds.

Maximum deviation allowed in accuracy of trigger value threshold is $1 \%$ Un for abnormal voltage protection and 0.01 Hz for abnormal frequency protection.

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### 4.4.1 Circuit breaker operating time

The operation time of circuit breaker is always the same $<50 \mathrm{~ms}$, this table shows the circuit breaker operation time:

| Testing the complete functional chain led to successful shutdown | $\square$ NO |
| :--- | :--- |
| Circuit breaker operating time | $\boxed{\text { YES }}$ |
| Failure of auxiliary power led to immediate shutdown | $\square \mathrm{ms}$ |

The following picture shows an example of the circuit breaker operation.


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### 4.4.2 Over \& undervoltage protection

Used settings of the measurement device for Over and undervoltage protection measurement.

| Measurement <br> device | Date of measurement | Recording | Sampling <br> frequency |
| :---: | :---: | :---: | :---: |
| PA3000 | $2019 / 12 / 05,2019 / 12 / 07,2019 / 12 / 08,2019 / 12 / 09$, | 100 ms values | 10 kHz |
| PA5000H | $2019 / 12 / 10,2020 / 03 / 06,2020 / 03 / 08,2020 / 03 / 14$, |  |  |
|  | $2020 / 03 / 16,2020 / 03 / 19,2020 / 03 / 24$, |  |  |
| $2020 / 04 / 30,2020 / 05 / 01$ |  |  |  |

For Over and Undervoltage protection test, the measurements have been carried out individually for all 3 phases and 3 phase test per each protection.

The following tables show the test results for trip value test and trip time test:

| Overvoltage ( $\mathrm{U}>$ ) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Settings | Setting values | Trigger values/times |  |  |  |
|  |  | 3-phase | $\mathrm{U}_{\text {A- }}$ | $\mathrm{U}_{\mathrm{B}-\mathrm{N}}$ | $\mathbf{U}_{\text {C-N }}$ |
| Min. threshold (Test case U1) | 1.00Un | 1.003Un | 1.003Un | 1.004Un | 1.004Un |
| Max. time (Test case U1) | 180.00s | 179.990s | 180.000s | 180.000s | 180.010s |
| Max. threshold (Test case U2) | 1.30Un | 1.299Un | 1.304Un | 1.304Un | 1.303Un |
| $\begin{gathered} \text { Min. time } \\ \text { (Test case U2) } \\ \hline \end{gathered}$ | 0.0s | 0.027s | 0.040s | 0.033s | 0.035s |
| Overvoltage ( $\mathrm{U} \gg$ ) |  |  |  |  |  |
| Settings | Setting values | Trigger values/times |  |  |  |
|  |  | 3-phase | $\mathrm{U}_{\text {A-N }}$ | $\mathrm{U}_{\mathrm{B}-\mathrm{N}}$ | $\mathrm{U}_{\mathrm{C}-\mathrm{N}}$ |
| Min. threshold (Test case U3) | 1.00Un | 0.998Un | 1.002 Un | 1.002 Un | 1.002 Un |
| Max. time (Test case U3) | 0.1 s | 0.125 s | 0.112 s | 0.112 s | 0.122 s |
| Max. threshold (Test case U4) | 1.30Un | 1.304Un | 1.303Un | 1.304Un | 1.304Un |
| $\begin{gathered} \text { Min. time } \\ \text { (Test case U4) } \end{gathered}$ | 0.15 | 0.105s | 0.101s | 0.095s | 0.102s |
| Undervoltage ( $\mathrm{U}<$ ) |  |  |  |  |  |
| Settings | Setting values | Trigger values/times |  |  |  |
|  |  | 3-phase | $\mathrm{U}_{\text {A-N }}$ | $\mathrm{U}_{\mathrm{B}-\mathrm{N}}$ | $\mathrm{U}_{\mathrm{C}-\mathrm{N}}$ |
| Min. threshold (Test case U5) | 0.10Un | 0.096Un | 0.096Un | 0.096Un | 0.096Un |
| Min. time (Test case U5) | 0.0s | 0.035s | 0.034s | 0.035 s | 0.043s |
| Max. threshold (Test case U6) | 1.00Un | 0.999Un | 0.998Un | 0.999Un | 0.998Un |
| Max. time (Test case U6) | 2.40 s | 2.390s | 2.390s | 2.400 s | 2.395 s |


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| Undervoltage (U<<) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Settings | Setting values | Trigger values/times |  |  |  |  |
|  | 3-phase | $\mathbf{U}_{\text {A-N }}$ | $\mathbf{U}_{\mathrm{B}-\mathrm{N}}$ | $\mathbf{U}_{\mathrm{C}-\mathrm{N}}$ |  |  |
| Min. threshold <br> (Test case U7) | 0.10 Un | 0.099 Un | 0.099 Un | 0.099 Un | 0.099 Un |  |
| Min. time <br> (Test case U7) | 0.10 s | 0.105 s | 0.093 s | 0.099 s | 0.090 s |  |
| Max. threshold <br> (Test case U8) | 1.00 Un | 0.998 Un | 0.999 Un | 0.998 Un | 0.998 Un |  |
| Max. time <br> (Test case U8) | 0.800 s | 0.818 s | 0.814 s | 0.816 s | 0.820 s |  |

The following pictures show the result obtained:


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### 4.4.3 Over \& underfrequency protection

Used settings of the measurement device for Over and undervoltage protection measurement.

| Measurement <br> device | Date of measurement | Recording | Sampling <br> frequency |
| :---: | :---: | :---: | :---: |
| PA3000 | $2019 / 12 / 05,2019 / 12 / 07,2019 / 12 / 08,2019 / 12 / 09$, | 100 ms values | 10 kHz |
| PA5000H | $2019 / 12 / 10,2020 / 03 / 06,2020 / 03 / 08,2020 / 03 / 14$, |  |  |
|  | $2020 / 03 / 16,2020 / 03 / 19,2020 / 03 / 24$, |  |  |
| $2020 / 04 / 30,2020 / 05 / 01$ |  |  |  |

For over and underfrequency protection test, the measurements have been carried out at the same time for all 3 phases.

The following tables show the test results for trip value test and trip time test:

| Overfrequency (F>) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Settings | Min. threshold |  | Max. threshold |  |
|  | Min. time (Test case F3) | Max. time (Test case F1) | Min. time (Test case F2) | Max. time (Test case F4) |
| Setting value | 50.00 Hz |  | 55.00 Hz |  |
| Trigger value | 49.998 Hz | 50.004 Hz | 55.002 Hz | 55.001 |
| Time setting value | Os | 5.000s | Os | 5s |
| Trigger time | 0.035s | 4.990 s | 0.036 s | 5.008s |


| Overfrequency ( $F \gg$ ) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Settings | Min. threshold |  | Max. threshold |  |
|  | Min. time (Test case F5) | Max. time (Test case F7) | Min. time (Test case F8) | Max. time (Test case F6) |
| Setting value | 50.00 Hz |  | 55.00 Hz |  |
| Trigger value | 49.993 Hz | 50.006 Hz | 55.050 Hz | 54.997 Hz |
| Time setting value | 0s | 0.1 s | Os | 0.1 s |
| Trigger time | 0.041s | 0.103s | 0.035s | 0.082s |


| Underfrequency ( $\mathrm{F}<$ ) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Settings | Min. threshold |  | Max. threshold |  |
|  | Min. time (Test case F9) | $\begin{gathered} \text { Max. time } \\ \text { (Test case F11) } \end{gathered}$ | Min. time (Test case F12) | Max. time (Test case F10) |
| Setting value | 45.00 Hz |  | 50.00 Hz |  |
| Trigger value | 44.994 Hz | 45.005 Hz | 49.996 Hz | 50.002 Hz |
| Time setting value | Os | 0.1 s | Os | 0.1 s |
| Trigger time | 0.036s | 0.104 s | 0.037s | 0.089s |


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### 4.4.4 Resetting Ratio

These tests have been done in order to see that if the time of the abnormal voltage conditions is lower in comparison with the setting time the inverter do not trip. These tests are only carried out on three phases. Trigger time has been set at 1.000 seconds and trigger values for over-voltage and under-voltaege at $110 \%$ Un and $80 \%$ Un respectively. Test procedure is detailed below in the following table and graphs from the standard:

## TEST PROCEDURE

| TEST PROCEDURE |  |
| :---: | :--- |
| Resetting ratio <br> Over-voltage <br> protection | Starting from a voltage of $0.98^{*}$ trigger value (S <br> tep 1), the voltage steps to $1.02^{*}$ trigger value for 500 ms (Step 2). The voltage <br> then steps back to a value of $0.98^{*}$ trigger value for 5 s (Step 3). After another <br> 5 s the voltage steps to $1.02^{*}$ trigger value and remains there until it triggers <br> (Step 4). |
| Resetting ratio <br> Under-voltage <br> protection | Starting from a voltage of $1.02^{*}$ trigger value (Step 1), the voltage steps to <br> $0.98^{*}$ trigger value for 500 $\mathrm{ms} \mathrm{(Step} \mathrm{2)} The voltage then steps back to a value$. <br> of 1.02*trigger value for 5s (Step 3). After another 5s the voltage steps to <br> $0.98^{*}$ trigger value and remains there until it triggers (Step 4). |



Fig. 4-23: Resetting ratio test for overvoltage protection


Fig. 4-24: Resetting ratio test for undervoltage protection
Used settings of the measurement device for resetting ratio.

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| PA3000 | $2019 / 12 / 11$ | 100 ms values | 10 kHz |


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The following table shows the result of resetting ratio results:

| Resetting Ratio test |  |  |  |  |  |
| :---: | :---: | :--- | :---: | :---: | :---: |
| Stage/Prot <br> Function | Step 1 |  | Step 2 |  |  |
|  | Voltage <br> measured <br> $(\%$ Un) | Time measured <br> $(\mathrm{s})$ | Voltage <br> measured <br> $(\%$ Un) | Time required <br> $(\mathrm{s})$ | Time measured <br> $(\mathrm{s})$ |
|  | 0.820 Un | 19.900 s | 0.784 Un | 0.5 s | 0.600 s |
| OV 120\% Un | 1.184 Un | 22.600 | 1.220 Un | 0.5 s | 0.600 s |


| Resetting Ratio test |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :--- | :---: |
| $\begin{array}{c}\text { Stage/Prot } \\ \text { Function }\end{array}$ | $\begin{array}{c}\text { Step 3 } \\ \text { Meltage } \\ \text { (\% Un) }\end{array}$ |  |  | $\begin{array}{c}\text { Time required } \\ \text { (s) }\end{array}$ | $\begin{array}{c}\text { Time measured } \\ \text { (s) }\end{array}$ | \(\left.$$
\begin{array}{c}\text { Disconnection }\end{array}
$$ \begin{array}{c}Disconection time <br>

(s)\end{array}\right)\)

| Resetting ratio |  |  |
| :---: | :---: | :---: |
| Type Protection | Requirement | Measurement |
| Overvoltage Protection | $>0.98$ | 1.016 |
| Undervoltage Protection | $<1.02$ | 1.025 |

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(Step 1 and Step 2)


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## Under voltage

(Step 3)

(Step 4)


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### 4.5 VERIFICATION OF CONNECTION CONDITIONS

### 4.5.1 Connection without previous protection trigger

The aim of this test is to demonstrate that a connection and reconnection of the EUT at the voltage and frequency ranges included below. This test is optional but has been tested nevertheless.

This test has been done according to chapter 4.5.1 of the standard.
Ranges for compliance with VDE AR-N 4110:2019 is:

| Type | Inferior Threshold | Superior Threshold |
| :---: | :---: | :---: |
| Voltage | $90 \% U \mathrm{Un} \pm 2 \% \mathrm{Un}$ | $110 \% \mathrm{Un} \pm 2 \% \mathrm{Un}$ |
| Frequency | $47.5 \mathrm{~Hz} \pm 0.1 \mathrm{~Hz}$ | $50.2 \mathrm{~Hz} \pm 0.1 \mathrm{~Hz}$ |

Used settings of the measurement device for connection conditions are:

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| PA3000 | $2019 / 12 / 05 \&$ | 100 ms values | 10 kHz |
|  | $2019 / 12 / 06,2020 / 4 / 23$ |  |  |

Tests consists in steps as included in table below. Each step has been maintained for 5 min and, once the EUT connects, the test is stopped.

The following table shows the test results:

| Undervoltage test |  | Overvoltage test |  | Underfrequency test |  | Overfrequecy test |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Step (\% of $U_{n}$ ) | Connection (Yes/No) | $\begin{gathered} \text { Step } \\ \text { (\% of } \\ \text { Un) } \end{gathered}$ | Connection (Yes/No) | Step <br> (Hz) | Connection (Yes/No) | Step <br> (Hz) | Connection (Yes/No) |
| 89 | $\begin{aligned} & \triangle \mathrm{NO} \\ & \square \mathrm{YES} \end{aligned}$ | 112 | $\begin{aligned} & \boxtimes \mathrm{NO} \\ & \square \mathrm{YES} \end{aligned}$ | 47.3 | $\begin{aligned} & \boxtimes \mathrm{NO} \\ & \square \mathrm{YES} \end{aligned}$ | 50.4 | $\begin{aligned} & \triangle \mathrm{NO} \\ & \square \mathrm{YES} \end{aligned}$ |
| 90 | $\begin{aligned} & \boxtimes \mathrm{NO} \\ & \square \mathrm{YES} \end{aligned}$ | 111 | $\begin{aligned} & \boxtimes \mathrm{NO} \\ & \square \mathrm{YES} \end{aligned}$ | 47.4 | $\begin{aligned} & \boxtimes \mathrm{NO} \\ & \square \text { YES } \end{aligned}$ | 50.3 | $\begin{aligned} & \boxtimes \mathrm{NO} \\ & \square \text { YES } \end{aligned}$ |
| 91 | $\begin{aligned} & \square \mathrm{NO} \\ & \triangle \mathrm{YES} \end{aligned}$ | 110 | $\begin{aligned} & \boxtimes \text { NO } \\ & \square \text { YES } \end{aligned}$ | 47.5 | $\begin{aligned} & \boxtimes \mathrm{NO} \\ & \square \text { YES } \end{aligned}$ | 50.2 | $\begin{aligned} & \boxtimes \mathrm{NO} \\ & \square \mathrm{YES} \end{aligned}$ |
|  |  | 109 | 囚 NO <br> $\square$ YES | 47.6 | $\square$ NO <br> ® YES | 50.1 | $\begin{aligned} & \square \mathrm{NO} \\ & \boxtimes \mathrm{YES} \end{aligned}$ |
|  |  | 108 | $\begin{aligned} & \square \mathrm{NO} \\ & \boxtimes \mathrm{YES} \end{aligned}$ | 47.7 | $\begin{aligned} & \square \mathrm{NO} \\ & \square \mathrm{YES} \end{aligned}$ | 50.0 | $\begin{aligned} & \square \mathrm{NO} \\ & \square \mathrm{YES} \end{aligned}$ |


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### 4.5.2 Connection after triggering of the uncoupling protection

The aim of this test is to demonstrate that the PGU does not connect within the voltage and frequency ranges given below.

This test has been performed according to point 4.5.2 of the standard.
This test allows to realize that the inverter does not connect to the grid when is out of normal operation range conditions; on the test performing time spend on each set point is greater than set reconnection time in order to see that the inverter does not connect to the grid before the normal operation conditions are reached.

Ranges for compliance with VDE AR-N 4110:2019 is:

| Type | Inferior Threshold | Superior Threshold |
| :---: | :---: | :---: |
| Voltage | $95 \% U n$ | -- |
| Frequency | 49.9 Hz | 50.1 Hz |

Used settings of the measurement device for connection conditions measurement:

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| PA3000 | $2019 / 12 / 05,2020 / 08 / 14$, | 100 ms values | 10 kHz |
|  | $2020 / 09 / 03$ |  |  |

Tests consists in steps as included in table below. Each step has been maintained for 5 min and, once the EUT connects, the test is stopped.

The following table shows the test results:

| Evidence of connection with previous protection triggering (under VDE-AR-N 4110) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Undervoltage test |  | Underfrequency test |  | Overfrequecy test |  |
| $\begin{gathered} \text { Step } \\ \left(\% \text { of } U_{n}\right) \end{gathered}$ | Connection (Yes/No) | Step (Hz) | Connection (Yes/No) | Step (Hz) | Connection (Yes/No) |
| 94 | $\begin{aligned} & \triangle N O \\ & \square \mathrm{YES} \end{aligned}$ | 49.86 | $\begin{aligned} & \triangle N O \\ & \square \mathrm{YES} \end{aligned}$ | 50.14 | $\begin{aligned} & \triangle N O \\ & \square \mathrm{YES} \end{aligned}$ |
| 95 | $\begin{aligned} & \mathrm{X} \text { NO } \\ & \square \mathrm{YES} \end{aligned}$ | 49.88 | $\begin{aligned} & \mathrm{BNO} \\ & \square \mathrm{YES} \end{aligned}$ | 50.12 | $\begin{aligned} & \triangle \mathrm{NO} \\ & \square \mathrm{YES} \end{aligned}$ |
| 96 | $\begin{aligned} & \square \mathrm{NO} \\ & \mathrm{XYES} \\ & \hline \end{aligned}$ | 49.90 | $\begin{aligned} & \mathrm{BNO} \\ & \square \mathrm{YES} \end{aligned}$ | 50.10 | $\begin{aligned} & \square \mathrm{NO} \\ & \boxtimes \mathrm{YES} \end{aligned}$ |
|  |  | 49.92 | $\begin{aligned} & \square \mathrm{NO} \\ & \boxtimes \mathrm{YES} \end{aligned}$ | 50.08 | $\begin{aligned} & \triangle \mathrm{NO} \\ & \square \mathrm{YES} \end{aligned}$ |
|  |  | 49.94 | $\begin{aligned} & \square \mathrm{NO} \\ & \square \mathrm{YES} \end{aligned}$ | 50.06 | $\begin{aligned} & \square \mathrm{NO} \\ & \square \mathrm{YES} \end{aligned}$ |

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Used settings of the measurement device for connection conditions measurement:

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| PA3000 | $2019 / 12 / 05,2020 / 09 / 03$ | 100 ms values | 10 kHz |

Tests consists in steps as included in table below. Each step has been maintained for 5 min and, once the EUT connects, the test is stopped.

The following table shows the test results:

| Evidence of connection with Release Signal (under VDE-AR-N 4110) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Undervoltage test |  |  | Underfrequency test |  |  | Overfrequecy test |  |  |
| $\begin{aligned} & \text { Step } \\ & \text { (\% of } \\ & \text { Un) } \end{aligned}$ | Release <br> Signal | Connection (Yes/No) | $\begin{aligned} & \text { Step } \\ & (\mathrm{Hz}) \end{aligned}$ | $\begin{gathered} \hline \text { Relea } \\ \text { se } \\ \text { Signal } \end{gathered}$ | Connectio n (Yes/No) | $\begin{aligned} & \text { Step } \\ & \text { (Hz) } \end{aligned}$ | Release <br> Signal | Connection (Yes/No) |
| 94 | OFF | $\begin{aligned} & \boxtimes \mathrm{NO} \\ & \square \mathrm{YES} \\ & \hline \end{aligned}$ | 49.84 | OFF | $\begin{aligned} & \mathrm{VNO} \\ & \square \mathrm{YES} \\ & \hline \end{aligned}$ | 50.14 | OFF | $\begin{aligned} & \boxtimes \mathrm{NO} \\ & \square \mathrm{YES} \\ & \hline \end{aligned}$ |
| 95 | OFF | $\begin{aligned} & \triangle \mathrm{NO} \\ & \square \mathrm{YES} \\ & \hline \end{aligned}$ | 49.86 | OFF | $\begin{aligned} & \triangle \mathrm{NO} \\ & \square \mathrm{YES} \end{aligned}$ | 50.12 | OFF | $\begin{aligned} & \triangle \mathrm{NO} \\ & \square \mathrm{YES} \end{aligned}$ |
| 96 | OFF | $\begin{aligned} & \boxed{\mathrm{NO}} \\ & \square \mathrm{YES} \\ & \hline \end{aligned}$ | 49.88 | OFF | $\begin{aligned} & \boxtimes \mathrm{NO} \\ & \square \mathrm{YES} \\ & \hline \end{aligned}$ | 50.10 | OFF | $\begin{aligned} & \boxed{\mathrm{NO}} \\ & \square \mathrm{YES} \\ & \hline \end{aligned}$ |
|  | ON | $\begin{aligned} & \square \mathrm{NO} \\ & \triangle \mathrm{YES} \\ & \hline \end{aligned}$ | 49.90 | OFF | $\begin{aligned} & \square \mathrm{NO} \\ & \triangle \mathrm{YES} \end{aligned}$ | 50.08 | OFF | $\begin{aligned} & \triangle \mathrm{NO} \\ & \square \mathrm{YES} \\ & \hline \end{aligned}$ |
|  |  |  | 49.92 | OFF | $\begin{aligned} & \mathrm{\otimes} \mathrm{NO} \\ & \square \mathrm{YES} \end{aligned}$ | 50.06 | OFF | $\begin{aligned} & \triangle \mathrm{NO} \\ & \square \mathrm{YES} \end{aligned}$ |
|  |  |  |  | ON | $\begin{aligned} & \square \mathrm{NO} \\ & \boxtimes \mathrm{YES} \end{aligned}$ |  | ON | $\begin{aligned} & \square \mathrm{NO} \\ & \triangle \mathrm{YES} \end{aligned}$ |

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### 4.6 RESPONSE DURING GRID FAULTS

The aim of this test is to determinate whether the EUT is able to detect a voltage dip and to ride through this undamaged. It can be applied to both PV and storage equipment.

These tests have been done according to point 4.6 of the standard.
The voltage dead band declared by the manufacturer is Un $\pm 10 \%$ Un for all the tests.
The inverter is configurated to limit the current when it reaches 100\% In.
The test has been carried out using a short circuit simulator which automatically adjusts the value of the series impedances and shotcircuit impedances in order to obtain the type of fault configurated for each test.

At the electric scheme below it can be seen the connection configuration for the short circuit simulator:


In the page below it is provided a table with the test conditions based on tables 4-68 and 4-69 of the FGWTG3 standard.

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| Remaining phase-to-phase voltaje [p.u] | Fault type | Fault duration compliant with: |  |  | Load | Reactive power Q/Pn | K | Test no. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AR-N <br> 4110 <br> [ms] | AR-N- <br> 4120 <br> [ms] | AR-N-4130 [ms] |  |  |  |  |
| Increase by $\geq 0.1$ to a value > 1.10 | Three phase | $\geq 5000$ |  |  | Full load | 0 \%-10 \% | $K=2$ | 115.1 |
|  |  |  |  |  | Partial Load |  |  | 115.2 |
| Rise by $\geq 0.1$ to a value $\geq 1.10$ as largest external vonductor voltage |  | $\geq 5000$ |  |  | Full load |  |  | 110.1 |
|  | Two phase |  |  |  | Partial Load | $0 \%-10 \%$ | $K=2$ | 110.2 |
| > 1.10 | Three phase | $\geq 60000$ |  |  | ( $\mathrm{P}>0,1 \mathrm{Pn}$ ) | 0 \%-10 \% | $\mathrm{K}=2$ | 110.3 |

Apart from test attached in the table above, idle tests have been performed to chech that the equipment is capable of producing te relevant voltage drop or increase with tolerances following the next images:


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For all tests, as stated in the standard, two repetitions have been done and measurements have been taken for 10 s before and after the fault. For asymmetric thwo-phase faults, different conductor voltages have been used in different tests as required by FGW TG3 Rev. 25.

Tests $50.5,50.6$ and 80.1 are done to comply with chapter 10.2.3.3.3 of VDE AR-N 4110:2018, where it is required that active and reactive current components shall be 0 A , with a maximum feed-in of apparent current ob 10\%In.

The capability of a Type-2 power generating unit to ride through several consecutive voltage dips is deemed to be proven, when the power generating unit is able to dissipate, during these network faults, at least the energy PEmax for a duration of 2 seconds without taking into account the energy fed into the network. This has been verified by testing optional test 25.3 , where multiple faults are tested in sequence.

As required by the standard, power generating systems must be capable of feeding a reactive current of $100 \%$ of the design current in each conductor. Regarding this, it has to be cheched that the following requirement is fulfilled:

$$
\begin{aligned}
& \qquad\left|I_{B 1}\right|+\left|I_{B 2}\right| \geq I_{r} \\
& \mathrm{I}_{\mathrm{B} 1}-\text { Positive sequence reactive current } \\
& \mathrm{I}_{\mathrm{B} 1}-\text { Negative sequence reactive current } \\
& \mathrm{I}_{\mathrm{r}}-\text { Rated current of the } \mathrm{PGU}
\end{aligned}
$$

For compliance with VDE AR-N 4110:2018, it has been checked that limits for rise time and settling time for both positive and negative sequence of the reactive current comply with:
$\mathrm{T}_{\text {Rise Time }} \leq 30 \mathrm{~ms}$
$\mathrm{T}_{\text {Settling Time }} \leq 60 \mathrm{~ms}$
Tolerance bands for reactive current is included in the graph below:


Figure C. 1 - Tolerance range for $\Delta i_{\mathrm{B}}$
For drops in voltage below $15 \%$ Un, rise time and settling time of reactive current is not required, and reactive current value measurement are substituted with apparent current value of positive sequence measurements.

Result tables and graphs have been included in 2219 / 0163 - A Attachment 1 of this report.

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### 4.7 Verification of the working range with regard to voltage and frequency

This test has been done according to chapter 4.7 of the standard in order to verify operation times of the EUT across the complete voltage and frequency range.

The test consists on verification of operation time at different measurement points. The test starts at rated values and then it goes through the measurements points with a gradient of maximum $5 \% \mathrm{Un} / \mathrm{min}$ or $0.5 \% \mathrm{fn} / \mathrm{min}$. In case both frequency and voltage have to change to a different setpoint, voltage changes first and then frequency, as stated in the standard. During the test, power feed-in of the EUT is set over 80\%Pn

Measurement points included in the standard are:

- Measurement point 1: $U=1.15$ p.u., $f=47.5 \mathrm{~Hz}$ recording period at least 60 s from reaching the measurement points.
- Measurement point 2: $\mathrm{U}=0.85$ p.u., $\mathrm{f}=51.5 \mathrm{~Hz}$ recording period at least 60 s from reaching the measurement points.
- Measurement point 3: $U=1.10$ p.u., $f=51.0 \mathrm{~Hz}$ recording period at least 60 min from reaching the measurement points.
- Measurement point 4: $\mathrm{U}=0.90$ p.u., $\mathrm{f}=49.0 \mathrm{~Hz}$ recording period at least 60 min from reaching the measurement points.
- Measurement point 5: U=0.90 p.u., $f=47.5 \mathrm{~Hz}$ recording period at least 30 min from reaching the measurement points.
- Measurement point 6: $U=1.09$ p.u., $f=51.5 \mathrm{~Hz}$ recording period at least 30 min from reaching the measurement points.

For each measurement point the 200 ms average values of the phase conductor voltages, the frequency as well as the active power habe been presented graphically.

These measurement points are used to verify chapters 10.2.1.2 and 11.2.3.1 of VDE AR-N 4110:2018 as, they require compliance with the following figure:


Used settings of the measurement device for connection conditions measurement:

| Measurement device | Date of measurement | Recording | Sampling frequency |
| :--- | :--- | :--- | :--- |
| PA3000 | $2019 / 12 / 05$ | 100 ms values | 10 kHz |

The following tables show the results of the tests performed:

| Measurement Point 1 |  | Over Voltage + Under Frequency |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Voltage | Frequency | Active Power <br> Desired (p.u) | Active Power <br> measured | Minimum Operation <br> Time | Time <br> measured |  |  |  |  |  |
| $\mathbf{1 1 5 \% U n}$ | 47.5 Hz | $>80.0 \% \mathrm{Pn}$ | $>95 \% \mathrm{Pn}$ | 60 seconds | 252 s |  |  |  |  |  |
| Disconnection |  |  |  |  |  |  | $\square$ YES |  |  |  |


| Measurement Point 2 |  | Under Voltage + Over Frequency |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Voltage | Frequency | Active Power <br> Desired (p.u) | Active Power <br> measured | Minimum Operation <br> Time | Time <br> measured |
| $\mathbf{8 5 \% U n}$ | 51.5 Hz | $>80.0 \% \mathrm{Pn}$ | $>95 \% \mathrm{Pn}$ | 60 seconds | 114 s |
| Disconnection |  |  |  |  |  |


| Measurement Point 3 |  | Over Voltage + Over Frequency |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Voltage | Frequency | Active Power <br> Desired (p.u) | Active Power <br> measured | Minimum Operation <br> Time | Time <br> measured |
| $110 \%$ Un | 51.0 Hz | $>80.0 \% \mathrm{Pn}$ | $>95 \% \mathrm{Pn}$ | 60 minutes | 72.6 min |
| Disconnection |  |  |  |  |  |
| $\boxed{y N O}$ | $\square$ YES |  |  |  |  |


| Measurement Point 4 |  | Under Voltage + Under Frequency |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Voltage | Frequency | Active Power <br> Desired (p.u) | Active Power <br> measured | Minimum Operation <br> Time | Time <br> measured |
| $90 \%$ Un | 49.0 Hz | $>80.0 \% \mathrm{Pn}$ | $>95 \% \mathrm{Pn}$ | 60 minutes | 63.9 min |
| Disconnection |  |  |  |  |  |
| $\square$ |  |  |  | $\square$ YES |  |


| Measurement Point 5 |  | Under Voltage + Under Frequency |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Voltage | Frequency | Active Power <br> Desired (p.u) | Active Power <br> measured | Minimum Operation <br> Time | Time <br> measured |  |  |  |  |  |  |
| $90 \%$ Un | 47.5 Hz | $>80.0 \% \mathrm{Pn}$ | $>95 \% \mathrm{Pn}$ | 30 minutes | 42 min |  |  |  |  |  |  |
| Disconnection |  |  |  |  |  |  |  | $\square$ |  |  |  |


| Measurement Point 6 |  | Over Voltage + Over Frequency |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Voltage | Frequency | Active Power <br> Desired (p.u) | Active Power <br> measured | Minimum Operation <br> Time | Time <br> measured |  |  |  |  |  |
| $109 \%$ Un | 51.5 Hz | $>80.0 \% \mathrm{Pn}$ | $>95 \% \mathrm{Pn}$ | 30 minutes | 58.2 min |  |  |  |  |  |
| Disconnection |  |  |  |  |  |  | $\square$ YES |  |  |  |

The following table shows the gradients obtained between measurement points:

| Between <br> Measurement Points | Voltage <br> Gradient <br> Required <br> $\left(\% U_{\mathbf{n}} / \mathbf{m i n}\right)$ | Voltage <br> Gradient <br> Measured <br> $\left(\% U_{\mathbf{n}} / \boldsymbol{m i n}\right)$ | Frequency <br> Gradient <br> Required <br> $\left(\% \mathbf{f}_{\mathrm{n}} / \boldsymbol{m i n}\right)$ | Frequency <br> Gradient <br> Measured <br> $\left(\% \mathbf{f}_{\boldsymbol{n}} / \mathbf{m i n}^{2}\right)$ |
| :---: | :---: | :---: | :---: | :---: |
| Point 1-2 | $<5$ | 3.97 | $<0.5$ | 0.184 |
| Point 2-3 | $<5$ | 4.17 | $<0.5$ | 0.143 |
| Point 3-4 | $<5$ | 3.99 | $<0.5$ | 0.170 |
| Point 4-5 | $<5$ | - | $<0.5$ | 0.170 |
| Point 5-6 | $<5$ | 3.34 | $<0.5$ | 0.164 |



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## Between points 2-3



Between points 3-4


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## 5 PICTURES



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Back view of main board


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Front view of display board


Back view of display board


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Front view of control board


Back view of control board


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## 6 ELECTRICAL SCHEMES

Equipment under testing


